



**A User Guide for DRAGON 3.06**

**G. MARLEAU, A. HÉBERT AND R. ROY**



## **COPYRIGHT NOTICE FOR DRAGON**

The development of DRAGON is financially supported, directly or indirectly, by various organizations including École Polytechnique de Montréal, Hydro-Québec and the Hydro-Québec chair in nuclear engineering, the Natural Science and Engineering Research Council of Canada (NSERC), Atomic Energy of Canada limited (AECL) and the CANDU Owners Group (COG). The code DRAGON and its users guide are and will remain the property of École Polytechnique de Montréal. The PostScript utility module used in DRAGON is based on PSLOT which is owned by Kevin E. Kohler at the Nova Southeastern University Oceanographic Center in Florida.

Permission is granted to the public to copy DRAGON without charge. École Polytechnique de Montréal, makes no warranty, express or implied, and assumes no liability or responsibility for the use of DRAGON.



## ACKNOWLEDGMENTS

The computer code DRAGON results from a concerted effort of professors, research scientists, research scientist and graduate students at École Polytechnique de Montréal. The main authors of this report would therefore like to express their thanks to École Polytechnique de Montréal for its support as well as to the graduate students and research staff who have contributed to the development of DRAGON along the years. We would also like to thank Kevin E. Kohler at the Nova Southeastern University Oceanographic Center for letting us use and distribute a PostScript utility module derived from his PSLOT package. Finally, the DRAGON team would never have survived without the financial support of the Natural Science and Engineering Research Council of Canada (NSERC), Hydro-Québec, Atomic Energy of Canada limited (AECL) and the CANDU Owners Group (COG).



## SUMMARY

The computer code DRAGON contains a collection of models that can simulate the neutron behavior of a unit cell or a fuel assembly in a nuclear reactor. It includes all of the functions that characterize a lattice cell code, namely: the interpolation of microscopic cross sections supplied by means of standard libraries; resonance self-shielding calculations in multidimensional geometries; multigroup and multidimensional neutron flux calculations that can take into account neutron leakage; transport-transport or transport-diffusion equivalence calculations as well as editing of condensed and homogenized nuclear properties for reactor calculations; and finally isotopic depletion calculations.

The code DRAGON contains a multigroup flux solver conceived that can use a various algorithms to solve the neutron transport equation for the spatial and angular distribution of the flux. Each of these algorithms is presented in the form of a one-group solution procedure where the contributions from other energy groups are considered as sources. The current release of DRAGON contains five such algorithms. The JPM option that solves the integral transport equation using the  $J_{\pm}$  method, (interface current method applied to homogeneous blocks); the SYBIL option that solves the integral transport equation using the collision probability method for simple one dimensional (1-D) or two dimensional (2-D) geometries and the interface current method for 2-D Cartesian or hexagonal assemblies; the EXCELL/NXT option to solve the integral transport equation using the collision probability method for more general 2-D geometries and for three dimensional (3-D) assemblies; the MOCC option to solve the transport equation using the method of cyclic characteristics in 2-D Cartesian, and finally the MCU option to solve the transport equation using the method of characteristics (non cyclic) for 3-D Cartesian geometries.

The execution of DRAGON is managed via the GAN generalized driver. The code is modular and can be interfaced easily with other production codes the finite reactor code DONJON.



## CONTENTS

COPYRIGHT NOTICE FOR DRAGON . . . . .	ii
ACKNOWLEDGMENTS . . . . .	iv
SUMMARY . . . . .	vi
CONTENTS . . . . .	viii
LIST OF FIGURES . . . . .	xii
LIST OF TABLES . . . . .	xiv
1 INTRODUCTION . . . . .	1
2 GENERAL STRUCTURE OF DRAGON INPUT . . . . .	3
2.1 Data organization . . . . .	3
2.2 DRAGON Data Structure and Module Declarations . . . . .	4
2.3 The DRAGON Modules . . . . .	5
2.4 The DRAGON Data Structures . . . . .	7
3 THE DRAGON MODULES . . . . .	9
3.1 The <b>MAC:</b> module . . . . .	9
3.1.1 The ( <b>descmac</b> ) input structure for <b>MAC:</b> . . . . .	9
3.1.2 The ( <b>descmaci</b> ) input structure for <b>MAC:</b> . . . . .	10
3.1.3 The ( <b>descmacm</b> ) input structure for <b>MAC:</b> . . . . .	12
3.1.4 Macroscopic cross section definition . . . . .	13
3.1.5 Multigroup physical albedo definition . . . . .	14
3.2 The <b>LIB:</b> module . . . . .	15
3.2.1 First format for <b>LIB:</b> data input . . . . .	16
3.2.2 Second format for <b>LIB:</b> data input . . . . .	18
3.2.3 Third format for <b>LIB:</b> data input . . . . .	19
3.2.4 Depletion data structure . . . . .	20
3.2.5 Format for ( <b>descmix1</b> ) . . . . .	21
3.2.6 Format for ( <b>descmix2</b> ) . . . . .	23
3.2.7 Format for ( <b>descmix3</b> ) . . . . .	24
3.3 The <b>GEO:</b> module . . . . .	25
3.3.1 Geometry types . . . . .	25
3.3.2 Boundary conditions . . . . .	27
3.3.3 Spatial description of geometry . . . . .	29
3.3.4 Physical properties of geometry . . . . .	33
3.3.5 Non standard geometries . . . . .	36
3.4 The tracking modules . . . . .	37
3.4.1 The general tracking data . . . . .	40
3.4.2 The <b>EXCELT:</b> specific tracking data . . . . .	41
3.4.3 The <b>NXT:</b> specific tracking data . . . . .	43
3.4.4 The <b>SYBILT:</b> specific tracking data . . . . .	45
3.4.5 The <b>JPMT:</b> specific tracking data . . . . .	47
3.4.6 The <b>BIVACT:</b> specific tracking data . . . . .	49
3.5 The <b>SHI:</b> module . . . . .	51
3.5.1 Data input for module <b>SHI:</b> . . . . .	51
3.6 The assembly modules . . . . .	53
3.6.1 Data input for module <b>ASM:</b> . . . . .	54
3.6.2 Data input for module <b>EXCELL:</b> . . . . .	55
3.7 The <b>FLU:</b> module . . . . .	56
3.7.1 Data input for module <b>FLU:</b> . . . . .	56
3.7.2 Leakage model specification structure . . . . .	59
3.8 The <b>MOCC:</b> and <b>MCU:</b> modules . . . . .	60

3.8.1	Data input for module MOCC:	61
3.8.2	Data input for module MCU:	62
3.9	The EDI: module	63
3.9.1	Data input for module EDI:	63
3.9.2	Description of the equivalence information	67
3.10	The EVO: module	69
3.10.1	Data input for module EVO:	69
3.11	The CPO: module	72
3.11.1	Data input for module CPO:	73
3.12	The INFO: module	74
3.12.1	Data input for module INFO:	74
3.13	The CFC: module	76
3.13.1	Data input for module CFC:	77
3.14	The MRG: module	78
3.14.1	Data input for module MRG:	78
3.15	The PSP: module	79
3.15.1	Data input for module PSP:	80
3.16	The SAD: module	81
3.16.1	Data input for module SAD:	81
3.17	The PER: module	84
3.17.1	Data input for module PER:	84
3.18	The HST: module	85
3.19	The TLM: module	88
3.19.1	Data input for module TLM:	89
4	EXAMPLES	91
4.1	Scattering cross sections	91
4.2	Geometries	91
4.3	Macroscopic cross sections examples	94
4.3.1	TCM01 – Annular region	94
4.3.2	TCM02 – The Stankovski test case	96
4.3.3	TCM03 – Watanabe and Maynard problem with a void region	98
4.3.4	TCM04 – Adjuster rod in a CANDU type supercell	103
4.3.5	TCM05 – Comparison of leakage models	105
4.3.6	TCM06 – Buckling search without fission source	109
4.3.7	TCM07 – Test of boundary conditions	110
4.3.8	TCM08 – Fixed source problem with fission	112
4.3.9	TCM09 – Solution of a 2-D problem using the MOCC: module	114
4.3.10	TCM10 – Solution of a 2-D problem using the MOCC: module	116
4.3.11	TCM11 – Solution of a 2-D problem using the MOCC: module	119
4.3.12	TCM12 – Solution of a 3-D problem using the MCU: module	122
4.4	WLUP microscopic cross section examples	125
4.4.1	TCWU01 – The Mosteller benchmark	125
4.4.2	TCWU02 – A 17 × 17 PWR type assembly	128
4.4.3	TCWU03 – An hexagonal assembly	131
4.4.4	TCWU04 – A Cylindrical cell with burnup	133
4.4.5	TCWU05 – A CANDU-6 type annular cell with burnup	136
4.4.6	TCWU06 – A CANDU-6 type supercell with control rods	140
4.4.7	TCWU07 – A CANDU-6 type calculation using various leakage options	143
4.4.8	TCWU08 – Burnup of an homogeneous cell	146
4.4.9	TCWU09 – Testing boundary conditions	148
4.4.10	TCWU10 – Fixed source problem in multiplicative media	150
4.4.11	TCWU11 – Two group burnup of a CANDU-6 type cell	152

4.4.12	<b>TCWU12</b> – Mixture composition . . . . .	155
4.4.13	<b>TCWU13</b> – Solution by the method of cyclic characteristics . . . . .	157
4.4.14	<b>TCWU14</b> – SPH Homogenisation without tracking . . . . .	159
REFERENCES . . . . .		163
INDEX . . . . .		193



## LIST OF FIGURES

1	Hexagonal geometries of type S30 and SA60 . . . . .	170
2	Hexagonal geometries of type SB60 and S90 . . . . .	171
3	Hexagonal geometries of type R120 and R180 . . . . .	172
4	Hexagonal geometry of type SA180 . . . . .	173
5	Hexagonal geometry of type SB180 . . . . .	174
6	Hexagonal geometry of type COMPLETE . . . . .	175
7	Description of the various rotations allowed for Cartesian geometries . . . . .	176
8	Description of the various rotation allowed for hexagonal geometries . . . . .	177
9	Typical cluster geometry . . . . .	178
10	Slab geometry with mesh splitting . . . . .	179
11	Two dimensional Cartesian assembly containing micro structures . . . . .	180
12	Cylindrical cluster geometry . . . . .	181
13	Two dimensional hexagonal geometry . . . . .	182
14	Three dimensional Cartesian supercell . . . . .	183
15	Hexagonal multicell lattice geometry . . . . .	184
16	Geometry for test case <b>TCM01</b> for an annular cell with macroscopic cross sections. . . . .	185
17	Geometry for test case <b>TCM02</b> . . . . .	186
18	Geometry for test case <b>TCM03</b> . . . . .	187
19	Geometry of the CANDU-6 supercell with stainless steel adjuster rods. . . . .	188
20	Geometry for the Mosteller benchmark problem used for <b>TCWU01</b> . . . . .	189
21	Geometry for test case <b>TCWU02</b> . . . . .	190
22	Geometry for test case <b>TCWU03</b> . . . . .	191
23	Geometry of the CANDU-6 cell. . . . .	192



## LIST OF TABLES

1	Structure ( <b>DRAGON</b> )	4
2	Structure ( <b>MAC:</b> )	9
3	Structure ( <b>descmac</b> )	10
4	Structure ( <b>descmaci</b> )	10
5	Structure ( <b>descmacm</b> )	12
6	Structure ( <b>descxs</b> )	13
7	Structure ( <b>descmpa</b> )	15
8	First form of the structure ( <b>LIB:</b> )	15
9	Second form of the structure ( <b>LIB:</b> )	15
10	Third form of the structure ( <b>LIB:</b> )	15
11	Structure ( <b>desclib</b> )	16
12	Structure ( <b>desclibbrn</b> )	19
13	Structure ( <b>desclibupd</b> )	19
14	Structure ( <b>descdepl</b> )	20
15	Structure ( <b>descmix1</b> )	21
16	Structure ( <b>descmix2</b> )	24
17	Structure ( <b>descmix3</b> )	24
18	Structure ( <b>GEO:</b> )	25
19	Structure ( <b>GEO:</b> )	25
20	Structure ( <b>descgtyp</b> )	25
21	Structure ( <b>descgent</b> )	26
22	Structure ( <b>descBC</b> )	28
23	Structure ( <b>descSP</b> )	30
24	Structure ( <b>descPP</b> )	34
25	Structure ( <b>descNSG</b> )	36
26	Structure ( <b>EXCELT:</b> )	39
27	Structure ( <b>NXT:</b> )	39
28	Structure ( <b>JPMT:</b> )	39
29	Structure ( <b>SYBILT:</b> )	40
30	Structure ( <b>BIVACT:</b> )	40
31	Structure ( <b>desctrack</b> )	40
32	Structure ( <b>descexcel</b> )	42
33	Structure ( <b>descnxt</b> )	43
34	Structure ( <b>descsybil</b> )	45
35	Structure ( <b>descjpm</b> )	47
36	Structure ( <b>descbivac</b> )	49
37	Structure ( <b>SHI:</b> )	51
38	Structure ( <b>descshi</b> )	52
39	Structure ( <b>ASM:</b> )	53
40	Structure ( <b>EXCELL:</b> )	53
41	Structure ( <b>descasm</b> )	54
42	Structure ( <b>descXL</b> )	55
43	Structure ( <b>FLU:</b> )	56
44	Structure ( <b>descflu</b> )	57
45	Structure ( <b>descleak</b> )	59
46	Structure ( <b>MOCC:</b> )	61
47	Structure ( <b>MCU:</b> )	61
48	Structure ( <b>descmoc</b> )	61
49	Structure ( <b>descmcu</b> )	62

50	Structure ( <b>EDI:</b> ) . . . . .	63
51	Structure ( <b>descedi</b> ) . . . . .	64
52	Structure ( <b>descsph</b> ) . . . . .	67
53	Structure ( <b>EVO:</b> ) . . . . .	69
54	Structure ( <b>evo</b> ) . . . . .	70
55	Structure ( <b>CPO:</b> ) . . . . .	72
56	Structure ( <b>descppo</b> ) . . . . .	73
57	Structure ( <b>INFO:</b> ) . . . . .	74
58	Structure ( <b>descinfo</b> ) . . . . .	75
59	Structure ( <b>CFC:</b> ) . . . . .	76
60	Structure ( <b>descfc</b> ) . . . . .	78
61	Structure ( <b>MRG:</b> ) . . . . .	78
62	Structure ( <b>descmrg</b> ) . . . . .	79
63	Structure ( <b>PSP:</b> ) . . . . .	79
64	Structure ( <b>descpsp</b> ) . . . . .	80
65	Structure ( <b>SAD:</b> ) . . . . .	81
66	Structure ( <b>descsad</b> ) . . . . .	81
67	Structure ( <b>PER:</b> ) . . . . .	84
68	Structure ( <b>descper</b> ) . . . . .	85
69	Updating an HISTORY structure using a MAP structure . . . . .	85
70	Updating an HISTORY structure using a BURNUP structure . . . . .	85
71	Updating a BURNUP structure using an HISTORY structure . . . . .	86
72	Updating an HISTORY structure using a MAP structure . . . . .	86
73	Structure ( <b>hstdim</b> ) . . . . .	87
74	Structure ( <b>hstbrn</b> ) . . . . .	88
75	Structure ( <b>hstpar</b> ) . . . . .	88
76	Structure ( <b>TLM:</b> ) . . . . .	88
77	Structure ( <b>desctlm</b> ) . . . . .	89

## 1 INTRODUCTION

The computer code DRAGON<sup>[1-6]</sup> results from an effort made at École Polytechnique de Montréal to rationalize and unify into a single code the different models and algorithms used to solve the neutron transport equation. One of the main concerns of the DRAGON development team was to ensure that the structure of the code was such that the development and implementation of new calculation techniques would be facilitated. DRAGON is therefore a lattice cell code which is divided into many calculation modules linked together using the GAN generalized driver<sup>[7,8]</sup>. These modules exchange information only via well defined data structures.

The two main components of the code DRAGON are its multigroup flux solver and its one group collision probability (CP) tracking modules. The CP modules all perform the same task but using different levels of approximation.

The JPM tracking option uses the interface current technique at the level of each homogeneous zones associated with a geometry ( $J_{\pm}$  method).<sup>[9]</sup> Such calculations can be performed through the use of the **JPMT:** module.<sup>[10-14]</sup> In this case one can either build the complete collision probabilities matrix or generate a response matrix both of which can be processed by the general multigroup solver. This last method permit a non iterative calculation of the one group neutron flux carried out using sparse matrix algebra.

The SYBIL tracking option emulates the main flux calculation option available in the APOLLO-1 code,<sup>[15,16]</sup> and includes a new version of the EURYDICE-2 code which performs reactor assembly calculations in both rectangular and hexagonal geometries using the interface current method. SYBIL is slightly more accurate than JPM due to the fact that it performs a complete calculation of the collision probabilities on the whole or a large part of the domain therefore avoiding for a large number of interfaces the angular flux approximation. The option is activated when the **SYBILT:** module is called.

The EXCELL tracking option is used to generate the collision probability matrices for the cases having cluster, two dimensional or three dimensional mixed rectangular and cylindrical geometries.<sup>[17,18]</sup> A cyclic tracking option is also available for treating specular boundary conditions in two dimensional rectangular geometry.<sup>[2,19-21]</sup> EXCELL calculations are performed using the **EXCELT:** module.

After the collision probability or response matrices associated with a given cell have been generated, the multigroup solution module can be activated. This module uses the power iteration method and requires a number of iteration types.<sup>[22]</sup> The thermal iterations are carried out by DRAGON so as to rebalance the flux distribution only in cases where neutron undergo upscattering. The power iterations are performed by DRAGON to solve the fixed source or eigenvalue problem in the cases where a multiplicative medium is analyzed. The effective multiplication factor ( $k_{eff}$ ) is obtained during the power iterations. A search for the critical buckling may be superimposed upon the power iterations so as to force the multiplication factor to take on a fixed value.<sup>[23]</sup>

DRAGON can access directly microscopic cross-section libraries defined according to the following standard formats: DRAGLIB<sup>[24]</sup>, MATXS<sup>[25-27]</sup> WIMS-D4<sup>[28-31]</sup> and WIMS-AECL<sup>[32]</sup>. It has the capability of exchanging macroscopic cross-section libraries with a code such as TRANSX-CTR or TRANSX-2 by the use of GOXS and ISOTXS format files.<sup>[25,33]</sup> The macroscopic cross section can also be read in DRAGON via the input data stream.



## 2 GENERAL STRUCTURE OF DRAGON INPUT

The input to DRAGON is set up in the form of a structure containing commands that call successively each of the calculation modules required in a given transport calculation.

### 2.1 Data organization

The instructions to control the execution DRAGON are generally stored in a file (also known as the the input deck or the INPUT data structure) as a collection of sequential ASCII record. The logical organization of the input deck is in the form of a list input variables and keywords presented in free format. This structure must be located in the first 72 columns of each record in the input stream. Characters located in column 73 and above can be used to identify a record and are treated as comments. An input variable can be defined in one of two ways.

- As a set of consecutive characters containing no blanks; it will be automatically interpreted by DRAGON as being either an INTEGER, a REAL, a DOUBLE PRECISION or a CHARACTER variable depending on the format of the input variable. The identification of INTEGER, REAL and DOUBLE PRECISION variables follows the FORTRAN prescriptions, everything else is automatically assumed to represent a character variable.
- As a set of characters enclosed between quotation marks ('\_'). In this case, the information is always assumed to represent a character variable.

The only separator allowed between two input variables is one or more blank character (not enclosed between quotation marks). A single input variable cannot span two records. Comments can also be included in the input deck in one of the following ways:

- characters in column 73 or higher on a record;
- characters following the ; keyword on a record;
- each record starting with the characters \*;
- characters on a given record following a ! are also commented out.

These comments are not transferred to DRAGON during the execution but are useful to document the input data structure.

This users guide was written using the following conventions:

- An input structure represents a set of input variables. It is identified by a name in boldface surrounded by parenthesis. For example, the complete DRAGON input deck is represented by the structure (**DRAGON**);
- A standard DRAGON data structure represents a set of records and directory stored in a hierarchical format on a direct access XSM file or in memory via a linked list.<sup>[4]</sup> It is identified by a name in small capital letters. For example, the data structure ASMPIJ contains the multigroup collision probability matrices generated by the ASM: module of DRAGON;
- The variables presented using the typewriter font are character variables used as keywords. For example **GEO:** is the keyword required to activate the geometry reading module of DRAGON.
- The variables in *italics* are user defined variables. When indexed and surrounded by parenthesis they denote arrays. If they are in lower case they represent either integer type (starting with *i* to *n*) or real type (starting with *a* to *h* or *o* to *z*) variables. If they are in upper case they represent character type variables. For example, *iprint* must be replaced in the input deck by an integer variable, (*energy(g)*, *g=1,ngroup+1*) states that a vector containing *ngroup+1* real elements is to be read while *FILE* must be replaced by a character variable, its maximum size being specified. No character variable can exceed 72 character in length.

- The variables or structures surrounded by single square brackets [  $\square$  ] are optional.
- The variables or structures surrounded by double square brackets [ [  $\square$  ] ] are also optional. However, they can be repeated as many times as required.
- The variables or structures surrounded by braces and separated by vertical bars {  $\square$  |  $\square$  |  $\square$  } represents various calculation options available in DRAGON. Only one of these options is permitted.
- The variables or structures surrounded by >>  $\square$  << represents CLE-2000 output parameters.<sup>[7,8]</sup>

When a fixed default value is specified for an optional parameter in a structure, it can be modified only locally and is reset to the original default value each time the module is called. When a floating default value is specified, it is saved on the output data structure and can be used in later calls to this module provided the same output data structure is in update mode. In DRAGON, almost every default value is a floating value, with the exception of the parameter *iprint*, which is set to 1 and is used to control the amount of information printed in the module. Departure from this general rule will be indicated in the following sections.

## 2.2 DRAGON Data Structure and Module Declarations

DRAGON is built around the GAN generalized driver.<sup>[7,8]</sup> Accordingly, all the modules that will be used during the current execution must first be identified. One must also define the format of each data structure that will be processed by these modules. Then, the modules required for the specific DRAGON calculation are called successively, the information generated by the execution of a module being transferred to another module via the data structures. Finally, the execution of DRAGON is terminated when it encounters the **END:** module even if it is followed by additional data records in the input data stream. The general input data structure therefore follows the calling specifications given below:

Table 1: Structure (**DRAGON**)

```
[ MODULE (MODNAME(i), i = 1, NM) ; ]
[ LINKED_LIST (STRNAME(i), i = 1, NL) ; ]
[ XSM_FILE (STRNAME(i), i = 1, NX) ; ]
[ SEQ_BINARY (STRNAME(i), i = 1, NB) ; ]
[ SEQ_ASCII (STRNAME(i), i = 1, NA) ; ]
[[ (module) ; ]]
[ PROCEDURE (PROCNAME(i), i = 1, NM) ; ]
END: ;
```

where

<b>MODULE</b>	keyword used to specify the list of modules to be used in this DRAGON execution.
<b>MODNAME</b>	list of $N_M$ character*12 name of DRAGON or utility module. The list of DRAGON module is provided in Section 2.3. The number of module declared $N_M$ depends on the particular application of DRAGON.
<b>LINKED_LIST</b>	keyword used to specify which data structures will be stored in linked lists.
<b>XSM_FILE</b>	keyword used to specify which data structures will be stored on XSM format files.
<b>SEQ_BINARY</b>	keyword used to specify which data structures will be stored on sequential binary files.
<b>SEQ_ASCII</b>	keyword used to specify which data structures will be stored on sequential ASCII files.

<b>STRNAME</b>	list of $N_L$ , $N_X$ , $N_B$ or $N_A$ <b>character*12</b> name of DRAGON data structure. The list of DRAGON data structure is presented in Section 2.4. The number of module of each type declared depends on the particular application of DRAGON.
<b>(module)</b>	input specifications for a DRAGON or utility module. For the DRAGON specific modules these input structures will be defined in Section 3.
<b>PROCEDURE</b>	keyword used to specify the list of user defined procedure to be used in this DRAGON execution.
<b>PROCNAME</b>	list of $N_M$ <b>character*12</b> name of DRAGON procedure. These procedures are stored in a file with name <b>PROCNAME.c2m</b> and contain standard DRAGON instructions. <sup>[7,8]</sup>
<b>END:</b>	keyword to call the normal end-of-execution utility module.
<b>;</b>	end of record keyword. This keyword is used by DRAGON to delimit the part of the input data stream associated with each module.

Note that the user generally has the choice to declare most of the data structures in the format of a linked list to reduce CPU times or as a XSM file to reduce memory resources. Some exceptions to this general rule are the tracking files as we will see in Section 3.4. In general, the data structure are stored on the sequential ASCII files only for backup purposes. The input data normally ends with a call to the **END:** module.

Each **(module)** specification contains a description of the execution modules to be called and its associated input structure. All these modules, except the **END:** module may be called more than once.

### 2.3 The DRAGON Modules

The code DRAGON has been divided into 24 main calculations sequences to which is generally associated a single calculation module. The only exception to this rule is the tracking sequence to which is associated five different modules, one for each of the standard CP and MOC tracking options and an additional module for diffusion calculations. However, this later module can only be used indirectly in the edition module of DRAGON. These modules perform the following tasks:

<b>MAC:</b>	module used to generate or modify a DRAGON MACROLIB (see Section 2.4) which contains the group ordered macroscopic cross sections for a series of mixture (see Section 3.1). This MACROLIB can be either an independent data structure or it can be included as a substructure in a MICROLIB. The spatial location of these mixtures in a geometry will be defined using the <b>GEO:</b> module (see Section 3.3).
<b>LIB:</b>	module used to generate or modify a DRAGON MICROLIB (see Section 2.4) that can read a number of different types of microscopic cross-section libraries (see Section 3.2). Each such access requires a double interpolation (temperature, dilution) carried out by a subroutine specifically tailored to each type of library. Currently the formats DRAGLIB <sup>[24]</sup> , MATXS <sup>[25,26]</sup> , WIMS-D4 <sup>[28-31]</sup> , and WIMS-AECL <sup>[32]</sup> are supported. After having interpolated the microscopic cross sections for each isotope, they are then multiplied by the isotopic concentrations (particles per $cm^3$ ) and combined in such a way as to produce an embedded MACROLIB (see Section 2.4). The spatial location of these mixtures in a geometry will be defined using the <b>GEO:</b> module (see Section 3.3).
<b>GEO:</b>	module used to generate or modify a geometry (see Section 3.3).
<b>EXCELLT:</b>	the standard EXCELL type tracking module for 2-D and 3-D geometries as well as isolated 2-D cells containing clusters (see Section 3.4.2).
<b>NXT:</b>	the new EXCELL type tracking module for 2-D and 3-D assemblies of clusters (see Section 3.4.3).

<b>SYBILT:</b>	the standard tracking module based on the Interface Current technique (see Section 3.4.4).
<b>JPMT:</b>	the standard tracking module based on the $J_{\pm}$ technique (see Section 3.4.5).
<b>BIVACT:</b>	the diffusion tracking module (see Section 3.4.6).
<b>SHI:</b>	module used to perform self-shielding calculations (see Section 3.5).
<b>ASM:</b>	module that uses the tracking information to generate a multigroup response or collision probability matrix (see Section 3.6.1).
<b>EXCELL:</b>	module that combines the tracking module <b>EXCELT:</b> and the assembly module <b>ASM:</b> thereby avoiding the generation of a binary tracking file (see Section 3.6.2).
<b>FLU:</b>	module that uses the multigroup response or collision probability matrix to solve the transport equation for the flux (see Section 3.7).
<b>MOCC:</b>	module to solve the transport equation for the flux using the cyclic method of characteristics with mirror like boundary conditions for 2-D geometry (see Section 3.8.1). <sup>[34,35]</sup>
<b>MCU:</b>	module to solve the transport equation for the flux using the method of characteristics with white boundary conditions for 3-D geometry (see Section 3.8.2). <sup>[36-38]</sup>
<b>EDI:</b>	editing module (see Section 3.9).
<b>EVO:</b>	burnup module (see Section 3.10).
<b>CPO:</b>	reactor database construction module (see Section 3.11).
<b>INFO:</b>	utility module to compute the density and isotopic contents of heavy or light water and the isotopic contents of $\text{UO}_2$ or $\text{ThUO}_2$ fuels (see Section 3.12).
<b>CFC:</b>	module used to create a reactor cross section database with Feedback coefficients (see Section 3.13). <sup>[39-41]</sup>
<b>MRG:</b>	module used to pre-homogenize a geometry tracked using the module <b>EXCELT:</b> (see Section 3.14).
<b>PSP:</b>	module to generate PostScript images for 2-D geometries that can be tracked using the module <b>EXCELT:</b> (see Section 3.15).
<b>SAD:</b>	module used to compute the generalized adjoint fluxes associated with the homogenized and condensed cross-sections (see Section 3.16). <sup>[42-46]</sup>
<b>PER:</b>	generalized perturbation theory module (see Section 3.17). <sup>[42-46]</sup>
<b>HST:</b>	module used to manage a full reactor execution in <b>DONJON</b> <sup>[47]</sup> using explicit <b>DRAGON</b> calculations for each cell (see Section 3.18). <sup>[48-51]</sup>
<b>TLM:</b>	module used to generate a Matlab <sup>[52]</sup> <b>m-file</b> to obtain a graphics representation of the <b>NXT:</b> tracking lines (see Section 3.19). <sup>[53]</sup>

## 2.4 The DRAGON Data Structures

The transfer of information between the DRAGON execution modules is ensured by well defined data structure. They are generally created or modified directly by one of the modules of DRAGON or by one of the utility modules. Here we will give a brief description of these data structures but their complete contents can be found in an independent report.<sup>[4]</sup>

Note that the execution of a sequence of module in DRAGON could easily be replaced by a sequence of DRAGON single module executions provided the data structure generated by the different modules are save on a physical support (created on an XSM file or exported to a XSM or a sequential ASCII file). These files can be re-imported in and then used for subsequent calculations. This is also the preferred method for restarting an execution that has been stopped prematurely.

MACROLIB	a standard data structure used by DRAGON to transfer group ordered macroscopic cross sections between its modules. It can be a stand-alone structure or it can be included into a larger structure, such as a MICROLIB or an EDITION structure. When used by a DRAGON module it must be stored either in a linked list or an XSM file. It can be created by the MAC:, LIB: and EDI: modules. It can also be modified by the SHI: and EVO: modules. Such a structure (either stand-alone or as part of a MICROLIB) is also required for a successful execution of the ASM: and FLU: modules.
MICROLIB	a standard data structure used by DRAGON to transfer microscopic and macroscopic cross sections between its modules. It always include a MACROLIB substructure. It can be a stand-alone structure or included into a larger structure, such as an EDITION structure. When used by a DRAGON module it must be stored either in a linked list or an XSM file. It can be created by the LIB: and EDI: modules. It can also be modified by the MAC:, SHI: and EVO: modules.
GEOMETRY	a standard data structure used by DRAGON to transfer the geometry between its modules. It can be a stand-alone structure or included into a larger structure, such as another GEOMETRY structure. When used by a DRAGON module it must be stored either in a linked list or an XSM file. It can be created by the GEO: module. Such a structure is also required for a successful execution of the modules JPMT:, SYBILT:, EXCELT:, EXCELL:, NXT:, BIVACT: and PSP:.
TRACKING	a standard data structure used by DRAGON to transfer the general tracking information between its modules. It is a stand-alone structure. When used by a DRAGON module it must be stored on a linked list (or an XSM file when the NXT: module is used). It can be created by the JPMT:, SYBILT:, EXCELT:, EXCELL: and NXT: modules. Such a structure is also required for a successful execution of the ASM:, FLU:, MOCC, MCU:, EDI:, EVO:, MRG:, PSP:, SAD: and PER: modules.
ASMPIJ	a standard data structure used by DRAGON to transfer the multigroup response and collision probability matrices between its modules. It is a stand-alone structure. When used by a DRAGON module it must be stored on a linked list or an XSM file. It is created by the ASM: and EXCELL: module. Such a structure is also required for a successful execution of the FLU: module.
FLUXUNK	a standard data structure used by DRAGON to transfer the flux between its modules. It is a stand-alone structure. When used by a DRAGON module it must be stored on a linked list or an XSM file. It is created by the FLU:, MOCC:, MCU: and SAD: modules. Such a structure is also required for a successful execution of the EDI: and EVO: modules. It can also be used by the PSP: module.
EDITION	a standard data structure used by DRAGON to store condensed and merged microscopic and macroscopic cross sections. It is a stand-alone structure but can contain MACROLIB and MICROLIB substructure. When used by a DRAGON module it must be stored on a linked list or an XSM file. It is created by the EDI: module. Such a structure is also required for a successful execution of the CPO: module.

BURNUP	a standard data structure used by DRAGON to store burnup information. It is a stand-alone structure that must be stored on a linked list or an XSM file. It is created by the EVO: module. Such a structure is also required for a successful execution of the CPO: module.
CPO	a standard data structure used by DRAGON to store reactor related diffusion coefficients and microscopic and macroscopic cross sections. It is a stand-alone structure that must be stored on a linked list or an XSM file. It is created by the CPO: module. Such a structure is also required for a successful execution of the CFC: module.
FBMXSDB	a standard data structure used by DRAGON to store a full reactor cross section database with Feedback coefficients. It is a stand-alone structure that must be stored on a linked list or an XSM file. It is created by the CFC: module.
HISTORY	This data structure contains the information required to ensure a smooth coupling of DRAGON with DONJON when an history based full reactor calculation is to be performed. It is used only by the HST: module.

### 3 THE DRAGON MODULES

The input to DRAGON is set up in the form of a structure containing commands that call successively each of the modules required for a given lattice calculation.

#### 3.1 The **MAC:** module

In DRAGON, the **MAC:** module is used to generate the macroscopic cross sections associated with a mixture and store them in a **MACROLIB**. The **MAC:** module may process the information in one of three different ways. First, one can read the cross sections directly the input stream. The second method is via a **GOXS** format binary sequential file.<sup>[25]</sup> It should be noted that a number of **GOXS** files may be read successively by DRAGON and that it is possible to combine data from **GOXS** files with data taken from the input stream. The third input method is through a file that already contains a **MACROLIB** (a **MICROLIB** or an **EDITION**). One can also transfer the macroscopic cross sections stored in a **MACROBIL** to a **GOXS** format binary file if required.

The general format of the data for the **MAC:** module is the following:

Table 2: Structure (**MAC:**)

```
{ MACLIB := MAC: [ MACLIB ] :: (descmac) (descmaci)
  | MICLIB := MAC: MICLIB :: (descmac) (descmaci)
  | MACLIB := MAC: [ MACLIB ] OLDLIB :: (descmac) (descmacm)
}
```

Here the first form is for the case where a single **MACROLIB** is involved, the second form corresponds to the case where a single **MICROLIB** is to be processed and finally the third form is valid when two **MACROLIB** or **MICROLIB** libraries are to be combined. The meaning of each of the terms above is:

<b>MACLIB</b>	<b>character*12</b> name of a <b>MACROLIB</b> that will contain the macroscopic cross sections. When <b>MACLIB</b> is created, all macroscopic cross sections are first initialized to zero.
<b>MICLIB</b>	<b>character*12</b> name of a <b>MICROLIB</b> . Only the <b>MACROLIB</b> data substructure of this <b>MICROLIB</b> is then updated. This is used mainly to associate fixed sources densities with various mixtures. If any other cross section is modified for a specific mixture, the microscopic and macroscopic cross sections are no longer compatible. One can return to a compatible library using the library update module (see Section 3.2).
<b>OLDLIB</b>	<b>character*12</b> name of a <b>MACROLIB</b> or a <b>MICROLIB</b> that will be used to update or create the <b>MACLIB</b> <b>MACROLIB</b> .
( <b>descmac</b> )	general <b>MAC:</b> processing instructions (see Section 3.1.1).
( <b>descmaci</b> )	instructions to read the macroscopic cross sections from the input data stream (see Section 3.1.2).
( <b>descmacm</b> )	instructions to transfer the macroscopic cross sections from <b>OLDLIB</b> to <b>MACLIB</b> (see Section 3.1.3).

##### 3.1.1 The (**descmac**) input structure for **MAC:**

The (**descmac**) input structure takes the form:

Table 3: Structure (**descmac**)

[ EDIT <i>iprint</i> ]
[ NMIX <i>nmixt</i> ]
[ NIFI <i>nifiss</i> ]
[ ANIS <i>naniso</i> ]

Here

**EDIT** keyword used to modify the print level *iprint*.

*iprint* index used to control the printing in this module. It must be set to 0 if no printing on the output file is required. The macroscopic cross sections can be written to the output file if the variable *iprint* is greater than or equal to 2. The transfer cross sections will be printed if this parameter is greater than or equal to 3. The normalization of the transfer cross sections will be checked if *iprint* is greater than or equal to 5.

**NMIX** keyword used to define the number of material mixtures. This information is required when the number of mixtures on the *MACLIB* is to be increased. When *MACLIB* is in creation mode, one assumes that at least one mixture will be added and *nmixt*=1. When *MACLIB* is in update mode *nmixt* is selected as the maximum mixture number currently stored on *MACLIB*.

*nmixt* the maximum mixtures number (a mixture is characterized by a unique set of macroscopic cross sections) that will be defined in this execution of the **MAC:** module. The value effectively used by DRAGON will be the maximum between *nmixt* and the maximum mixture number defined on *MACLIB*.

**NIFI** keyword used to specify the maximum number of fissile spectrum associated with each mixture. Each fission spectrum generally represents a fissile isotope. This information is required only if *MACLIB* is created and the cross sections are taken from the input data stream.

*nifiss* the maximum number of fissile spectrum per mixture. By default *nifiss*=1.

**ANIS** keyword used to specify the maximum level of anisotropy permitted in the scattering cross sections. This information is required only if *MACLIB* is created and the cross sections are taken directly from the input data stream.

*naniso* number of Legendre orders for the representation of the scattering cross sections. By default *naniso*=1 corresponding to the use of  $P_0$  (isotropic) scattering cross sections. A value of *naniso*=2 indicates that  $P_1$  (linearly anisotropic) scattering cross sections will be provided as input data.

### 3.1.2 The (**descmaci**) input structure for **MAC:**

The (**descmaci**) input structure takes the form:

Table 4: Structure (**descmaci**)

[ NGRO <i>ngroup</i> ]
------------------------

continued on next page

Structure (**descmaci**)

continued from last page

```

[ CTRA { OFF | APOL | WIMS igroup } ]
[ NALBP nalbp ]
[ ALBP (albedp(i),i=1,nalbp) ]
[ WRIT GOXSWN ]
[ ENER (energy(g),g=1,ngroup +1) ]
[ ADD ]
[[ { READ [ (imat(i),i=1,nmixt) ] GOXSRN [ DELE ] | READ INPUT [[ (descxs) ] ] [ (descmpa) ] ] ]
[ NORM ]

```

Here

NGRO	keyword to specify the number of energy groups for which the macroscopic cross sections will be provided. This information is required only if <i>MACLIB</i> is created and the cross sections are taken directly from the input data stream.
<i>ngroup</i>	the number of energy groups used for the calculations in DRAGON. By default <i>ngroup</i> =1.
CTRA	keyword to specify the type of transport correction that should be generated and stored on the MACROLIB. All the modules that will read this MACROLIB will have access this transport correction to produce transport corrected cross sections. By default there is no transport correction when the MACROLIB is created from the input or GOXS files.
OFF	do not use the transport correction ( $\Sigma_{tr,m}^g$ ) stored on the MACROLIB.
ON	use the transport correction ( $\Sigma_{tr,m}^g$ ) stored on the MACROLIB.
APOL	keyword to specify that an APOLLO type transport correction ( $\Sigma_{tr,m}^g$ ) based on the linearly anisotropic scattering cross sections will be computed and used for the total and isotropic scattering cross sections. This correction assumes that the micro-reversibility principle is valid for all energy groups. This option is valid only if the $P_1$ scattering cross sections exist on the MACROLIB.
WIMS	keyword to specify that a WIMS-AECL type transport correction ( $\Sigma_{tr,m}^g$ ) based on the linearly anisotropic scattering cross sections will be computed and used for the total and isotropic scattering cross sections. This correction assumes that the micro-reversibility principle is valid only for groups with an index greater than that specified by the reference group <i>igroup</i> . For the remaining groups a $1/E$ flux spectrum is considered in the evaluation of the transport correction.
<i>igroup</i>	group number with lowest energy limits which will use a $1/E$ flux spectrum. For the WIMS-AECL and WIMS-D4 69 groups libraries, <i>igroup</i> =27 and the micro-reversibility principle is a used only for group 28 to 69.
NALBP	keyword to specify the maximum number of physical albedos that will be read. These can be used by the GEO: module (see Section 3.3).
<i>nalbp</i>	the maximum number of physical albedos. By default <i>nalbp</i> =0.
ALBP	keyword used for the input of the group independent physical albedos array.
<i>albedp</i>	group independent physical albedos array. A maximum of <i>nalbp</i> entries can be specified.
WRIT	keyword used to write cross section data to a GOXS file.

<b>GOXSWN</b>	<code>character*7</code> name of the GOXS file to be created or updated.
<b>ENER</b>	keyword to specify the energy group limits.
<b>energy</b>	energy (eV) array which define the limits of the groups ( <i>ngroup</i> +1 elements). Generally the first element in the array <i>energy</i> is considered to be the highest energy that can be reached by the neutron.
<b>ADD</b>	keyword for adding increments to existing macroscopic cross sections. In this case, the information provided in <b>(descxs)</b> represents incremental rather than standard cross sections.
<b>READ</b>	keyword to specify the input file format. One can use either the input stream (keyword <b>INPUT</b> ) or a GOXS format file.
<b>imat</b>	array of mixture identifiers to be read from a GOXS file. The maximum number of identifiers permitted is <i>nmixt</i> and the maximum value that <i>imat</i> may take is <i>nmixt</i> . When <i>imat</i> is 0, the corresponding mixture on the GOXS file is not included in the MACROLIB. In the cases where <i>imat</i> is absent all the mixtures on the GOXS file are available in a DRAGON execution. They are numbered consecutively starting at 1 or from the last number reached during a previous execution of the <b>MAC :</b> module.
<b>GOXSRN</b>	<code>character*7</code> name of the GOXS file to be read.
<b>DELE</b>	keyword to specify that the GOXS file is deleted after being read.
<b>INPUT</b>	keyword to specify that mixture cross sections will be read on the input stream.
<b>(descxs)</b>	structure describing the format used for reading the mixture cross sections from the input stream (see Section 3.1.4).
<b>(descmpa)</b>	structure describing the format used for reading multigroup physical albedos from the input stream (see Section 3.1.5).
<b>NORM</b>	keyword to specify that the fission spectrum will be normalized. This implies that the fission energy spectrum $\chi_D^g$ that will be stored in the output MACROLIB will satisfy:

$$\sum_{g=1}^G \chi_D^g = 1$$

This option is available even if the mixture cross sections were not read by the **MAC :** module.

### 3.1.3 The **(descmacm)** input structure for **MAC :**

The **(descmacm)** input structure takes the form:

Table 5: Structure **(descmacm)**

```
[ CTRA { OFF | ON } ]
[[ MIX numnew [ numold { UPDL | OLDDL } ] ]]
```

Here

<b>CTRA</b>	keyword to specify the transport correction option. All the modules that will read this MACROLIB will have access this transport correction to produce transport corrected cross sections. By default there is no transport correction when the MACROLIB is created from the input or GOXS files.
<b>OFF</b>	do not use the transport correction ( $\Sigma_{tr,m}^g$ ) stored on the MACROLIB.
<b>ON</b>	use the transport correction ( $\Sigma_{tr,m}^g$ ) stored on the MACROLIB.
<b>MIX</b>	keyword to specify that the macroscopic cross sections associated with a mixture are to be created or updated.
<i>numnew</i>	mixture number to be updated or created on the output MACROLIB.
<i>numold</i>	mixture number on an old MACROLIB or MICROLIB that will be used to update or create <i>numnew</i> on the output MACROLIB.
<b>OLDL</b>	the macroscopic cross sections associated with mixture <i>numold</i> are taken from <i>OLDLIB</i> . This is the default option.
<b>UPDL</b>	the macroscopic cross sections associated with mixture <i>numold</i> are taken from <i>MACLIB</i> .

### 3.1.4 Macroscopic cross section definition

Table 6: Structure (**descxs**)

```

MIX [ matnum ]
  [ EFISS (efiss(i), i=1,nifiss) ]
  [ TOTAL (xssigt(g), g=1,ngroup) ]
  [ TRAN (xssigtr(g), g=1,ngroup) ]
  [ NUSIGF ((xssigf(i,g), g=1,ngroup), i=1,nifiss) ]
  [ NFTOT ((xsfiss(i,g), g=1,ngroup), i=1,nifiss) ]
  [ CHI ((xschi(i,g), g=1,ngroup), i=1,nifiss) ]
  [ FIXE (xsfixe(g), g=1,ngroup) ]
  [ FIXA (xsfixa(g), g=1,ngroup) ]
  [ FIXG (xsfixg(g), g=1,ngroup) ]
  [ SCAT (( nbscat(l,h), ilastg(l,h), (xssc(l,h,g),
    g=1,nbscat(l,h)), h=1,ngroup), l=1,naniso) ]

```

<b>MIX</b>	keyword to specify that the macroscopic cross sections associated with a new mixture are to be read.
<i>matnum</i>	identifier for the next mixture to be read. The maximum value permitted for this identifier is <i>nmixt</i> . When <i>matnum</i> is absent, the mixtures are numbered consecutively starting at 1 or after the last mixture number read either on the GOXS or the input stream.
<b>EFISS</b>	keyword to specify the energy released per fission for each fissile spectrum.

<i>efiss</i>	energy (MeV) released per fission for each fissile spectrum.
<b>TOTAL</b>	keyword to specify that the total macroscopic cross sections for this mixture follows.
<i>xssigt</i>	array of multigroup total macroscopic cross section ( $\Sigma_m^g$ in $\text{cm}^{-1}$ ) associated with mixture $m$ .
<b>TRAN</b>	keyword to specify that the macroscopic cross sections associated with the transport correction for this mixture follows.
<i>xssigr</i>	array of multigroup transport correction macroscopic cross section ( $\Sigma_{tr,m}^g$ in $\text{cm}^{-1}$ ) associated with mixture $m$ .
<b>NUSIGF</b>	keyword to specify that the macroscopic fission cross section multiplied by the average number of neutron per fission for this mixture follows.
<i>xssigf</i>	array of multigroup macroscopic fission cross section multiplied by the average number of neutron per fission ( $\nu\Sigma_{f,i,m}^g$ in $\text{cm}^{-1}$ ) for fissile spectrum $i$ and mixture $m$ .
<b>NFTOT</b>	keyword to specify that the macroscopic fission cross section for this mixture follows.
<i>xsfiiss</i>	array of multigroup macroscopic fission cross section ( $\Sigma_{f,i,m}^g$ in $\text{cm}^{-1}$ ) for fissile spectrum $i$ and mixture $m$ .
<b>CHI</b>	keyword to specify that the fission spectrum for this mixture follows.
<i>xschi</i>	array of multigroup fission spectrum ( $\chi_{I,m}^g$ ) for fissile spectrum $i$ and mixture $m$ .
<b>FIXE</b>	keyword to specify that the fixed neutron source density for this mixture follows.
<i>xsfixe</i>	array of multigroup fixed neutron source density ( $S_m^g$ in $s^{-1}\text{cm}^{-3}$ ) for mixture $m$ .
<b>FIXA</b>	keyword to specify that the adjoint fixed neutron source density for this mixture follows.
<i>xsfixa</i>	array of multigroup adjoint fixed neutron source density ( $S_{A,m}^g$ in $\text{cm}^{-1}$ ) for mixture $m$ .
<b>FIXG</b>	keyword to specify that the fixed generalized adjoint neutron source density for this mixture follows.
<i>xsfixg</i>	array of multigroup generalized adjoint fixed neutron source density ( $S_{G,m}^g$ in $\text{cm}^{-1}$ ) for mixture $m$ .
<b>SCAT</b>	keyword to specify that the macroscopic scattering cross section matrix for this mixture follows.
<i>nbscat</i>	array that defines the number of groups ( $g$ ) for which macroscopic scattering cross section ( $\Sigma_{sl,m}^{g \rightarrow h}$ ) towards the group ( $h$ ) will be provided for each anisotropy level associated with this mixture. We will assume that for the remaining groups, the scattering cross section vanishes.
<i>ilastg</i>	array that defines the group index associated with the most thermal group for which macroscopic scattering cross section towards group $h$ will be provided for each anisotropy level associated with this mixture.
<i>xsscatt</i>	array of multigroup macroscopic scattering cross section ( $\Sigma_{sl,m}^{g \rightarrow h}$ in $\text{cm}^{-1}$ ) from the scattering from group $g$ towards group $h$ . The elements are ordered using decreasing from group number $g=\text{ilastg}$ to $g=(\text{ilastg}-\text{nbscat}+1)$ , and from $h=1$ to $h=G$ . An example of an input structure for macroscopic scattering cross sections can be found in Section 4.1.

### 3.1.5 Multigroup physical albedo definition

Table 7: Structure (**descmpa**)

ALBPG [ <i>ialbp</i> ] ( <i>albp</i> ( <i>g</i> ), <i>g</i> =1, <i>ngroup</i> ) ]
---

**ALBPG** keyword to specify that the multigroup data associated with a physical albedo are to be read.

*ialbp* identifier for physical albedo to be read. The maximum value permitted for this identifier is *nalbp*.

*albp* array of multigroup data associated with physical albedo *ialbp*.

### 3.2 The **LIB:** module

The general format of the input data for the **LIB:** module is the following:

Table 8: First form of the structure (**LIB:**)

<i>MICLIB</i> := <b>LIB:</b> [ <i>MICLIB</i> ] :: ( <b>desclib</b> )
--

Table 9: Second form of the structure (**LIB:**)

<i>MICLIB</i> := <b>LIB:</b> [ <i>MICLIB</i> [ <i>MICOLD</i> ] ] :: ( <b>desclibupd</b> )
---

or

Table 10: Third form of the structure (**LIB:**)

<i>MICLIB</i> := <b>LIB:</b> [ <i>MICLIB</i> [ <i>BRNOLD</i> ] ] :: ( <b>desclibbrn</b> )
---

where

**MICLIB** **character\*12** name of the MICROLIB that will contain the MICROLIB.

**MICOLD** **character\*12** name of a read-only MICROLIB data structure. In the case where a second MICROLIB data structure is provided, the number densities for the isotopes in file *MICLIB* will be replaced selectively by those found in *MICOLD*.

**BRNOLD** **character\*12** name of a read-only BURNUP data structure. In the case where a BURNUP data structure is provided, the number densities for the isotopes in file *MICLIB* will be replaced selectively by those found in *BRNOLD*.

- (**desclib**)            general input structure for this module (see Section 3.2.1).
- (**desclibbrn**)        BURNUP related input structure for this module (see Section 3.2.2).
- (**desclibupd**)        MACROLIB related input structure for this module (see Section 3.2.3).

### 3.2.1 First format for LIB: data input

The general format of (**desclib**) is of the form:

Table 11: Structure (**desclib**)

```
[ EDIT iprint ]
[ MXIS nmisot ]
[ NMIX nmixt ]
[ CTRA { NONE | APOL | WIMS | OLDW } ]
[ ANIS naniso ]
[ PROM ]
[ ADED nedit ( HEDIT(i), i=1,nedit ) ]
[ [ { CDEPCHN | RDEPCHN } ] DEPL { LIB: { DRAGON | WIMS | WIMSAECL | WIMSD4 }
  FIL: NAMEFIL | ndepl (descdepl) } ]
[[ MIXS LIB: { DRAGON | MATXS | MATXS2 | WIMSD4 | WIMS | WIMSAECL | APLIB1 }
  FIL: NAMEFIL [[ (descmix1) ] ] ] ]
```

with

- EDIT**            keyword used to modify the print level *iprint*.
- iprint*            index used to control the printing in this module. It must be set to 0 if no printing on the output file is required while values >0 will increase in steps the amount of information transferred to the output file.
- MXIS**            keyword used to redefine the maximum number of isotopes per mixture.
- nmisot*           the maximum number of isotopes per mixture. By default up to 200 different isotopes per mixture are permitted.
- NMIX**           keyword used to define the number of material mixtures. This data is required if *MICLIB* is created.
- nmixt*           the maximum number of mixtures.
- CTRA**           keyword to specify the type of transport correction that should be generated and stored on the MICROLIB. All the modules that will read this MICROLIB will then have access to transport corrected cross sections. The default is no transport correction.
- NONE**           keyword to specify that no transport correction should be used in this calculation.

APOL	keyword to specify that an APOLLO type transport correction based on the linearly anisotropic scattering cross sections is to be used for the total and isotropic scattering cross sections. This correction assumes that the micro-reversibility principle is valid for all energy groups. This type of correction implies that the $P_1$ scattering cross sections must be present on the original library.
OLDW	keyword to specify that a WIMS type transport correction based on the linearly anisotropic scattering cross sections is to be used for the total and isotropic scattering cross sections. This correction assumes that the micro-reversibility principle is valid only for groups energies less than 4.0 eV. For the remaining groups a $1/E$ flux spectrum is considered in the evaluation of the transport correction. In addition for WIMSD4 and WIMSAECL libraries, linearly anisotropic diagonal scattering cross sections are generated in the cases where the transport correction differs from 0.0 while no anisotropic scattering cross sections is provided on the library. This option was inserted for compatibility with the WIMS transport correction of older versions of DRAGON.
WIMS	keyword to specify that the transport correction is to be used for the total and isotropic scattering cross sections. This type of correction uses directly the transport correction cross sections provided on the original library. Such information is available only in WIMSD4 and WIMSAECL format libraries. In the case where a library of another type is considered, this correction is identical to the OLDW option described above.
ANIS	keyword to specify the maximum level of anisotropy for the scattering cross sections.
naniso	number of Legendre orders for the representation of the scattering cross sections. Isotropic scattering is represented by <i>naniso</i> =1 while <i>naniso</i> =2 represents linearly anisotropic scattering. The linearly anisotropic scattering contributions are generally taken into account via the transport correction (see CTRA keyword) in the transport calculation. For $B_1$ or $P_1$ leakage calculations, the linearly anisotropic scattering cross sections are taken into account explicitly. The default value is <i>naniso</i> =2.
PROM	keyword to specify that prompt neutron are to be considered for the calculation of the fission spectrum. By default, the contribution due to delayed neutron is considered. This option is only compatible with a MATXS or MATXS2 format library.
ADED	keyword to specify the input of additional cross sections to be treated by DRAGON. These cross sections are not needed to solve the transport equation but are recognized by the EDI : module.
nedit	number of types of additional cross sections.
HEDIT	<p>character*6 name of an additional cross-section type. This name also corresponds to vector reactions in a MATXS and MATXS2 format library not automatically recognized by DRAGON. For example:</p> <p>NWT0/NWT1=<math>P_0/P_1</math> library weight functions.  NTOT0/NTOT1=<math>P_0/P_1</math> neutron total cross sections.  NELAS=Neutron elastic scattering cross sections (MT=2).  NINEL=Neutron inelastic scattering cross sections (MT=4).  NG=Neutron capture cross sections (MT=102).  NUDEL=Number of delayed secondary neutron (Nu-D / MT=455).  NFSLO=<math>\nu</math>*slow fission cross section.  NHEAT=Heat production cross section.  CHIS/CHID=Slow/delayed fission spectrum.  NF/NNF/N2NF/N3NF=<math>\nu</math>*partial fission cross sections (MT=19, 20, 21 and 38).  N2N/N3N/N4N=(n,2n), (n,3n), (n,4n) cross sections (MT=16, 17 and 37).  NP/NA=(n,p) and (n,<math>\alpha</math>) transmutation cross sections (MT=103 and 107).</p> <p>By default, DRAGON will always attempt to recover the additional cross sections NG, and NHEAT since they may be required for the depletion calculations.</p>

<b>CDEPCHN</b>	keyword to specify that a complete depletion chain is to be considered. As a result the isotopes in a depletion chain (specified by keyword <b>DEPL</b> ) not present in a mixture containing burnup material will be added automatically with 0.0 concentrations. This is the default option when the keyword <b>DEPL</b> is activated.
<b>RDEPCHN</b>	keyword to specify that a reduced depletion chain is to be considered. As a result the isotopes in a depletion chain (specified by keyword <b>DEPL</b> ) not present in a mixture containing burnup material will not be added automatically.
<b>DEPL</b>	keyword to specify that the isotopic depletion (burnup) chain is to be read. For a given <b>LIB:</b> execution only one isotopic depletion chain can be read.
<b>MIXS</b>	keyword to specify that the mixture description is to be read. For a given <b>LIB:</b> execution more than one cross-section library can be read.
<b>LIB:</b>	keyword to specify the type of library from which the isotopic depletion chain or microscopic cross section is to be read. It is optional when preceded by the keyword <b>DEPL</b> in which case the isotopic depletion chain is read from the standard input file.
<b>DRAGON</b>	keyword to specify that the isotopic depletion chain or the microscopic cross sections are in the DRAGLIB format. <sup>[24]</sup>
<b>MATXS</b>	keyword to specify that the microscopic cross sections are in the MATXS format of NJOY-II and NJOY-89 (no depletion data available for libraries using this format).
<b>MATXS2</b>	keyword to specify that the microscopic cross sections are in the MATXS format of NJOY-91 (no depletion data available for libraries using this format).
<b>WIMSD4</b>	keyword to specify that the isotopic depletion chain or the microscopic cross sections are in the WIMS-D4 format.
<b>WIMS</b>	keyword to specify that the isotopic depletion chain or the microscopic cross sections are in the WIMS-AECL format.
<b>WIMSAECL</b>	keyword to specify that the isotopic depletion chain or the microscopic cross sections are in the WIMS-AECL format.
<b>FIL:</b>	keyword to specify the name of the file from which the isotopic depletion chain or microscopic cross section is to be read.
<b>NAMEFIL</b>	character*8 of the library where the isotopic depletion chain or the microscopic cross sections are stored.
<i>ndepl</i>	number of isotopes in the depleting chain.
<b>(descdepl)</b>	input structure describing the depletion chain (see Section 3.2.4).
<b>(descmix1)</b>	input structure describing the isotopic and physical properties of a given mixture (see Section 3.2.5).

### 3.2.2 Second format for **LIB:** data input

The general format of **(desclibbrn)** is of the form:

Table 12: Structure (**desclibbrn**)

```
[ EDIT iprint ]
BURN { iburn | tburn } [[ (descmix2) ]]
```

with

<b>EDIT</b>	keyword used to modify the print level <i>iprint</i> .
<i>iprint</i>	index used to control the printing in this module. It must be set to 0 if no printing on the output file is required while values >0 will increase in steps the amount of information transferred to the output file.
<b>BURN</b>	keyword to specify that the mixture density on <i>MICLIB</i> are to be updated using information taken from <i>BRNOLD</i> . If ( <b>descmix2</b> ) is absent, a direct one to one correspondence between the isotope on <i>BRNOLD</i> and <i>MICLIB</i> is assumed. If ( <b>descmix2</b> ) is present, only the mixture specified by ( <b>descmix2</b> ) are updated using information from <i>BRNOLD</i> .
<i>iburn</i>	burnup step selected on <i>BRNOLD</i> . This step must be present on the burnup file.
<i>tburn</i>	burnup time in days on <i>BRNOLD</i> . This time step must be present on the burnup file.
<b>(descmix2)</b>	input structure describing perturbations to the isotopic and physical properties of a given mixture (see Section 3.2.6).

### 3.2.3 Third format for LIB: data input

The general format of (**desclibupd**) is of the form:

Table 13: Structure (**desclibupd**)

```
[ EDIT iprint ]
MAXS [[ (descmix3) ]]
```

with

<b>EDIT</b>	keyword used to modify the print level <i>iprint</i> .
<i>iprint</i>	index used to control the printing in this module. It must be set to 0 if no printing on the output file is required while values >0 will increase in steps the amount of information transferred to the output file.
<b>MAXS</b>	keyword to specify that the mixture density on <i>MICLIB</i> are to be modified. If <i>MACOLD</i> is present and ( <b>descmix3</b> ) is absent, a direct one to one correspondence between the isotope on both libraries is assumed. If <i>MICOLD</i> and ( <b>descmix3</b> ) are present, only the mixture on the library file specified by ( <b>descmix3</b> ) are updated using information from the <i>MICOLD</i> . If <i>MICOLD</i> is

absent and **(descmix3)** is present, only the mixture on *MICLIB* specified by **(descmix3)** are updated.

**(descmix3)** input structure describing perturbations to the isotopic and physical properties of a given mixture (see Section 3.2.7).

### 3.2.4 Depletion data structure

The structure **(descdepl)** describes the radioactive decay and neutron activation chain to be used in the isotopic depletion calculation.

Table 14: Structure **(descdepl)**

```
CHAIN
[[ NAMDPL [ izeae ]
  [[ { DECAY dcr |
      reaction [ energy ] } ]]
  [ { STABLE |
      FROM [[ { DECAY | reaction } [[ yield NAMPAR ]] ] ] ] ] ] ]
ENDCHAIN
```

with:

<b>CHAIN</b>	keyword to specify the beginning of the depletion chain.
<b>NAMDPL</b>	<b>character*12</b> name of an isotope (or isomer) of the depletion chain that appears in the cross-section library.
<b>izeae</b>	six digit integer representing the isotope. The first two digits represent the atomic number of the isotope; the next three indicate its mass number and the last digit indicates the excitation level of the nucleus (0 for a nucleus in its ground state, 1 for an isomer in its first excited state, etc.). For example, $^{238}\text{U}$ in its ground state will be represented by <b>izeae=922380</b> .
<b>STABLE</b>	non depleting isotope.
<b>DECAY</b>	indicates that a decay reaction takes place either for production of this isotope or its depletion.
<b>dcr</b>	radioactive decay constant (in $10^{-8} \text{ s}^{-1}$ ) of the isotope. By default, <b>dcr=0.0</b> .
<b>reaction</b>	<b>character*6</b> identification of a neutron-induced reaction that takes place either for production of this isotope, its depletion, or for producing energy. Example of reactions are following:
<b>NG</b>	indicates that a radiative capture reaction takes place either for production of this isotope, its depletion or for producing energy.
<b>N2N</b>	indicates that the following reaction is taking place: ${}_0^1n + {}_Z^A\text{X} \rightarrow {}_0^1n + {}_Z^{A-1}\text{X}$
<b>N3N</b>	indicates that the following reaction is taking place: ${}_0^1n + {}_Z^A\text{X} \rightarrow {}_0^3n + {}_Z^{A-2}\text{X}$

N4N	indicates that the following reaction is taking place:
	${}_0^1n + {}_Z^AX \rightarrow 4{}_0^1n + {}_Z^{A-3}X$
NP	indicates that the following reaction is taking place:
	${}_0^1n + {}_Z^AX \rightarrow {}_1^1p + {}_{Z-1}^{A-1}Y$
NA	indicates that the following reaction is taking place:
	${}_0^1n + {}_Z^AX \rightarrow {}_2^4He + {}_{Z-2}^{A-3}Y$
NFTOT	indicates that a fission is taking place.
energy	energy (in MeV) recoverable per neutron-induced reaction of type <i>reaction</i> . If the energy associated to radiative capture is not explicitly given, it should be added to the energy released per fission. By default, <i>energy</i> =0.0 MeV.
STABLE	non depleting isotope. Such an isotope may produces energy by neutron-induced reactions (such as radiative capture).
FROM	indicates that this isotope is produced from decay or neutron-induced reactions.
yield	production yield for fission (expressed in %) or for other reaction (given in absolute value).
NAMPAR	character*12 name of the parent isotope (or isomer) that appears in the cross-section library.
ENDCHAIN	keyword to specify the end of the depletion chain.

### 3.2.5 Format for (**descmix1**)

The structure (**descmix1**) is used to describe the isotopic composition and the physical properties, such as the temperature and density, of a mixture.

Table 15: Structure (**descmix1**)

```

MIX [ matnum ] {
    [temp [ denmix ] ]
    [[ [ NAMALI = ] NAMISO dens [ { dil | INF } ]
      [ inrs ] [ DBYE tempd ] [ SHIB NAMS ] [ THER ntfg HINC [ TCOH HCOH ] ] [ NOEV ] ] ] |
    COMB [[ mati relvol ] ] }

```

where:

MIX	keyword to specify the number identifying the mixture to be read.
matnum	mixture identifier. The maximum value that <i>matnum</i> may have is <i>nmixt</i> . When <i>matnum</i> is absent, the mixtures are numbered successively starting from 1 if no mixture has yet been specified or from the last mixture number specified + 1.

<i>temp</i>	absolute temperature (in Kelvin) of the isotopic mixture. It is optional only when this mixture is to be updated. Otherwise, the old temperature associated with the mixture is used.
<i>denmix</i>	mixture density in $g\ cm^{-3}$ .
<i>NAMALI</i>	<code>character*8</code> alias name for an isotope to be used locally. When the alias name is absent, the isotope name used locally is identical to the isotope name on the library.
<code>=</code>	keyword to specify to which isotope in a library is associated the previous alias name.
<i>NAMISO</i>	<code>character*12</code> name of an isotope present in the library which is included in this mixture.
<i>dens</i>	isotopic concentration of the isotope <i>NAMISO</i> in the current mixture in $10^{24}cm^{-3}$ . When the mixture density <i>denmix</i> is specified, the relative weight percentage of each of the isotopes in this mixture is to be provided.
<i>dil</i>	group independent microscopic dilution cross section (in barns) of the isotope <i>NAMISO</i> in this mixture. It is possible to recalculate a group dependent dilution for an isotope by the use of the <b>SHI :</b> module (see Section 3.5). In this case, the dilution is only used as a starting point for the self-shielding iterations and has no effect on the final result. If the dilution is not given or is larger than an $10^{10}$ barns, an infinite dilution is assumed.
<b>INF</b>	keyword to specify that an infinite dilution ( $10^{10}$ barns) is to be associated with this isotope. This value implies that the isotope is present in trace amounts only.
<i>inrs</i>	number of the resonant region associated with this isotope. By default <i>inrs</i> =0 and the isotope is not a candidate for self-shielding. When <i>inrs</i> ≠0, the isotope can be self-shielded using the <b>SHI :</b> module (see Section 3.5) where it is assumed that a given isotope distributed with different concentrations in a number of mixtures and having the same value of <i>inrs</i> will share the same fine flux. This approximation is similar to the PIC approximation of Livolant-Jeanpierre. Should one wish to self-shield both the fuel sheaths and the fuel it is important to assign a different <i>inrs</i> number to each. If a single type of fuel is located in different mixture in <i>onion-peel fashion</i> , it is necessary to attribute a single <i>inrs</i> value to this fuel.
<b>DBYE</b>	keyword to specify that the absolute temperature of the isotope is different from that of the isotopic mixture. This option is useful to define Debye-corrected temperature.
<i>tempd</i>	absolute temperature (in Kelvin) of the isotope. By default <i>tempd</i> = <i>temp</i> .
<b>SHIB</b>	keyword to specify that the name of the isotope containing the information related to the self-shielding is different from the initial name of the isotope.
<i>NAMS</i>	<code>character*12</code> name of a record in the library containing the self-shielding data. This name is required if the dilution is not infinite or a non zero resonant region is associated with this isotope and <i>NAMS</i> is different from <i>NAMISO</i> .
<b>THER</b>	keyword to specify that the thermalization effects are to be included with the cross sections when using a <b>MATXS</b> or <b>MATXS2</b> format library.
<i>HINC</i>	<code>character*6</code> name of the incoherent thermalization effects which will be taken into account. The incoherent effects are those that may be described by the $S(\alpha, \beta)$ scattering law. The value <b>FREE</b> is used to simulate the effects of a gas.
<b>TCOH</b>	keyword to specify that coherent thermalization effects will be taken into account.
<i>HCOH</i>	<code>character*6</code> name of the coherent thermalization effects which will be taken into account. The coherent effects are the <i>vector reactions</i> in the <b>MATXS</b> or <b>MATXS2</b> format library where the name is terminated by the \$ suffix. They are generally available for graphite, beryllium, beryllium oxide, polyethylene and zirconium hydroxide.

<i>ntfg</i>	number of energy groups that will be affected by the thermalization effects.
<i>NOEV</i>	keyword to force a mixture or a nuclide to be non-depleting (even in cases where it is potentially depleting). Note that the mixture or nuclide keeps its capability to produce energy. By default, the depleting isotopes are automatically regognized as depleting.
<i>COMB</i>	keyword to specify that this mixture represents a combination of previously defined mixtures.
<i>mati</i>	number associated with a previously defined mixture. In order to insert some void in a mixture use <i>mati</i> =0. If the mixture is not already defined one assumes that it represents a voided mixture.
<i>relvol</i>	relative volume $V_m$ occupied by mixture $m=mati$ in <i>matnum</i> . Two cases can be considered, namely that where the density $\rho_m$ of each mixture <i>mati</i> is provided along with the weight percent for each isotopes $J$ ( $W_m^J$ ) and the case where the explicit concentration $N_m^J$ of each isotope in a <i>mati</i> was provided (it is forbidden to combined two mixtures with different isotopic content description). In the case where the initial mixtures are defined using densities $\rho_m$ , the density ( $\rho_k$ ) and volume ( $V_k$ ) of the final mixture will become:

$$V_k = \sum_m V_m$$

$$\rho_k = \frac{1}{V_k} \sum_m \rho_m V_m$$

and the weight percent will be changed in a consistent way, namely

$$W_{k,J} = \frac{\rho_m V_m W_{m,J}}{\rho_k V_k}$$

When the explicit concentration are given we will use:

$$N_{k,J} = \frac{V_m N_{m,J}}{V_k}$$

Note that in the structure (**descmix1**) one only needs to describe the isotopes initially present in each mixture. DRAGON will then automatically associate with each depleting mixture the additional isotopes required by the available burnup chain. Moreover, the microscopic cross-section library associated with these new isotopes will be the same as that of their parent isotope. For example, suppose that mixture 1 contains isotope U235 which is to be read on the DRAGON format library associated with file DRAGLIB. Also assume that the depletion chain, which is written on the WIMS-AECL format library associated with file WIMSLIB, states that isotope U236 (initially absent in the mixture) can be generated from U235 by neutron capture. Then, one can either specify explicitly from which library file the microscopic cross sections associated with isotope U236 (zero concentration) are to be read, or omit U236 from the mixture description in which case DRAGON will assume that the microscopic cross sections associated with isotope U236 are to be read from the same library as the cross section for isotope U235. Note that the isotopes added automatically will remain at infinite dilution.

### 3.2.6 Format for (**descmix2**)

The structure (**descmix2**) is used to describe the modifications in the isotopic composition of a mixture taken from a BURNUP data structure.

Table 16: Structure (**descmix2**)

MIX matnum [matold ] [ NAMALI dens ]
--------------------------------------

where:

<b>MIX</b>	keyword to specify the number identifying the next mixture to be updated. If no mixture is specified then all the mixtures are updated.
<i>matnum</i>	mixture identifier on <i>MICLIB</i> .
<i>matold</i>	mixture identifier on <i>BRNOLD</i> . When <i>matold</i> is not specified this mixture is not updated.
<i>NAMALI</i>	<code>character*8</code> alias name for an isotope on <i>MICLIB</i> to be modified.
<i>dens</i>	isotopic concentration of the isotope <i>NAMISO</i> in the current mixture in $10^{24}\text{cm}^{-3}$ . When $\text{dens} \geq 0$ , the isotopic concentration for this isotope becomes <i>dens</i> , while all the other isotopes take the value specified on <i>BRNOLD</i> . When $\text{dens} = -1.0$ , the isotopic concentration of this isotope is not updated.

### 3.2.7 Format for (**descmix3**)

The structure (**descmix3**) is used to describe the modifications in the isotopic composition of a mixture taken from an old MICROLIB data structure.

Table 17: Structure (**descmix3**)

MIX matnum [matold ] [ relden ] [ NAMALI dens ]
---

where:

<b>MIX</b>	keyword to specify the number identifying the next mixture to be updated. If no mixture is specified then all the mixtures are updated.
<i>matnum</i>	mixture identifier on <i>MICLIB</i> .
<i>matold</i>	mixture identifier on <i>MICOLD</i> . When <i>matold</i> is not specified this mixture is not updated.
<i>relden</i>	relative density of updated mixture. The concentration of each isotope in the mixture will be multiplied by this factor independent of the fact that the original concentrations were defined in <i>MICLIB</i> , <i>MICOLD</i> or is specified explicitly using <i>dens</i> .
<i>NAMALI</i>	<code>character*8</code> alias name for an isotope on <i>MICLIB</i> to be modified.
<i>dens</i>	isotopic concentration of the isotope <i>NAMISO</i> in the current mixture in $10^{24}\text{cm}^{-3}$ . When $\text{dens} \geq 0$ , the isotopic concentration for this isotope becomes $\text{dens} \times \text{relden}$ , while all the other isotopes are multiplied by <i>relden</i> only. When $\text{dens} = -1.0$ , the isotopic concentration of this isotope is not updated while all the other isotopes are multiplied by <i>relden</i> .

### 3.3 The GEO: module

The **GEO:** module is used to create or modify a geometry. All the characteristics (dimensions, region contents and boundary conditions) of a simple or complex geometry will be specified using this module of DRAGON. The specifications of the geometry are independent of the tracking module to be used subsequently in DRAGON. Each geometry is stored in a GEOMETRY data structure under its given name. Once a geometry has been specified, it can be easily modified using the **GEO:** module again on the geometry. The calling specifications for the **GEO:** module are:

Table 18: Structure (**GEO:**)

**GEONAM** := **GEO:** :: (**descgtyp**)  
(**descgcnt**)

to create a new geometry or

Table 19: Structure (**GEO:**)

**GEONAM** := **GEO:** { *GEONAM* | *OLDGEO* } ::  
(**descgcnt**)

to import and modify an old geometry. Here

<b>GEONAM</b>	<b>character*12</b> name of the GEOMETRY created or modified.
<b>OLDGEO</b>	<b>character*12</b> name of a read-only GEOMETRY. The type and all the characteristics of <i>OLDGEO</i> will be copied onto <i>GEONAM</i> before this later geometry is modified.
( <b>descgtyp</b> )	structure describing the geometry type of <i>GEONAM</i> (see Section 3.3.1).
( <b>descgcnt</b> )	structure describing the characteristics of a geometry (see Section 3.3.1).

#### 3.3.1 Geometry types

Structures (**descgtyp**) and (**descgcnt**) are used to define respectively the type of geometry that will be define and the contents of this geometry (dimensions, materials, boundary conditions). The module **GEO:** can be recursively called from (**descgcnt**) as an embedded module, in order to define sub-geometries:

Table 20: Structure (**descgtyp**)

{ **VIRTUAL** | **HOMOGE** | **SPHERE** *lr* |

continued on next page

Structure (**descgtyp**)

continued from last page

```

CAR1D lx | CAR2D lx ly | CAR3D lx ly lz |
HEX lh | HEXZ lh lz |
TUBE lr [ lx ly ] | TUBEX lr { lx | lx ly lz } | TUBEY lr { ly | lx ly lz } | TUBEZ lr { lz | lx ly lz } |
CARCEL lr [ lx ly ] | CARCELX lr { lx | lx ly lz } |
CARCELY lr { ly | lx ly lz } | CARCELZ lr { lz | lx ly lz } |
HEXCEL lr | HEXCELZ lr lz |
GROUP lp }

```

Table 21: Structure (**descgcnt**)

```

[ EDIT iprint ]
(descBC)
(descSP)
(descPP)
(descNSG)
[[ :: SUBGEO := GEO: { (descgtyp) | SUBGEO | OLDGEO } (descgcnt) ; ]]

```

where

VIRTUAL	keyword to specify that a virtual geometry description follows. This type of geometry is used to complete an assembly that has irregular boundaries.
HOMOGE	keyword to specify that a infinite homogeneous geometry description follows.
SPHERE	keyword to specify that a spherical geometry (concentric spheres) description follows.
CAR1D	keyword to specify that a one dimensional plane geometry (infinite slab) description follows.
CAR2D	keyword to specify that a two dimensional Cartesian geometry description follows.
CAR3D	keyword to specify that a three dimensional Cartesian geometry description follows.
HEX	keyword to specify that a two dimensional hexagonal geometry description follows.
HEXZ	keyword to specify that a three dimensional hexagonal geometry description follows.
TUBE	keyword to specify that a cylindrical geometry (infinite tubes or cylinders) description follows. This geometry can contain an imbedded $X - Y$ Cartesian mesh.
TUBEX	keyword to specify that a polar geometry ( $R - X$ ) description follows. This geometry can contain an imbedded $Y - Z$ Cartesian mesh.
TUBEY	keyword to specify that a polar geometry ( $R - Y$ ) description follows. This geometry can contain an imbedded $Z - X$ Cartesian mesh.
TUBEZ	keyword to specify that a polar geometry ( $R - Z$ ) description follows. This geometry can contain an imbedded $X - Y$ Cartesian mesh.

CARCEL	keyword to specify that a two dimensional mixed Cartesian cell (concentric tubes surrounded by a rectangle) description follows.
CARCELX	keyword to specify that a three dimensional mixed Cartesian cell with tubes oriented along the $X$ -axis description follows.
CARCELY	keyword to specify that a three dimensional mixed Cartesian cell with tubes oriented along the $Y$ -axis description follows.
CARCELZ	keyword to specify that a three dimensional mixed Cartesian cell with tubes oriented along the $Z$ -axis description follows.
HEXCEL	keyword to specify that a two dimensional mixed hexagonal cell (concentric tubes surrounded by a hexagon) description follows.
HEXCELZ	keyword to specify that a three dimensional mixed hexagonal cell with tubes oriented along the $Z$ -axis description follows.
GROUP	keyword to specify that a <i>do-it-yourself</i> type geometry description follows.
$lx$	number of subdivisions along the $X$ -axis (before mesh splitting).
$ly$	number of subdivisions along the $Y$ -axis (before mesh splitting).
$lz$	number of subdivisions along the $Z$ -axis (before mesh splitting).
$lr$	number of cylinders or spherical shells (before mesh splitting).
$lh$	number of hexagon in an axial plane (including the virtual hexagon).
$lp$	number of types of cells (number of cells inside which a distinct flux will be calculated).
EDIT	keyword used to modify the print level <i>iprint</i> .
<i>iprint</i>	index used to control the printing in this module. It must be set to 0 if no printing on the output file is required, to 1 for minimum printing (fixed default value) and to 2 for printing the geometry state vector.
(descBC)	structure defining the boundary conditions associated with a geometry (see Section 3.3.2).
(descSP)	structure defining the spatial coordinates associated with a geometry (see Section 3.3.3).
(descPP)	structure defining the physical properties associated with a geometry (see Section 3.3.4).
(descNSG)	structure used to specify the properties of non standard geometries (see Section 3.3.5).
SUBGEO	character*12 name of the directory that will contain the sub-geometry.
OLDGEO	character*12 name of a parallel directory containing an existing sub-geometry. The type and all the characteristics of <i>OLDGEO</i> will be copied onto <i>SUBGEO</i> .

### 3.3.2 Boundary conditions

The data corresponding to the (descBC) structure is:

Table 22: Structure (**descBC**)

```

[ X- { VOID | REFL | SSYM | TRAN | SYME | ALBE { albedo | icode } | DIAG } ]
[ X+ { VOID | REFL | SSYM | TRAN | SYME | ALBE { albedo | icode } | DIAG } ]
[ Y- { VOID | REFL | SSYM | TRAN | SYME | ALBE { albedo | icode } | DIAG } ]
[ Y+ { VOID | REFL | SSYM | TRAN | SYME | ALBE { albedo | icode } | DIAG } ]
[ Z- { VOID | REFL | SSYM | TRAN | SYME | ALBE { albedo | icode } } ]
[ Z+ { VOID | REFL | SSYM | TRAN | SYME | ALBE { albedo | icode } } ]
[ R+ { VOID | REFL | ALBE { albedo | icode } } ]
[ HBC { S30 | SA60 | SB60 | S90 | R120 | R180 | SA180 | SB180 | COMPLETE }
{ VOID | REFL | SYME | ALBE { albedo | icode } } ]

```

where:

<b>X-</b>	keyword to specify the boundary conditions associated with the negative $X$ surface in a Cartesian geometry.
<b>X+</b>	keyword to specify the boundary conditions associated with the positive $X$ surface in a Cartesian geometry.
<b>Y-</b>	keyword to specify the boundary conditions associated with the negative $Y$ surface in a Cartesian geometry.
<b>Y+</b>	keyword to specify the boundary conditions associated with the positive $Y$ surface in a Cartesian geometry.
<b>Z-</b>	keyword to specify the boundary conditions associated with the negative $Z$ surface in a Cartesian geometry.
<b>Z+</b>	keyword to specify the boundary conditions associated with the positive $Z$ surface in a Cartesian geometry.
<b>R+</b>	keyword to specify the boundary conditions associated with the outer surface of a cylindrical or spherical geometry.
<b>VOID</b>	keyword to specify that the surface under consideration has zero reentrant angular flux.
<b>REFL</b>	keyword to specify that the surface under consideration has a reflective boundary condition. In most DRAGON calculations, this implies white boundary conditions. The main exception to this rule is when cyclic tracking in 2-D is considered and mirror like reflections are considered. In DRAGON the cell is never unfolded to take into account a REFL boundary condition.
<b>SSYM</b>	keyword to specify that the surface under consideration has a reflective boundary condition. The main difference between REFL and SSYM is that for SSYM the cell is always unfolded to take into account the reflection at the boundary. Accordingly, SSYM implies the use of a mirror like reflection.
<b>TRAN</b>	keyword to specify that periodic boundary conditions are considered. The surface under consideration is therefore connected to the opposite surface in the Cartesian domain. The only combinations of periodic boundary conditions permitted are:

- Periodicity along the  $X$ -axis

X- TRAN X+ TRAN

- Periodicity along the  $Y$ -axis

Y- TRAN Y+ TRAN

- Periodicity along the  $Z$ -axis

Z- TRAN Z+ TRAN

**SYME** keyword to specify that the Cartesian surface under consideration is virtual and that a reflection symmetry is associated with the axis running through the center of the cells closest to this surface.

**DIAG** keyword to specify that the Cartesian surface under consideration has the same properties as that associated with a diagonal through the geometry. Note that two and only two **DIAG** surfaces must be specified. The diagonal symmetry is only permitted for square geometry and in the following combinations:

X+ DIAG Y- DIAG

or

X- DIAG Y+ DIAG

**ALBE** keyword to specify that the surface under consideration has an arbitrary albedo. In most DRAGON calculations, this implies white boundary conditions. The main exception to this rule is when cyclic tracking in 2-D is considered and mirror like reflections are considered. In DRAGON the cell is never unfolded to take into account a **ALBE** boundary condition.

*albedo* geometric albedo corresponding to the boundary condition **ALBE** (*albedo*>0.0).

*icode* index of a physical albedo corresponding to the boundary condition **ALBE**. The numerical values of the physical albedo are supplied by the module **MAC** : (see Section 3.1).

**HBC** keyword to specify the boundary conditions associated with the outer surface of an hexagonal geometry.

**S30** keyword to specify an hexagonal symmetry of one twelfth of an assembly (see Figure 1).

**SA60** keyword to specify an hexagonal symmetry of one sixth of an assembly of type A (see Figure 1).

**SB60** keyword to specify an hexagonal symmetry of one sixth of an assembly of type B (see Figure 2).

**S90** keyword to specify an hexagonal symmetry of one quarter of an assembly (see Figure 2).

**R120** keyword to specify a rotation symmetry of one third of an assembly (see Figure 3).

**R180** keyword to specify a rotation symmetry of a half assembly (see Figure 3).

**SA180** keyword to specify an hexagonal symmetry of half a type A assembly (see Figure 4).

**SB180** keyword to specify an hexagonal symmetry of half a type B assembly (see Figure 5).

**COMPLETE** keyword to specify a complete hexagonal assembly (see figure Figure 6).

### 3.3.3 Spatial description of geometry

The (**descSP**) structure has the following contents:

Table 23: Structure (**descSP**)

```

[ MESHX (xxx(i), i=1,lx+1) ]
[ SPLITX (ispltx(i), i=1,lx) ]
[ MESHY (yyy(i), i=1,ly+1) ]
[ SPLITY (isply(i), i=1,ly) ]
[ MESHZ (zzz(i), i=1,lz+1) ]
[ SPLITZ (ispltz(i), i=1,lz) ]
[ RADIUS (rrr(i), i=1,lr+1) ]
[ OFFCENTER (disxyz(i), i=1,3) ]
[ SPLITR (isplr(i), i=1,lr) ]
[ SIDE sidhex ]
[ NPIN npins ]
[ RPIN { rpins | (rpins(i), i=1, npins) } ]
[ APIN { apins | (apins(i), i=1, npins) } ]

```

<b>MESHX</b>	keyword to specify the spatial mesh defining the regions along the $X$ –axis.
<i>xxx</i>	array giving the $X$ limits (cm) of the regions making up the geometry. These values must be given in order, from $X-$ to $X+$ . If the geometry presents a diagonal symmetry the same data is also used along the $Y$ –axis.
<b>SPLITX</b>	keyword to specify that a mesh splitting of the geometry along the $X$ –axis is to be performed.
<i>ispltx</i>	array giving the number of zones that will be considered for each region along the $X$ –axis. If the geometry presents a diagonal symmetry this information is also used for the splitting along the $Y$ –axis. By default, <i>ispltx</i> =1.
<b>MESHY</b>	keyword to specify the spatial mesh defining the regions along the $Y$ –axis.
<i>yyy</i>	array giving the $Y$ limits (cm) of the regions making up the geometry. These values must be given in order, from $Y-$ to $Y+$ .
<b>SPLITY</b>	keyword to specify that a mesh splitting of the geometry along the $Y$ –axis is to be performed.
<i>isply</i>	array giving the number of zones that will be considered for each region along the $Y$ –axis. By default, <i>isply</i> =1 unless a diagonal symmetry is used in which case <i>isply</i> = <i>ispltx</i> .
<b>MESHZ</b>	keyword to specify the spatial mesh defining the regions along the $Z$ –axis.
<i>zzz</i>	array giving the $Z$ limits (cm) of the regions making up the geometry. These values must be given in order, from $Z-$ to $Z+$ .
<b>SPLITZ</b>	keyword to specify that a mesh splitting of the geometry along the $Z$ –axis is to be performed.
<i>ispltz</i>	array giving the number of zones that will be considered for each region along the $Z$ –axis. By default, <i>ispltz</i> =1.
<b>RADIUS</b>	keyword to specify the spatial mesh along the radial direction.
<i>rrr</i>	array giving the radial limits (cm) of the annular regions (cylindrical or spherical) making up the geometry. It is important to note that we must have <i>rrr</i> (1)=0.0.

<b>OFFCENTER</b>	keyword to specify that the concentric annular regions in a <b>CARCEL</b> , <b>CARCELX</b> , <b>CARCELY</b> , <b>CARCELZ</b> , <b>TUBE</b> , <b>TUBEX</b> , <b>TUBEY</b> and <b>TUBEZ</b> geometry can now be displaced with respect to the center of the Cartesian mesh. This option will only be treated when the <b>EXCELT:</b> , <b>NXT:</b> and <b>EXCELL:</b> modules are used.
<i>disxyz</i>	array giving the $x$ ( <i>disxyz(1)</i> ), $y$ ( <i>disxyz(2)</i> ) and $z$ ( <i>disxyz(3)</i> ) displacement (cm) of the concentric annular regions with respect to the center of the Cartesian mesh.
<b>SPLITR</b>	keyword to specify that a mesh splitting of the geometry along the radial direction is to be performed.
<i>ispltr</i>	array giving the number of zones that will be considered for each region along the radial axis. A negative value results in a splitting of the regions into zones of equal volumes; a positive value results in a uniform splitting along the radial direction. By default, <i>ispltr</i> =1.
<b>SIDE</b>	keyword to specify the length of a side of a hexagon.
<i>sidhex</i>	length of a side of a hexagon (cm).
<b>NPIN</b>	keyword to specify the number of pins located in a cluster geometry. It can only be used for <b>TUBE</b> , <b>TUBEX</b> , <b>TUBEY</b> and <b>TUBEZ</b> sub-geometry.
<i>npins</i>	the number of pins associated with this sub-geometry in the primary geometry.
<b>RPIN</b>	keyword to specify the radius of an imaginary cylinder where the centers of the pins are to be placed in a cluster geometry. It can only be used for <b>TUBE</b> , <b>TUBEX</b> , <b>TUBEY</b> and <b>TUBEZ</b> sub-geometry.
<i>rpins</i>	the radius (cm) of an imaginary cylinder where the centers of the pins are to be placed.
<b>APIN</b>	keyword to specify the angle of the first pin centered on an imaginary cylinder in a cluster geometry. It can only be used for <b>TUBE</b> , <b>TUBEX</b> , <b>TUBEY</b> and <b>TUBEZ</b> sub-geometry.
<i>apins</i>	the angle (radian) of the first pin in the ring or the angle of each pins in the ring.

The user should be warned that the maximum number of zones resulting from the above description of a geometry  $L_t$  should not exceed the limits imposed by *maxreg* and defined in the tracking module **JPMT:**, **SYBILT:** or **EXCELT:** (see Section 3.4). For pure geometry with splitting we can define the variables  $L_x$ ,  $L_y$ ,  $L_z$ ,  $L_r$  and  $L_h$  as:

$$\begin{aligned}
 L_x &= \sum_{i=1}^{l_x} ispltx(i) \\
 L_y &= \sum_{i=1}^{l_y} isplty(i) \\
 L_z &= \sum_{i=1}^{l_z} ispltz(i) \\
 L_r &= \sum_{i=1}^{l_r} |ispltr(i)| \\
 L_h &= lh
 \end{aligned}$$

and  $L_t$  will be given by:

- CAR1D geometry.

$$L_t = L_x$$

- HEX geometry.

$$L_t = L_h$$

- SPHERE geometry.

$$L_t = L_r$$

- CAR2D geometry without diagonal symmetry.

$$L_t = L_x L_y$$

- CAR2D geometry with diagonal symmetry.

$$L_t = \frac{L_x(L_y + 1)}{2} = \frac{(L_x + 1)L_y}{2}$$

- CAR3D geometry without diagonal symmetry.

$$L_t = L_x L_y L_z$$

- CAR3D geometry with diagonal symmetry.

$$L_t = \frac{L_x(L_y + 1)L_z}{2} = \frac{(L_x + 1)L_y L_z}{2}$$

- TUBE geometry.

$$L_t = L_x L_y L_r$$

- TUBEX geometry.

$$L_t = L_x L_y L_z L_r$$

- TUBEY geometry.

$$L_t = L_x L_y L_z L_r$$

- TUBEZ geometry.

$$L_t = L_x L_y L_z L_r$$

- CARCEL geometries.

$$L_t = L_x L_y (L_r + 1)$$

- CARCELX geometry.

$$L_t = L_x L_y L_z (L_r + 1)$$

- CARCELY geometry.

$$L_t = L_x L_y L_z (L_r + 1)$$

- CARCELZ geometries.

$$L_t = L_x L_y L_z (L_r + 1)$$

- HEXZ geometry.

$$L_t = L_z L_h$$

- HEXCEL geometries.

$$L_t = (L_r + 1)$$

- HEXCELZ geometries.

$$L_t = L_z (L_r + 1)$$

For mixed geometries, it is important to ensure that  $L_t$  which represents the sum over all the sub-geometries of the total number of regions  $L_t^i$  associated with each pure sub-geometry  $i$  computed using the technique described above. For cluster geometries, only one region is associated with each zone in a pin even if this pin is repeated  $npins$  times.

### 3.3.4 Physical properties of geometry

In addition to specifying the mixture associated with each region in the geometry, the (**descPP**) structure is also used to provide information on the sub-geometry required in this geometry. For example, an optional procedure in DRAGON groups together regions so as to reduce the number of unknowns in the flux calculation. In this way, only the merged regions contribute to the cost of the calculation. However, the following points must be considered:

1. All the cells belonging to the same merged region must have the same dimensions and contain the same mixtures.
2. The grouping procedure is based on the approximation that all the regions belonging to the same merged region share the same flux.
3. The merging can also take into account region orientation (by a rotation and/or transposition) before they are merged. This procedure facilitates the merging of regions when a DIAG or SYME boundary condition is used.

The (**descPP**) structure has the following contents:

Table 24: Structure (**descPP**)

```
[ MIX (imix(i), i = 1, nt) [ REPEAT ] ]
[ CELL (HCELL(i), i = 1, Nt) ]
[ MERGE (imerge(i), i = 1, Nt) ]
[ TURN (HTURN(i), i = 1, Nt) ]
[ CLUSTER (NAMPIN(i), i = 1, Np) ]
```

where  $N_p$  is the number of pin types in the cluster and  $N_t$  is computed in just the same way as  $L_t$  except that one uses:

$$\begin{aligned}
 L_x &= lx \\
 L_y &= ly \\
 L_z &= lz \\
 L_r &= lr \\
 L_h &= lh
 \end{aligned}$$

The inputs associated with this structure have the following meaning:

- |             |   |
|-------------|---|
| <b>MIX</b>  | keyword to specify the isotopic mixture number associated with each region inside the geometry. When diagonal symmetries are considered, only the mixture associated with regions inside the original geometry need to be specified. Here $n_t \leq N_t$ .  |
| <i>imix</i> | array of mixture numbers associated with a region $imix \leq maxmix$ (see Sections 3.1 and 3.2). If $imix=0$ , the corresponding volume is replaced by a void region. These values must be specified in the following order for most geometries: <ol style="list-style-type: none"> <li>1. radially from the inside out (<math>lr+1</math> mixtures for CARCEL, CARCELZ, HEXCEL or HEXCELZ and <math>lr</math> for TUBE or TUBEZ).</li> <li>2. from surface X- to surface X+</li> <li>3. from surface Y- to surface Y+</li> <li>4. from surface Z- to surface Z+</li> </ol> |

In the cases where a CARCELX and a TUBEX geometry are defined then we will use

1. radially from the inside out ( $lr + 1$  mixtures for CARCELX and  $lr$  for TUBEX).

2. from surface Y- to surface Y+
3. from surface Z- to surface Z+
4. from surface X- to surface X+

Finally, for a CARCELY and TUBEY geometry are defined the following order is considered:

1. radially from the inside out ( $lr + 1$  mixtures for CARCELY and  $lr$  for TUBEY)
2. from surface Z- to surface Z+
3. from surface X- to surface X+
4. from surface Y- to surface Y+

REPEAT	keyword to specify the previous list of mixtures will be repeated. This is valid only when $N_t/n_t$ is an integer. If this keyword is absent and $n_t < N_t$ , then the missing mixtures will be replaced with void ( $imix=0$ ).
CELL	keyword to specify the location of the sub-geometry called <i>generating cells</i> in a Cartesian geometry. When a sub-geometry is located inside a geometry but outside the calculation region it must be declared <i>virtual</i> (for example, the corners of a nuclear reactor).
HCELL	array of sub-geometry <code>character*12</code> names which will be superimposed upon the current cartesian geometry. The same sub-geometry may appear in different positions within the global geometry if the material properties and dimensions are identical. The concept of sub-geometry is useful for the JPMT: and SYBILT: calculation options since the collision probability matrix associated with each sub-geometry is computed independently of its location in the geometry. In general, the neutron flux in identical sub-geometry located at different locations will be different even if they are associated with the same collision probability matrix. These sub-geometry names must be specified in the following order: <ol style="list-style-type: none"> <li>1. from surface X- to surface X+</li> <li>2. from surface Y- to surface Y+</li> <li>3. from surface Z- to surface Z+</li> </ol>
MERGE	keyword to specify that some sub-geometries or regions must be merged.
imerge	array of numbers that associate a global sub-geometry or region number with each sub-geometry or region. All the sub-geometries or regions with the same global number will be attributed the same flux.
TURN	keyword to specify that some sub-geometries must be rotated in space before being located at a specific position.
HTURN	array of <code>character*1</code> keywords to rotate conveniently each sub-geometry. The letters A to L are used as keywords to specify these rotation. For Cartesian geometries, the eight possible orientations are shown in figure Figure 7 while for hexagonal geometries the orientations available are illustrated in figure Figure 8. For 3-D cells, the same letters can be used to describe the rotation in the X - Y plane. However, an additional - sign can be glued to the 2-D rotation identifier to indicate reflection of the cell along the Z-axis (-A to -L).
CLUSTER	keyword to specify that pin sub-geometry will be inserted in the geometry (see Figure 9).
NAMPIN	array of sub-geometry <code>character*12</code> name representing a pin. This sub-geometry must be of type TUBE, TUBEX, TUBEY or TUBEZ.

### 3.3.5 Non standard geometries

Finally the structure (**descNSG**) provides the possibility to define non standard geometries such as double-heterogeneity and *do-it-yourself* assemblies:

Table 25: Structure (**descNSG**)

```
[ BIHET { TUBE | SPHE } nmistr nmilg
  (ns(i), i=1,nmistr)
  ((rs(i, j), j=1,ns(i)+1), i=1,nmistr)
  (milie(i), i=1,nmilg)
  (mixdil(i), i=1,nmilg)
  ( fract(i, j), j=1,nmistr) ( [(mixgr(i, j, k), k=1,ns(j))], j=1,nmistr), i=1,nmilg ]
[ POURCE (pcinl(i), i=1,lp) ]
[ PROCEL ((pijcel(i, j), j=1,lp), i=1,lp) ]
```

where

<b>BIHET</b>	keyword to specify that a sub-geometry made up of spherical or cylindrical micro structures is to be inserted into the current geometry. Each micro structure can be composed of many micro volumes. <sup>[54,55]</sup>
<b>TUBE</b>	keyword to specify that the micro structures are of a cylindrical geometry;
<b>SPHE</b>	keyword to specify that the micro structures are of a spherical geometry.
<b>nmistr</b>	number of micro structure types in the region. Each type of micro structure is characterized by its dimension and may have distinct volumetric concentrations in each of the macro geometry volumes. All the micro structures of a given type have the same nuclear properties in a given macro volume. The micro structures of a given type may have different nuclear properties within different macro volumes.
<b>nmilg</b>	number of micro structures regions.
<b>ns</b>	array giving the number of sub-regions (tubes or spherical shells) in the micro structures. Each type of micro structures may contain a different number of micro volumes.
<b>rs</b>	array giving the radius of the tubes or spherical shells making up the micro structures. For each type of micro structure $i$ , we will have an initial radius of $rs(1, i) = 0.0$ .
<b>milie</b>	array giving the composite mixture number associated with each region in the micro structures. These composite mixture numbers must be greater than the maximum number of real mixtures $maxmix$ .
<b>mixdil</b>	array giving the mixture number associated with each region of the geometry where the micro structure is to be inserted. It is required that $mixdil \leq maxmix$ .
<b>fract</b>	array of volumetric concentration ( $V_G/V_R$ ) of each micro structures (volume $V_G$ ) in a given region (volume $V_R$ ) of the geometry.

<i>mixgr</i>	array giving the mixture number associated with each region of the micro structures. Note that <i>mixgr</i> should be specified only for the regions of the micro structure which have a concentration <i>fract</i> > 0. It is required that $mixgr \leq maxmix$ .
<b>POURCE</b>	keyword to specify that a <i>do-it-yourself</i> type geometry is to be defined, that is to say a geometry resembling the multicell geometry seen in APOLLO-1. <sup>[15]</sup> This option permits the interactions between different arbitrarily and statistically (default option) arranged cells in an infinite lattice to be treated. The cells are identified by the information following the keyword <b>CELL</b> . The user must ensure that the total number of regions appearing in all the cells must be less than <i>maxreg</i> .
<i>pcinl</i>	array giving the proportion of each cells type in the lattice such that:

$$\left| \sum_{i=1}^{lp} pcinl(i) - 1. \right| < 10^{-5}$$

<b>PROCEL</b>	keyword to specify that in a <i>do-it-yourself</i> type geometry rather than using a statistical arrangement of cells, a pre-calculated cell distribution is to be considered.
<i>pijcel</i>	array giving the pre-calculated probability for a neutron leaving a cell of type <i>i</i> to enter a cell of type <i>j</i> without crossing any other cell. We require:

$$|S(i)pcinl(i)pijcel(i, j) - S(j)pcinl(j)pijcel(j, i)| < 10^{-4}$$

where  $S(i)$  and  $S(j)$  are the exterior surfaces area of the cells of type *i* and *j* respectively.

Examples of geometry definitions for DRAGON can be found in Section 4.2.

### 3.4 The tracking modules

A tracking module is required to analyze a spatial domain (geometry) assuming a given algorithm will be used for the collision probability calculations of for a solution by the method of characteristics. These modules perform an analysis of the geometry including volume and surface area calculations and generate the integration lines for a geometry that was previously defined in the **GEO:** module. These operations are carried out differently depending on the solution algorithm considered.

Five different modules are available for tracking in DRAGON. The **JPMT:** module is used to perform an interface current tracking inside homogeneous region.<sup>[10-14]</sup> The **SYBILT:** module is used for interface current tracking inside heterogeneous blocks. The **EXCELT:** module performs full cell collision probability tracking with isotropic<sup>[17,18]</sup> or specular<sup>[2,19-21]</sup> surface current. Finally, the **NXT:** module is an extension of the **EXCELT:** module to more complex geometry including assemblies of clusters in two and three dimensions.<sup>[56]</sup> These are the tracking modules that can be used to generate the information required for a solution to the transport equation.

The final module **BIVACT:** is used to perform a 2-D diffusion like tracking that may be required for homogenization purposes.<sup>[57]</sup> In this case, a finite element or finite difference discretization will be considered. Note that this module can only be used in the **EDI:** module since it is not compatible with the flux solution **FLU:** and self-shielding **SHI:** modules.

None of these modules can analyze all of the geometry available in the code DRAGON. In general, some restrictions apply to each tracking module as a function of the approximations associated with the specific transport solution method. In other instances, some geometries that could have been tracked by two different method, such as tube geometry for the **SYBILT:** and **EXCELT:** module, can only be analyzed by one of these tracking module (module **SYBILT:** in this case) to avoid redundancy.

Accordingly, only the following geometries can be analyzed by the module **EXCELT:**:

1. The two dimensional geometries (CAR2D and HEX) that contain sub-geometries (CARCEL and HEXCEL respectively).
2. The two dimensional cluster geometries corresponding to a TUBE sub-geometry superimposed on a global TUBE, CARCEL or HEXCEL geometry. Here, the only restriction is that the pins are fully located inside the annular part of the cell and they do not overlap even if they can overlap with internal annular regions.
3. Three dimensional geometry (CAR3D or HEXZ that contain sub-geometries (CARCELX, CARCELY and CARCELZ or HEXCEL respectively).

The following geometries can be analyzed by the module **NXT** : module:

1. The Cartesian 2-D and 3-D geometries that can be processed by the **EXCELT** : module described above.
2. A generalization of the Cartesian 2-D and 3-D geometries that can be processed by the **EXCELT** : module described above that includes pin clusters

The geometries that can be treated by the module **SYBILT** : are

1. The homogeneous geometry **HOMOG**.
2. The one dimensional geometries **SPHERE**, **TUBE** and **CAR1D**.
3. The two dimensional geometries **CAR2D** and **HEX** including **CARCEL** and **HEXCEL** sub-geometries as well as **VIRTUAL** sub-geometries.
4. Two dimensional non standard geometries containing micro structures.
5. The double heterogeneity option.

The module **JPMT** : can be used to analyze:

1. The one dimensional geometries **SPHERE**, **TUBE** and **CAR1D**.
2. The two dimensional geometries **CAR2D** and **HEX** including **CARCEL** and **HEXCEL** sub-geometries as well as **VIRTUAL** sub-geometries.
3. The two dimensional cluster geometries corresponding to a **TUBE** sub-geometry superimposed on a global **TUBE**, **CARCEL** or **HEXCEL** geometry. Here, each cluster must be located between two independent annular regions and the clusters must not overlap.
4. The three dimensional **TUBEZ** geometry.
5. The double heterogeneity option.

Finally, the **BIVACT** : module can only process directly:

- The two dimensional geometries **CAR2D** and **HEX**.

The general information resulting from these tracking module is stored in a **TRACKING** data structure. For the **JPMT** : , **EXCELT** : and **NXT** : modules, an additional sequential binary tracking file may be generated.

The global numbering of the zones in for a specific geometry proceeds following an order of priorities given by:

- the different rings of a cylindrical or spherical region starting with the inner most after mesh splitting;

- for a cluster regions located in a ring, two different numbering schemes are possible. For the **EXCELT:** module, one first numbers the region inside the pin in the same way as for cylindrical regions and finishes by associating the next region number to the shell of the global geometry which contains this pin. If two cluster types are located in a given ring, they are classified according to increasing *rpins* and *apins* and then numbered in this order. Cluster overlapping annular region are numbered before considering the annular regions. For the **NXT:** module, each pin is numbered individually in a Cartesian region according to their ordered in the **CLUSTER** keywords and then the Cartesian regions are numbered sequentially. A description of the explicit numbering of regions and surfaces can be found in report IGE-260.<sup>[56]</sup>
- the zones in ascending order corresponding to the first axial component (normally *X*) after mesh splitting;
- the zones in ascending order corresponding to the second axial component (normally *Y*) after mesh splitting;
- the hexagonal zones corresponding to the order described in Figures 1 to 6.
- In the module **EXCELT:** the sub-geometry of type **CARCELX**, **CARCELY** and **CARCELZ** are numbered assuming that the third component corresponds to *X*, *Y* and *Z* respectively. For the module **NXT:**, the regions are always numbered in *X*, *Y* and *Z*.<sup>[56]</sup>

One should also note that symmetry conditions implicitly force the grouping of certain calculation zones. The calling specifications for each of these modules is:

Table 26: Structure (**EXCELT:**)

```
TRKNAM [ TRKFIL ] := EXCELT: [ TRKNAM ] [ TRKFIL ] GEONAM :: (desctrack) (descexcel)
```

Table 27: Structure (**NXT:**)

```
{ TRKNAM := NXT: GEONAM :: (desctrack) (descnxt)
| TRKFIL TRKNAM := NXT: TRKNAM :: (desctrack) (descnxt)
| TRKFIL TRKNAM := NXT: GEONAM :: (desctrack) (descnxt) }
```

The first form will be used to analyze the geometry and track it but will not generate the tracking file. The second form will be used to generate the tracking file from a compatible **TRACKING** data structure. Finally the last form will generate both the tracking file and the **TRACKING** from the **GEOMETRY**. Thus, even if **TRKFIL** is not provided the tracking of the geometry may still take place and will be validated. The track normalization factors required to ensure volume preservation will also be computed and stored on **TRKNAM**. This information is required by the **ASM:** module for collision probability integration with inline track generation (see Section 3.6).

Table 28: Structure (**JPMT:**)

```
TRKNAM [ TRKFIL ] := JPMT: [ TRKNAM ] [ TRKFIL ] GEONAM :: (desctrack) (descjpm)
```

Table 29: Structure (**SYBILT:**)

$TRKNAM := SYBILT: [ TRKNAM ] GEONAM :: (desctrack) (descsybil)$
--

Table 30: Structure (**BIVACT:**)

$TRKNAM := BIVACT: [ TRKNAM ] GEONAM :: (desctrack) (descbivac)$
--

where

<b>TRKNAM</b>	character*12 name of the TRACKING data structure that will contain region volume and surface area vectors in addition to region identification pointers and other tracking information.
<b>TRKFIL</b>	character*12 name of the sequential binary tracking file used to store the tracks lengths. <sup>[6]</sup> This file is always required for the EXCELT: and NXT: modules. It is also required if the JPMT: module is applied to a cluster type geometry.
<b>GEONAM</b>	character*12 name of the GEOMETRY data structure.
<b>(desctrack)</b>	structure describing the general tracking data (see Section 3.4.1)
<b>(descexcel)</b>	structure describing the transport tracking data specific to EXCELT: (see Section 3.4.2).
<b>(descnxt)</b>	structure describing the transport tracking data specific to NXT: (see Section 3.4.3).
<b>(descsybil)</b>	structure describing the transport tracking data specific to SYBILT: (see Section 3.4.4).
<b>(descjpm)</b>	structure describing the transport tracking data specific to JPMT: (see Section 3.4.5).
<b>(descbivac)</b>	structure describing the diffusion tracking data specific to BIVACT: (see Section 3.4.6).

### 3.4.1 The general tracking data

Table 31: Structure (**desctrack**)

$[ EDIT\ iprint ]$ $[ TITL\ TITLE ]$ $[ ANIS\ nanis ]$ $[ \{ RENO\   NORE\   RENM\   REND\ } ]$
--

with

<b>EDIT</b>	keyword used to modify the print level <i>iprint</i> .
<i>iprint</i>	index used to control the printing of this module. The amount of output produced by this tracking modules will vary substantially depending on the print level specified. For example, <ul style="list-style-type: none"> <li>• when <i>iprint</i>=0 no output is produced;</li> <li>• when <i>iprint</i>=1 a minimum amount of output is produced; the main geometry properties are printed (fixed default option);</li> <li>• when <i>iprint</i>≥2 In addition to the information printed when using <i>iprint</i>=1 the zone numbering (zones associated with a flux) is printed;</li> <li>• when <i>iprint</i>≤-1000 is equivalent to <i>iprint</i>=0 except that an extended version of the tracking file is created that contains, in addition to the standard information, the initial position in space of each tracking line that can be used with a line plotting module;</li> </ul>
<b>TITL</b>	keyword which allows the run title to be set.
<i>TITLE</i>	the title associated with a DRAGON run. This title may contain up to 72 characters. The default when <b>TITL</b> is not specified is no title.
<b>ANIS</b>	keyword to specify the order of anisotropy in collision probability or for the method of characteristics.
<i>nanis</i>	order of anisotropy in collision probability or for the method of characteristics. A default value of 1 represents isotropic calculations while a value of 2 corresponds to linearly anisotropic collision probability. For the <b>PIJK</b> option, a value of 2 is required (see Section 3.6).
<b>RENO</b>	keyword to specify the use of the automatic procedure for integration lines normalization to the fine mesh volumes. This normalization procedure should always be used to ensure neutron balances for each fine mesh zone. It is the default option for transport tracking and is forbidden for the <b>BIVACT</b> : diffusion tracking module.
<b>NORE</b>	keyword to specify that the automatic normalization of the integration lines should be deactivated. It is forbidden for the <b>BIVACT</b> : diffusion tracking module.
<b>RENM</b>	keyword to specify the use of the automatic procedure for integration lines normalization to the merged volumes. This normalization procedure should always be used to ensure neutron balances for each merged zone. This option is only valid when the <b>EXCELT</b> : module is called.
<b>REND</b>	keyword to specify the use of the automatic procedure for integration lines normalization to the merged volumes for each tracking direction. This option is only valid when the <b>NXT</b> : module is called.

### 3.4.2 The **EXCELT**: specific tracking data

Table 32: Structure (**descexcel**)

```
[ MAXR maxreg ]
[ { PISO | PSPC [ CUT pcut ] } ]
[ TRAK { TISO [ { EQW | GAUS } ] nangl ]
[ { GAUS | LCMD | CACA | CACB } nphi ]
dens [ densz ] CORN pcorn ]
[ SYMM isymm ]
    | TSPC [ MEDI ] nangl dens } ]
```

where

MAXR	keyword which permits the maximum number of regions to be considered during a DRAGON run to be specified.
maxreg	maximum dimensions of the problem to be considered. The default value is set to the number of regions previously computed by the GEO: module. However this value is generally insufficient if symmetries or mesh splitting are specified.
PISO	keyword to specify that a collision probability calculation with isotropic reflection boundary conditions is required. It is the default option if a TISO type integration is chosen. To obtain accurate transmission probabilities for the isotropic case it is recommended that the normalization options in the ASM: module be used.
PSPC	keyword to specify that a collision probability calculation with mirror like reflection or periodic boundary conditions is required; this is the default option if a TSPC type integration is chosen. This calculation is only possible if the file was initially constructed using the TSPC option.
CUT	keyword to specify the input of cutting parameters for the specular collision probability of characteristic integration.
pcut	real value representing the maximum error allowed on the exponential function used for specular collision probability calculations. Tracks will be cut at a length such that the error in the probabilities resulting from this reduced track will be of the order of <i>pcut</i> . By default, the tracks are extended to infinity and <i>pcut</i> =0.0. If this option is used in an entirely reflected case, it is recommended to use the NORM command in the ASM: module.
TRAK	keyword to specify the tracking parameters to be used.
TISO	keyword to specify that isotropic tracking parameters will be supplied. This is the default tracking option for cluster geometries.
EQW	keyword to specify the use of equal weight quadrature. <sup>[58]</sup>
GAUS	keyword to specify the use of the Gauss-Legendre quadrature. This option is valid only if an hexagonal geometry is considered.
TSPC	keyword to specify that specular tracking parameters will be supplied. This option is invalid if an hexagonal geometry is considered.
MEDI	keyword to specify that instead of selecting the angles located at the end of each angular interval, the angles located in the middle of these intervals are selected. This is particularly useful if one wants to avoid tracking angles that are parallel to the <i>X</i> – or <i>Y</i> – axis as its is the case when the external region of a CARCEL geometry is voided.

<i>nangl</i>	angular quadrature parameter. For 3-D geometry, only the EQW option is permitted with <i>nangl</i> =2, 4, 8, 10, 12, 14 or 16. <sup>[6]</sup> For 2-D isotropic applications, any value of <i>nangl</i> may be used, equidistant angles will be selected. For 2-D specular applications the input value must be of the form $p + 1$ where $p$ is a prime number (for example $p=7,11$ , etc.); the choice of <i>nangl</i> = 8, 12, 14, 18, 20, 24, or 30 are allowed.
GAUS	keyword to specify that Gauss polar integration angles are to be selected.
LCMD	keyword to specify that optimized polar integration angles are to be selected. <sup>[59]</sup> This is the default option.
CACA	keyword to specify that CACTUS type equal weight polar integration angles are to be selected. <sup>[60]</sup>
CACB	keyword to specify that CACTUS type uniformly distributed integration polar angles are to be selected. <sup>[60]</sup>
<i>nphi</i>	the polar quadrature order.
<i>dens</i>	real value representing the density of the integration lines (in $\text{cm}^{-1}$ for 2-D Cartesian cases and $\text{cm}^{-2}$ for 3-D cases Cartesian cases ). This choice of density along the plan perpendicular to each angle depends on the geometry of the cell to be analyzed. If there are zones of very small volume, a high line density is essential. This value will be readjusted by EXCELT: . In the case of the analysis of a cluster type geometry the default value of this parameter is $5/r_m$ where $r_m$ is the minimum radius of the pins or the minimum thickness of an annular ring in the geometry.
<i>densz</i>	real value representing the density of the integration lines (in $\text{cm}^{-1}$ for 3-D hexagonal cases).
CORN	keyword to specify that the input of the parameters used to treat the corners for the isotropic integration.
<i>pcorn</i>	maximum distance (cm) between a line and the intersection of $n \geq 2$ external surfaces where track redistributing will take place. Track redistribution will take place if a line comes close to the intersection of $n \geq 2$ external surfaces. In this case the line will be replicated $n$ times, each of these lines being associated with a different external surface, while its weight is reduced by a factor of $1/n$ . This allows for a better distribution of tracks which are relatively close to $n$ external surfaces. By default, there is no treatment of the corners and <i>pcorn</i> =0.0.
SYMM	keyword to specify that the geometry has a rotation symmetry.
<i>isymm</i>	integer value describing the rotation symmetry of the geometry. The fixed default of this parameter is 1.

### 3.4.3 The NXT: specific tracking data

Table 33: Structure (**descnxt**)

```
[ { PISO | PSPC [ CUT pcut ] } ]
[ NOTR ]
TISO [ { EQW | PNTN | SMS | GAUS } ] nangl [ { GAUS | LCMD | CACA | CACB } nphi ] dens [ CORN pcorn ]
```

where

PISO	keyword to specify that a collision probability calculation with isotropic reflection boundary conditions is required. It is the default option if a TISO type integration is chosen. To obtain accurate transmission probabilities for the isotropic case it is recommended that the normalization options in the ASM: module be used.
PSPC	keyword to specify that a collision probability calculation with mirror like reflection or periodic boundary conditions is required; this is the default option if a TSPC type integration is chosen. This calculation is only possible if the file was initially constructed using the TSPC option.
CUT	keyword to specify the input of cutting parameters for the specular collision probability of characteristic integration.
<i>pcut</i>	real value representing the maximum error allowed on the exponential function used for specular collision probability calculations. Tracks will be cut at a length such that the error in the probabilities resulting from this reduced track will be of the order of <i>pcut</i> . By default, the tracks are extended to infinity and <i>pcut</i> =0.0. If this option is used in an entirely reflected case, it is recommended to use the NORM command in the ASM: module.
NOTR	keyword to specify that the geometry will not be tracked. This is useful for 2-D geometries to generate a tracking data structure that can be used by the PSP: module (see Section 3.15). One can then verify visually if the geometry is adequate before the tracking process as such is undertaken.
TISO	keyword to specify that isotropic tracking parameters will be supplied. This is the default tracking option for cluster geometries.
EQW	keyword to specify the use of equal weight quadrature. <sup>[58]</sup>
PNTN	keyword to specify that Legendre-Techbychev quadrature quadrature will be selected. <sup>[61]</sup>
SMS	keyword to specify that Legendre-trapezoidal quadrature quadrature will be selected. <sup>[62]</sup>
GAUS	keyword to specify the use of the Gauss-Legendre quadrature. This option is valid only if an hexagonal geometry is considered.
<i>nangl</i>	angular quadrature parameter. For a 3-D EQW option, the choices are <i>nangl</i> =2, 4, 8, 10, 12, 14 or 16. For a 3-D PNTN or SMS option, <i>nangl</i> is an even number smaller than 46. <sup>[56]</sup> For 2-D isotropic applications, any value of <i>nangl</i> may be used, equidistant angles will be selected. For 2-D specular applications the input value must be of the form $p + 1$ where $p$ is a prime number (for example $p=7, 11$ , etc.); the choice of <i>nangl</i> = 8, 12, 14, 18, 20, 24, or 30 are allowed.
GAUS	keyword to specify that Gauss polar integration angles are to be selected.
LCMD	keyword to specify that optimized polar integration angles are to be selected. <sup>[59]</sup> This is the default option.
CACA	keyword to specify that CACTUS type equal weight polar integration angles are to be selected. <sup>[60]</sup>
CACB	keyword to specify that CACTUS type uniformly distributed integration polar angles are to be selected. <sup>[60]</sup>
<i>nphi</i>	the polar quadrature order.

<i>dens</i>	real value representing the density of the integration lines (in $\text{cm}^{-1}$ for 2-D Cartesian cases and 3-D hexagonal cases and $\text{cm}^{-2}$ for 3-D cases Cartesian cases ). This choice of density along the plan perpendicular to each angle depends on the geometry of the cell to be analyzed. If there are zones of very small volume, a high line density is essential. This value will be readjusted by <b>NXT</b> : .
<i>densz</i>	real value representing the density of the integration lines (in $\text{cm}^{-1}$ for 3-D hexagonal cases).
<b>CORN</b>	keyword to specify that the input of the parameters used to treat the corners for the isotropic integration.
<i>pcorn</i>	maximum distance (cm) between a line and the intersection of $n \geq 2$ external surfaces where track redistributing will take place. Track redistribution will take place if a line comes close to the intersection of $n \geq 2$ external surfaces. In this case the line will be replicated $n$ times, each of these lines being associated with a different external surface, while its weight is reduced by a factor of $1/n$ . This allows for a better distribution of tracks which are relatively close to $n$ external surfaces. By default, there is no treatment of the corners and <i>pcorn</i> =0.0.

#### 3.4.4 The **SYBILT**: specific tracking data

Table 34: Structure (**descsybil**)

```
[ MAXR maxreg ]
[ MAXJ maxcur ] [ MAXZ maxint ]
[ HALT ]
[ QUA1 iqua1 ] [ QUA2 iqua2 nsegment ] [ { EQW | GAUS } ]
[ { ROTH | ROT+ | DP00 | DP01 } ]
[ ASKE ] [ LIGN ] [ RECT ]
[ QUAB iquab ]
```

where

<b>MAXR</b>	keyword which permits the maximum number of regions to be considered during a <b>DRAGON</b> run to be specified.
<i>maxreg</i>	maximum dimensions of the problem to be considered. The default value is set to the number of regions previously computed by the <b>GEO</b> : module. However this value is generally insufficient if symmetries or mesh splitting are specified.
<b>MAXJ</b>	keyword to specify the maximum number of interface currents surrounding the blocks in the calculations.
<i>maxcur</i>	the maximum number of interface currents surrounding the blocks. The default value is <i>maxcur</i> =max(18,4× <i>maxreg</i> ) for the <b>SYBILT</b> : module.
<b>MAXZ</b>	keyword to specify the maximum amount of memory required to store the integration lines.
<i>maxint</i>	the maximum amount of memory required to store the integration lines. The default value is <i>maxint</i> =10000.

HALT	keyword to specify that the program is to be stopped at the end of the geometry calculations. This option permits the geometry inputs to be checked, the number of blocks and interface currents to be calculated, and a conservative estimate of the memory required for storing the tracks to be made for mixed geometries.
QUA1	keyword to specify the one dimensional integration parameters.
<i>iqua1</i>	number of basis points for the angular integration of the blocks in a one dimensional geometry. This parameter is not used for CAR1D geometries. If a Gauss-Legendre or Gauss-Jacobi quadrature is used, the values of <i>iqua1</i> allowed are: 1 to 20, 24, 28, 32 or 64. The default value is <i>iqua1</i> =5.
QUA2	keyword to specify the two dimensional integration parameters.
<i>iqua2</i>	number of basis points for the angular integration of the blocks in a two dimensional geometry appearing during assembly calculations. If a Gauss-Legendre or Gauss-Jacobi formula is used the values allowed for <i>iqua2</i> are: 1 to 20, 24, 28, 32 or 64. The default value is <i>iqua2</i> =6 and represents the number of angles in $(0, \pi/4)$ for Cartesian geometries and $(0, \pi/6)$ for hexagonal geometries.
<i>nsegment</i>	number of basis points for the spatial integration of the blocks in a two dimensional geometry appearing during assembly calculations. The default value is <i>nsegment</i> =3.
EQW	keyword to specify the use of equal weight quadrature.
GAUS	keyword to specify the use of the Gauss-Legendre or the Gauss-Jacobi quadrature. This is the default option.
ROTH	keyword to specify that the isotropic ( $DP_0$ ) components of the current at cell interface is used with the incoming current being averaged over all the faces surrounding a cell. The global collision matrix is calculated in a annular model. Only used when a 2-D assembly of cells is considered.
ROT+	keyword to specify that the isotropic ( $DP_0$ ) components of the current at cell interface is used. The global collision matrix is calculated in a annular model. Only used when a 2-D assembly of cells is considered.
DP00	keyword to specify that the isotropic ( $DP_0$ ) components of the current at cell interface is used. The global collision matrix is computed explicitly. Only used when a 2-D assembly of cells is considered.
DP01	keyword to specify that the linearly anisotropic ( $DP_1$ ) components of the current at cell interface are used. This hypothesis implies 12 currents per cell in a cartesian geometry and 18 currents per cell for a hexagonal geometry. Linearly anisotropic reflection is used. Only used when a 2-D assembly of cells is considered.
ASKE	keyword to specify the use of an Askew cylinderization which preserves both the external surface of the cells and the material balance of the external crown (by a modification of its concentration). By default a Wigner cylinderization is used which preserves the volume of the external crown. Note, that an assembly of a number of rectangular cells having unequal volumes requires an Askew cylinderization. This applies only in cases where the external surface is annular using the ROTH or ROT+ options. Only used when a 2-D assembly of cells is considered.
LIGN	keyword to specify that all the integration lines are to be printed. This option should only be used when absolutely necessary because it generates a rather large amount of output. Only used when a 2-D assembly of cells is considered.

RECT	keyword to specify that square cells are to be treated as if they were rectangular cells, with the inherent loss in performance that this entails. This option is of purely academic interest.
QUAB	keyword to specify the initial number of basis point for the numerical integration of each micro structure in cases involving double heterogeneity.
<i>iquab</i>	the number of basis point for the numerical integration of the collision probabilities in the micro volumes using the Gauss-Jacobi formula. The values permitted are: 1 to 20, 24, 28, 32 or 64. The default value is <i>iquab</i> =5.

### 3.4.5 The JPMT : specific tracking data

Table 35: Structure (**descjpm**)

```
[ MAXR maxreg ]
[ MAXJ maxcur ] [ MAXZ maxint ]
[ HALT ] [ OLD ]
[ { IP00 | SP01 | IP01 } ]
[ QUA1 iqua1 ] [ QUA2 iqua2 nsegment ] [ { EQW | GAUS } ]
[ { ROTH | ROT+ | DP00 | DP01 } ]
[ ASKE ] [ LIGN ] [ RECT ]
[ { RECD | RECR } ]
[ { BP00 | BP01 } ] [ QUAB iquab ]
```

where

MAXR	keyword which permits the maximum number of regions to be considered during a DRAGON run to be specified.
<i>maxreg</i>	maximum dimensions of the problem to be considered. The default value is set to the number of regions previously computed by the GEO : module. However this value is generally insufficient if symmetries or mesh splitting are specified.
MAXJ	keyword to specify the maximum number of interface currents surrounding the blocks in the calculations.
<i>maxcur</i>	the maximum number of interface currents surrounding the blocks. The default value is <i>maxcur</i> =max(50,6× <i>maxreg</i> ) for the JPMT : module.
MAXZ	keyword to specify the maximum amount of memory required to store the integration lines. Not used for cluster geometries.
<i>maxint</i>	the maximum amount of memory required to store the integration lines. The default value is <i>maxint</i> =10000.
OLD	keyword to specify that a set of previously calculated collision probabilities previously saved on <i>TRKNAM</i> is to be recovered. This option is of interest in cases where the coolant occupies a region of a complex geometry (such as a fuel assembly or bundle) and calculations of isotopic

evolution (burnup) or resonance self-shielding are required. By default, all the probabilities are recalculated even if only one isotopic mixture is modified.

HALT	keyword to specify that the program is to be stopped at the end of the geometry calculations. This option permits the geometry inputs to be checked, the number of blocks and interface currents to be calculated, and a conservative estimate of the memory required for storing the tracks to be made for mixed geometries. This keyword is not used for cluster type geometries.
IP00	keyword to specify that an isotropic angular flux between each block is used (default option for the TUBEZ geometries).
SP01	keyword to specify that a linearly anisotropic angular flux between each block is used in combination with linearly anisotropic boundary conditions (default option for all geometries except TUBE, SPHERE and TUBEZ).
IP01	keyword to specify that a linearly anisotropic angular flux between each block is used in combination with isotropic boundary conditions (default option for the TUBE and SPHERE geometries).
QUA1	keyword to specify the one dimensional integration parameters.
<i>iqua1</i>	number of basis points for the angular integration of the blocks in a one dimensional geometry. This parameter is not used for CAR1D geometries. If a Gauss-Legendre or Gauss-Jacobi quadrature is used, the values of <i>iqua1</i> allowed are: 1 to 20, 24, 28, 32 or 64. The default value is <i>iqua1</i> =5.
QUA2	keyword to specify the two dimensional integration parameters.
<i>iqua2</i>	number of basis points for the angular integration of the blocks in a two dimensional geometry appearing during assembly and cluster calculations. If a Gauss-Legendre or Gauss-Jacobi formula is used the values allowed for <i>iqua2</i> are: 1 to 20, 24, 28, 32 or 64. The default value is <i>iqua2</i> =6 and represents the number of angles in $(0, \pi/4)$ for cartesian geometries and $(0, \pi/6)$ for hexagonal geometries.
<i>nsegment</i>	number of basis points for the spatial integration of the blocks in a two dimensional geometry appearing during assembly and cluster calculations. The default value is <i>nsegment</i> =3.
EQW	keyword to specify the use of equal weight quadrature.
GAUS	keyword to specify the use of the Gauss-Legendre or the Gauss-Jacobi quadrature. This is the default option.
ROTH	keyword to specify that the isotropic ( $DP_0$ ) components of the current at cell interface is used with the incoming current being averaged over all the faces surrounding a cell. The global collision matrix is calculated in an annular model. Only used when a 2-D assembly of cells is considered.
ROT+	keyword to specify that the isotropic ( $DP_0$ ) components of the current at cell interface is used. The global collision matrix is calculated in an annular model. Only used when a 2-D assembly of cells is considered.
DP00	keyword to specify that the isotropic ( $DP_0$ ) components of the current at cell interface is used. The global collision matrix is computed explicitly. Only used when a 2-D assembly of cells is considered.

DP01	keyword to specify that the linearly anisotropic ( $DP_1$ ) components of the current at cell interface are used. This hypothesis implies 12 currents per cell in a cartesian geometry and 18 currents per cell for a hexagonal geometry. Linearly anisotropic reflection is used. Only used when a 2-D assembly of cells is considered.
ASKE	keyword to specify the use of an <i>Askew</i> cylinderization which preserves both the external surface of the cells and the material balance of the external crown (by a modification of its concentration). By default a <i>Wigner</i> cylinderization is used which preserves the volume of the external crown. Note, that an assembly of a number of rectangular cells having unequal volumes requires an <i>Askew</i> cylinderization. This applies only in cases where the external surface is annular using the ROTH or ROT+ options. Only used when a 2-D assembly of cells is considered.
LIGN	keyword to specify that all the integration lines are to be printed. This option should only be used when absolutely necessary because it generates a rather large amount of output. Only used when a 2-D assembly of cells is considered.
RECT	keyword to specify that square cells are to be treated as if they were rectangular cells, with the inherent loss in performance that this entails. This option is of purely academic interest.
RECD	keyword to specify the use of the direct reconstruction method for the collision probabilities (method with refraction effects). Only used when cluster geometries are considered.
RECR	keyword to specify the use of the surface fractioning reconstruction method for the collision probabilities (no refraction effect but twice the number of interfaces). This is the default option. Only used when cluster geometries are considered.
BP00	keyword to specify the use of an isotropic angular flux ( $DP_0$ ) approximation between the micro volumes making up the micro structures in a case involving the treatment of double heterogeneity.
BP01	keyword to specify the use of a linearly anisotropic angular flux ( $DP_1$ ) approximation between the micro volumes making up the micro structures in a case involving the treatment of double heterogeneity. In all cases, an approximation of isotropic angular flux is used on the interface between the micro structures and the macro volumes. This is the default option.
QUAB	keyword to specify the initial number of basis point for the numerical integration of each micro structure in cases involving double heterogeneity.
<i>iquab</i>	the number of basis point for the numerical integration of the collision probabilities in the micro volumes using the Gauss-Jacobi formula. The values permitted are: 1 to 20, 24, 28, 32 or 64. The default value is <i>iquab</i> =5.

### 3.4.6 The BIVACT : specific tracking data

Note that this tracking option can be used only indirectly through the SPH homogenization option (see Section 3.9.1):

Table 36: Structure (**deschivac**)

<pre>[ MAXR maxreg ] [ { PRIM   DUAL } [ ielem icol [ isplh ] ] ]</pre>
---

where

<b>MAXR</b>	keyword which permits the maximum number of regions to be considered during a DRAGON run to be specified.
<i>maxreg</i>	maximum dimensions of the problem to be considered. The default value is set to the number of regions previously computed by the <b>GEO:</b> module. However this value is generally insufficient if symmetries or mesh splitting are specified.
<b>PRIM</b>	keyword to set a primal finite element (classical) discretization.
<b>DUAL</b>	keyword to set a mixed-dual finite element discretization.
<i>ielem</i>	order of the finite element representation. The values permitted are 1 (linear polynomials), 2 (parabolic polynomials), 3 (cubic polynomials) or 4 (quartic polynomials). By default <i>ielem</i> =1. Discretization of a hexagonal geometry is only available with <i>ielem</i> =1.
<i>icol</i>	type of quadrature used to integrate the mass matrices. The values permitted are 1 (analytical integration), 2 (Gauss-Lobatto quadrature) or 3 (Gauss-Legendre quadrature). By default <i>icol</i> =2. The analytical integration corresponds to classical finite elements; the Gauss-Lobatto quadrature corresponds to a variational or nodal type collocation and the Gauss-Legendre quadrature corresponds to superconvergent finite elements.
<i>isplh</i>	type of hexagonal mesh splitting. This data is given only if the geometry is 2-D hexagonal. The values permitted are 1 (full hexagon), 2 for splitting each hexagon into 6 triangles, 3 for splitting each hexagon into 24 triangles, 5 for splitting each hexagon into 96 triangles, 9 for splitting each hexagon into 384 triangles and 17 for splitting each hexagon into 1536 triangles.

Various finite element approximations can be obtained by combining different values of *ielem* and *icol*:

- **PRIM 1 1** Linear finite elements;
- **PRIM 1 2** Mesh corner finite differences;
- **PRIM 1 3** Linear superconvergent finite elements;
- **PRIM 2 1** Quadratic finite elements;
- **PRIM 2 2** Quadratic variational collocation method;
- **PRIM 2 3** Quadratic superconvergent finite elements;
- **PRIM 3 1** Cubic finite elements;
- **PRIM 3 2** Cubic variational collocation method;
- **PRIM 3 3** Cubic superconvergent finite elements;
- **PRIM 4 2** Quartic variational collocation method;
- **DUAL 1 1** Mixed-dual linear finite elements;
- **DUAL 1 2** Mesh centered finite differences;
- **DUAL 1 3** Mixed-dual linear superconvergent finite elements  
(numerically equivalent to **PRIM 1 3**);
- **DUAL 2 1** Mixed-dual quadratic finite elements;
- **DUAL 2 2** Quadratic nodal collocation method;

- DUAL 2 3 Mixed-dual quadratic superconvergent finite elements  
(numerically equivalent to PRIM<sup>2 3</sup>);
- DUAL 3 1 Mixed-dual cubic finite elements;
- DUAL 3 2 Cubic nodal collocation method;
- DUAL 3 3 Mixed-dual cubic superconvergent finite elements  
(numerically equivalent to PRIM<sup>3 3</sup>);
- DUAL 4 2 Quartic nodal collocation method;

### 3.5 The SHI : module

The self-shielding module in DRAGON, called SHIBA<sup>[63]</sup>, allows the energy dependent dilution parameter (microscopic dilution cross section) associated with each resonant isotope, identified as such by the *inrs* parameter defined in Section 3.2, to be recalculated. The general input format for this module is:

Table 37: Structure (SHI:)

*MICLIB* := SHI : { *MICLIB* | *OLDLIB* } *TRKNAM* [ *TRKFIL* ] : : (descshi)

where

<i>MICLIB</i>	character*12 name of the MICROLIB that will contain the microscopic and macroscopic cross sections updated by the self-shielding module.
<i>OLDLIB</i>	character*12 name of a read-only MICROLIB that is copied into <i>MICLIB</i> . The library <i>OLDLIB</i> is first copied into <i>MICLIB</i> before it is updated.
<i>TRKNAM</i>	character*12 name of the required TRACKING data structure.
<i>TRKFIL</i>	character*12 name of the sequential binary tracking file used to store the tracks lengths. This file is given if and only if it was required in the previous tracking module call (see Section 3.4).
(descshi)	structure describing the self-shielding options.

Each time the SHI : module is called, a sub-directory is updated in the MICROLIB data structure to hold the last values defined in the (descshi) structure. The next time this module is called, these values will be used as floating defaults.

#### 3.5.1 Data input for module SHI :

Table 38: Structure (**descshi**)

```
[ EDIT iprint ]
[ GRMIN lgrmin ] [ GRMAX lgrmax ]
[ MXIT imxit ] [ EPS valeps ]
[ { LJ | NOLJ } ] [ { GC | NOGC } ] [ { NOTR } ]
[ LEVE level ] [ PIJ ]
```

where

EDIT	keyword used to modify the print level <i>iprint</i> .
<i>iprint</i>	index used to control the printing of this module. The amount of output produced by this tracking module will vary substantially depending on the print level specified.
GRMIN	keyword to specify the minimum group number considered during the self-shielding process.
<i>lgrmin</i>	first group number considered during the self-shielding process. By default, <i>lgrmin</i> is set to 1 for all the libraries except for those in the WIMSAECL and WIMSD4 format where this information is provided explicitly in the library.
GRMAX	keyword to specify the maximum group number considered during the self-shielding process.
<i>lgrmax</i>	last group number considered during the self-shielding process. By default, <i>lgrmax</i> is set to the group closer to 4.0 eV for all the libraries except for those in the WIMSAECL and WIMSD4 format where this information is provided explicitly in the library.
MXIT	keyword to specify the maximum number of iterations during the self-shielding process.
<i>imxit</i>	the maximum number of iterations. The default is <i>imxit</i> =20.
EPS	keyword to specify the convergence criterion for the self-shielding iteration.
<i>valeps</i>	the convergence criterion for the self-shielding iteration. By default, <i>valeps</i> is set to $1.0 \times 10^{-4}$ .
LJ	keyword to activate the Livolant-Jeanpierre normalization scheme that modifies the self-shielded averaged neutron flux in heterogeneous geometries. By default the Livolant-Jeanpierre normalization scheme is not activated.
NOLJ	keyword to deactivate the Livolant-Jeanpierre normalization scheme. This is the default option.
GC	keyword to activate the Goldstein-Cohen approximation in cases where Goldstein-Cohen parameters are stored on the microscopic cross section library. These parameters are not available if the resonant isotopes are interpolated from a MATXS type library. This is the default option.
NOGC	keyword to deactivate the Goldstein-Cohen approximation even if Goldstein-Cohen parameters are stored on the microscopic cross section library.
NOTR	keyword to deactivate the transport correction option for self-shielding calculations (see CTRA in Sections 3.1 and 3.2).
LEVE	keyword to specified the self-shielding correction option. When this option is not specified the option <i>level</i> =0 is selected.

<i>level</i>	the self-shielding correction option. In the case where <i>level</i> =0, the original Stamm'ler model is used (DRAGON 3.05 and before). For <i>level</i> =1 the original Stamm'ler model with Nordheim approximation is selected while for <i>level</i> =2 the Stamm'ler model with Nordheim approximation and Riemann integration method is selected. <sup>[64]</sup>
<b>PIJ</b>	keyword to specify the use of complete collision probabilities for the <b>JPMT:</b> calculation option. By default, a fast reconstruction algorithm based on sparse matrix algebra is used.

### 3.6 The assembly modules

We will now describe the assembly modules that can be used to prepare the group dependent complete collision probability or the assembly matrices required by the flux solution module of DRAGON. There are two assembly modules: **ASM:** and **EXCELL:**. The assembly module **ASM:** is generally called after a tracking module; it recovers tracking lengths and material numbers from the sequential tracking file and then computes the collision probability matrices under various normalization. The **EXCELL:** module can also be used to perform the work of both the **EXCELT:** and the **ASM:** modules for computing collision probabilities in 3-D geometries. This last module has been programmed to enhance the capability and performance of collision probability calculations for 3-D applications. The **EXCELL:** module does not keep the tracking file, the file is rebuilt at the same time as collision probabilities are computed. This feature enables users to do fine mesh calculations in 3-D domains without any limitation on the size of the tracking file. The input specifications for these modules are :

Table 39: Structure (**ASM:**)

<i>PIJNAM</i> := <b>ASM:</b> [ <i>PIJNAM</i> ] <i>LIBNAM</i> <i>TRKNAM</i> [ <i>TRKFIL</i> ] :: ( <b>descasm</b> )
--

and

Table 40: Structure (**EXCELL:**)

<i>PIJNAM</i> <i>TRKNAM</i> := <b>EXCELL:</b> <i>GEONAM</i> <i>LIBNAM</i> :: ( <b>desctrack</b> ) ( <b>descXL</b> )
---

where

<i>PIJNAM</i>	character*12 name of ASMPIJ data structure containing the system matrices.
<i>LIBNAM</i>	character*12 name of the MACROLIB or MICROLIB data structure that contains the macroscopic cross sections (see Sections 3.1 and 3.2).
<i>TRKNAM</i>	character*12 name of the TRACKING data structure containing the tracking (see Section 3.4).
<i>TRKFIL</i>	character*12 name of the sequential binary tracking file used to store the tracks lengths. This file is required if it is produced by the tracking module (see Section 3.4).
<i>GEONAM</i>	character*12 name of the GEOMETRY data structure for the <b>EXCELL:</b> module (see Section 3.3).
( <b>descasm</b> )	structure containing the input data to this module (see Section 3.6.1).

**(desctrack)** structure containing the general tracking data to the EXCELL: module (see Section 3.4.2).

**(descXL)** structure containing the input data to the EXCELL: module (see Section 3.6.2).

Note that for a TRACKING generated using the NXT: module, the file *TRKFIL* is not required. In this case the integration lines will be generated directly in the ASM: module. This is the equivalent of the EXCELL: module for the NXT: processed geometries.

### 3.6.1 Data input for module ASM:

Table 41: Structure (**descasm**)

```
[ EDIT iprint ]
[ { ARM [ NOR2 ] } ]
[ { PIJ | PIJK } [ SKIP ] [ [ NORM ] ALBS ] [ NAME NMPIJ ] ]
[ PNOR { NONE | DIAG | GELB | HELI | NONL } ]
[ ALLG ]
```

where

**EDIT** keyword used to modify the print level *iprint*.

*iprint* index used to control the printing of this module. The amount of output produced by this tracking module will vary substantially depending on the print level specified.

**ARM** keyword to specify that an assembly calculation is carried out without building the full collision probability matrices. This option can only be used for a geometry tracked using the JPMT: module. By default, the PIJ option is used.

**NOR2** keyword to specify that the matrix required for residual calculation is not required. This is active only when the JPMT: tracking module is called. Only the variational acceleration technique in module FLU: uses this information (see Section 3.7).

**PIJ** keyword to specify that the standard collision probabilities must be computed. This is the default option.

**PIJK** keyword to specify that both the directional and standard collision probabilities must be computed. Note that the additional directional collision probability matrix can only be used if *nanis* is set to 2 in Section 3.4 and HETE is activated in Section 3.7. Finally, the PIJK option is only available for 2-D geometries analyzed with the module EXCELT:.

**SKIP** keyword to specify that only the complete collision probability matrix  $p_{ij}^g$  is to be computed. In general, the scattering modified collision probability matrix  $p_{s,ij}^g$  is also computed using:

$$p_{s,ij}^g = [I - p_{ij}^g \Sigma_{s0}^{g \rightarrow g}]^{-1} p_{ij}^g$$

where  $\Sigma_{s0}^{g \rightarrow g}$  is the within group isotropic scattering cross section. When available,  $p_{s,ij}^g$  is used in the flux solution module in such a way that for the groups where there is no up-scattering, the thermal iteration is automatically deactivated. In the case where the SKIP option is activated, the  $p_{ij}^g$  matrix is used and thermal iterations are required in every energy group.

NORM	keyword to specify that the collision probability matrix is to be normalized in such a way as to eliminate all neutron loss (even if the region under consideration has external albedo boundary conditions which should result in neutron loss). When used with a void boundary condition (zero reentrant current), this option is equivalent to imposing <i>a posteriori</i> a uniform reentrant current.
ALBS	keyword to specify that a consistent Selengut normalization of the collision probability matrix is to be used both for the flux solution module (see Section 3.7) and in the equivalence calculation (see Section 3.9). This keyword results in storing the escape probabilities $P_{iS}$ in <i>PIJNAM</i> . For all the cases where this option is used, it is necessary to define a geometry with VOID external boundary conditions (see Section 3.3).
NAME	keyword to specify that the complete collision probability matrices are to be computed even if they are not required in the flux solution module (keyword <i>PIJ</i> or <i>SKIP</i> absent) and stored under a specific name on <i>PIJNAM</i> .
NMPIJ	name under which the complete collision probability matrices are saved.
PNOR	keyword to specify that the collision, leakage and escape probability matrices are to be normalized in such a way as to satisfy explicitly the neutron conservation laws. This option compensates for the errors that arise due to the numerical evaluation of the probabilities that may result in non-conservative collision probability matrices. The default option is now <i>HELI</i> ..
NONE	keyword to specify that the probability matrices are not to be normalized for neutron conservation.
DIAG	keyword to specify that only the diagonal element of the probability matrices will be modified in order to insure the validity of the conservation laws.
GELB	keyword to specify that the Gelbard algorithm will be used to normalize the collision probability matrices. <sup>[65]</sup>
HELI	keyword to specify that the HELIOS algorithm will be used to normalize the collision probability matrices. <sup>[66]</sup>
NONL	keyword to specify that a non linear multiplicative algorithm will be used to normalize the collision probability matrices. <sup>[65]</sup>
ALLG	keyword to specify that the contribution of a tracking line to the multigroup collision probabilities will be processed before the next tracking line is analyzed. This means that for a multigroup problem the tracking file is read once. The default option is to generate the collision probability matrices group by group implying multiple readings of the tracking file. The major drawback of using the <i>ALLG</i> keyword is that the space requirement for the problem is $N \times N \times G$ for a $N$ region $G$ groups problem while only a $N \times N$ array is required when this option is not activated.

### 3.6.2 Data input for module EXCELL :

Table 42: Structure (**descXL**)

TRAK [ SUBG <i>nsubg</i> ]
----------------------------

continued on next page

Structure (**descXL**)

continued from last page

```
[ PNOR { NONE | DIAG | GELB | HELI | NONL } ]
[ [ NORM ] ALBS ] [ SKIP ]
TISO nangl dens [ CORN pcorn ] [ SYMM isymm ]
```

where

**SUBG** keyword to specify the number of groups in each subgroup for collision probability calculations.

*nsubg* number of groups in each subgroup in collision probability calculations. The default value is the total number of groups contained in the *LIBNAM* object. However, in applications needing a large amount of memory to store group-dependent collision probability, this number can be smaller (the minimal value is indeed 1). In all cases, the tracking file is rebuilt for every subgroup, and the collision probability matrices are computed by block of *nsubg* groups until all groups are processed.

All other keywords and values have already been defined in the previous section (see Section 3.6.1) or in the **EXCEL T**: section (see Section 3.4.2). Note that the **EXCELL**: module is limited to 3-D geometries.

### 3.7 The **FLU**: module

The **FLU**: module is used to solve the linear system of multigroup collision probability or response matrix equations in DRAGON. The calling specifications are:

Table 43: Structure (**FLU**:)

```
FLUNAM := FLU: [ FLUNAM ] PIJNAM LIBNAM TRKNAM :: (descflu)
```

where

*FLUNAM* character\*12 name of the FLUXUNK data structure containing the solution. If *FLUNAM* appears on the RHS, the solution previously stored in *FLUNAM* can be used to initialize the new iterative process.

*PIJNAM* character\*12 name of the ASMPIJ data structure containing the group dependent system matrices (see Section 3.6).

*LIBNAM* character\*12 name of the MACROLIB or MICROLIB data structure that contains the macroscopic cross sections (see Sections 3.1 and 3.2).

*TRKNAM* character\*12 name of the TRACKING data structure containing the tracking (see Section 3.4).

**(descflu)** structure containing the input data to this module (see Section 3.7.1).

#### 3.7.1 Data input for module **FLU**:

Table 44: Structure (**descflu**)

```

[ EDIT iprint ]
[ INIT { OFF | ON ((fluxes(i, g), i=1,nregion ), g=1,ngroup ) } ]
[ { FLX | PAF | AF } ]
TYPE { N | S | K [ (descleak) ] | { B | L } (descleak) } ]
[ THER [ maxthr ] [ epsthr ] ]
[ EXTE [ maxout ] [ epsout ] ]
[ UNKT [ epsunk ] ]
[ REBA [ OFF ] ]
[ ACCE nlibre naccel ]
[ EGPA epsgpa ] [ CGPA congpa ] [ DECO { ON | OFF } ]

```

where

EDIT	keyword used to modify the print level <i>iprint</i> .
<i>iprint</i>	index used to control the printing of this module. The amount of output produced by this tracking module will vary substantially depending on the print level specified.
INIT	keyword to specify the neutron flux initialization option used.
OFF	keyword to specify that the initial neutron flux distribution is not to be initialized.
ON	keyword to specify that the initial neutron flux distribution follows.
<i>fluxes</i>	array of average flux per region and per group.
FLX	keyword to specify that a flux solution is to be considered. This is the default option.
PAF	keyword to specify that a pseudo-adjoint flux solution is to be considered. <sup>[42]</sup>
AF	keyword to specify that a pseudo-adjoint flux solution is to be considered and that both the pseudo-adjoint and adjoint flux are to be saved on the FLUXUNK data structure.
TYPE	keyword to specify the type of flux or adjoint calculation to be performed.
N	keyword to specify that no flux calculation is to be performed. This option is usually activated when one simply wishes to initialize the neutron flux distribution and to store this information in <i>FLUNAM</i> (see ON parameter above).
S	keyword to specify that a fixed source problem is to be treated. Such problem can also include fission source contributions.
K	keyword to specify that a fission source eigenvalue problem is to be treated. The eigenvalue is then the effective multiplication factor with a fixed buckling. In this case, the fixed source, if any is present on the MACROLIB or MICROLIB data structure, is not used.
B	keyword to specify that a fission source eigenvalue problem is to be treated. The eigenvalue in this case is the critical buckling with a fixed effective multiplication factor. The buckling eigenvalue has meaning only in the case of a cell without leakages (see the structure ( <b>descBC</b> ) in Section 3.3.2). It is also possible to use an open geometry with VOID boundary conditions provided it is closed by the <b>ASM:</b> module (see Section 3.6.1) using the keywords NORM or ALSB.

L	keyword to specify that an eigenvalue problem for a non multiplicative medium is to be treated. The eigenvalue in this case is the critical buckling. The buckling eigenvalue has meaning only in the case of a cell without leakages (see the structure ( <b>descBC</b> ) in Section 3.3.2). It is also possible to use an open geometry with VOID boundary conditions provided it is closed by the <b>ASM:</b> module (see Section 3.6.1) using the keywords <b>NORM</b> or <b>ALSB</b> .
( <b>descleak</b> )	structure describing the general leakage parameters options (see Section 3.7.2).
THER	keyword to specify that the control parameters for the thermal iterations are to be modified.
maxthr	maximum number of thermal iterations. The fixed default value is $2 \times ngroup - 1$ (using scattering modified CP) or $4 \times ngroup - 1$ (using standard CP).
epsthr	convergence criterion for the thermal iterations. The fixed default value is $5.0 \times 10^{-5}$ .
EXTE	keyword to specify that the control parameters for the external iteration are to be modified.
maxout	maximum number of external iterations. The fixed default value for a case with no leakage model is $2 \times n_f - 1$ where $n_f$ is the number of regions containing fuel. The fixed default value for a case with a leakage model is $10 \times n_f - 1$ .
epsout	convergence criterion for the external iterations. The fixed default value is $5.0 \times 10^{-5}$ .
UNKT	keyword to specify that the flux/current error tolerance in the outer iteration.
epsunk	convergence criterion for flux/current in the outer iteration. The fixed default value is $epsunk = epsthr$ .
REBA	keyword used to specify that the flux rebalancing option is to be turned on or off in the thermal iteration. By default (floating default) the flux rebalancing option is initially activated. This keyword is required to toggle between the on and off position of the flux rebalancing option.
OFF	keyword used to deactivate the flux rebalancing option. When this keyword is absent the flux rebalancing option is reactivated.
ACCE	keyword used to modify the variational acceleration parameters. This option is active by default (floating default) with $nlibre=3$ free iterations followed by $naccel=3$ accelerated iterations.
nlibre	number of free iterations per cycle of $nlibre + naccel$ iterations.
naccel	number of accelerated iterations per cycle of $nlibre + naccel$ iterations. Variational acceleration may be deactivated by using $naccel=0$ . This is required when the <b>NOR2</b> is used in the <b>ASM:</b> module (see Section 3.6.1).
EGPA	keyword to specify that the control parameters for the generalized adjoint flux iteration are to be modified.
epsgps	relative convergence criterion for the adjoint flux. The explicit convergence criteria for the generalized adjoint will be given by $epsgps \times epsunk$ . By default, $epsgps=10$ .
CGPA	keyword to specify the contamination factor for the generalized adjoint.
congpa	contamination factor for the adjoint flux. By default, $congpa=100$ .
DECO	keyword to activate or deactivate the decontamination option.
OFF	keyword used to deactivate the decontamination option.
ON	keyword used to activate the decontamination option.

## 3.7.2 Leakage model specification structure

The **(descleak)** structure allows the following information to be specified:

Table 45: Structure **(descleak)**

```
{ LKRD | P0 | P1 | B0 | B1 | B0TR }
{ SIGS | PNL | ALBS | HETE [ { G | R | Z | X | Y } ] }
[ { BUCK { valb2 | [ G valb2 ] [ R valbr2 ] [ Z valbz2 ] [ X valbx2 ] [ Y valby2 ] } |
  KEFF valk | IDEM [ { B2 | DB2 } ] } ]
```

LKRD	keyword used to specify that the leakage coefficients are recovered from data structure named <i>FLUNAM</i> .
P0	keyword used to specify that the leakage coefficients are calculated using a $P_0$ model.
P1	keyword used to specify that the leakage coefficients are calculated using a $P_1$ model.
B0	keyword used to specify that the leakage coefficients are calculated using a $B_0$ model. This is the default value when a buckling calculation is required (B).
B1	keyword used to specify that the leakage coefficients are calculated using a $B_1$ model.
B0TR	keyword used to specify that the leakage coefficients are calculated using a $B_0$ model with transport correction.
SIGS	keyword used to specify that an homogeneous buckling correction is to be applied on the diffusion cross section ( $\Sigma_s - dB^2$ ).
PNL	keyword used to specify that the elements of the collision probability (SKIP) or the scattering modified collision probability matrix are multiplied by the adequate non leakage homogeneous buckling dependent factor. <sup>[67]</sup> This is the default option when a buckling calculation is required (B) or a fission source eigenvalue problem (K) with imposed buckling is considered.
ALBS	keyword used to specify that an homogeneous buckling contribution is introduced by a group dependent correction of the albedo. <sup>[68]</sup> It is then necessary to define the geometry with an external boundary condition of type VOID (see Section 3.3.2) and to close the region in module <b>ASM</b> : using the ALBS option (see Section 3.6.1).
HETE	keyword used to specify that the leakage and anisotropic effects will be taken into account using a consistent $P_n$ <sup>[69]</sup> or a $B_n$ <sup>[70,71]</sup> model. The heterogeneous buckling contribution is introduced in the $B_n$ model using the PIJK method. It is activated only if ANIS 2 is specified in module <b>EXCELT</b> : (see Section 3.4.2) and the option PIJK is used in module <b>ASM</b> : (see Section 3.6.1). Otherwise, a consistent $P_n$ model is used.
G	keyword used to specify that the buckling search will assume all directional buckling to be identical (floating default option).
R	keyword used to specify that a radial buckling search will be considered assuming an imposed $Z$ direction buckling.

<b>Z</b>	keyword used to specify that a <i>Z</i> direction buckling search will be considered assuming an imposed <i>X</i> direction and <i>Y</i> direction buckling.
<b>X</b>	keyword used to specify that a <i>X</i> direction buckling search will be considered assuming an imposed <i>Y</i> direction and <i>Z</i> direction buckling.
<b>Y</b>	keyword used to specify that a <i>Y</i> direction buckling search will be considered assuming an imposed <i>X</i> direction and <i>Z</i> direction buckling.
<b>BUCK</b>	keyword used to specify the initial (for a buckling eigenvalue problem) or fixed (for a effective multiplication constant eigenvalue problem) buckling.
<b>G</b>	keyword used to specify that the buckling in the <i>X</i> direction, <i>Y</i> direction and <i>Z</i> direction are to be initialized to <i>valb2</i> /3 (floating default).
<b>R</b>	keyword used to specify that the buckling in the <i>X</i> direction, and <i>Y</i> direction are to be initialized to <i>valbr2</i> /2.
<b>Z</b>	keyword used to specify that the buckling in the <i>Z</i> direction, is to be initialized to <i>valbz2</i> .
<b>X</b>	keyword used to specify that the buckling in the <i>X</i> direction, is to be initialized to <i>valbx2</i> .
<b>Y</b>	keyword used to specify that the buckling in the <i>Y</i> direction, is to be initialized to <i>valby2</i> .
<b>valb2</b>	value of the fixed or initial total buckling in $\text{cm}^{-2}$ . The floating default value is $\text{valb2} = \text{valbx2} + \text{valby2} + \text{valbz2}$
<b>valbr2</b>	value of the fixed or initial radial buckling in $\text{cm}^{-2}$ . The floating default value is $\text{valbr2} = \text{valbx2} + \text{valby2}$
<b>valbz2</b>	value of the fixed or initial <i>Z</i> direction buckling in $\text{cm}^{-2}$ . By default <i>valbz2</i> =0.0 $\text{cm}^{-2}$ . If <i>valb2</i> is specified then <i>valbz2</i> = <i>valb2</i> /3.
<b>valbx2</b>	value of the fixed or initial <i>Z</i> direction buckling in $\text{cm}^{-2}$ . By default <i>valbx2</i> =0.0 $\text{cm}^{-2}$ . If <i>valb2</i> is specified then <i>valbx2</i> = <i>valb2</i> /3. If <i>valbr2</i> is specified then <i>valbx2</i> = <i>valbr2</i> /2.
<b>valby2</b>	value of the fixed or initial <i>Z</i> direction buckling in $\text{cm}^{-2}$ . By default <i>valby2</i> =0.0 $\text{cm}^{-2}$ . If <i>valb2</i> is specified then <i>valby2</i> = <i>valb2</i> /3. If <i>valbr2</i> is specified then <i>valby2</i> = <i>valbr2</i> /2.
<b>KEFF</b>	keyword used to specify the fixed (for a buckling eigenvalue problem) effective multiplication constant.
<b>valk</b>	value of the fixed effective multiplication constant. The fixed default value is <i>valk</i> =1.0.
<b>IDEM</b>	keyword used to specify that the initial (for a buckling eigenvalue problem) or fixed (for a effective multiplication constant eigenvalue problem) leakage is to be read from the data structure <i>FLUNAM</i> .
<b>B2</b>	keyword used to specify that only the buckling is to be read from the data structure <i>FLUNAM</i> . This is the default value.
<b>DB2</b>	keyword used to specify that the initial buckling and diffusion coefficients are to be read from the data structure <i>FLUNAM</i> .

### 3.8 The MOCC: and MCU: modules

The MOCC: and MCU modules can be used respectively to solve the transport equation using the method of cyclic characteristics<sup>[34,35]</sup> or the method of characteristics in 3-D geometry.<sup>[36-38]</sup> The calling specifications are:

Table 46: Structure (**MOCC:**)

<i>FLUNAM</i> := <b>MOCC:</b> [ <i>FLUNAM</i> ] <i>LIBNAM</i> <i>TRKNAM</i> <i>TRKFIL</i> :: ( <b>descmoc</b> )
---

and

Table 47: Structure (**MCU:**)

{ <i>FLUNAM</i> <i>TRKNAM</i> := <b>MCU:</b> [ <i>FLUNAM</i> ] <i>GEONAM</i> <i>LIBNAM</i> <i>TRKFIL</i> :: ( <b>descmcu</b> ) ( <b>desctrak</b> )   <i>FLUNAM</i> := <b>MCU:</b> [ <i>FLUNAM</i> ] <i>TRKNAM</i> <i>TRKFIL</i> <i>LIBNAM</i> :: ( <b>descmcu</b> ) }
--

where

<i>FLUNAM</i>	<b>character*12</b> name of the FLUXUNK data structure containing the solution. If <i>FLUNAM</i> appears on the RHS, the solution previously stored in <i>FLUNAM</i> is used to initialize the iterative process.
<i>LIBNAM</i>	<b>character*12</b> name of the MACROLIB or MICROLIB data structure that contains the macroscopic cross sections (see Sections 3.1 and 3.2).
<i>TRKNAM</i>	<b>character*12</b> name of the TRACKING data structure containing the tracking (see Section 3.4).
<i>TRKFIL</i>	<b>character*12</b> name of the sequential binary tracking file used to store the tracks lengths. This file is given if and only if it was required in the previous tracking module call (see Section 3.4).
<i>GEONAM</i>	<b>character*12</b> name of GEOMETRY data structure that contains a physical description of the problem to be solved.
( <b>descmoc</b> )	structure containing the input data to the <b>MOCC:</b> module (see Section 3.8.1).
( <b>descmcu</b> )	structure containing the input data to the <b>MCU:</b> module (see Section 3.8.2).
( <b>descexcel</b> )	structure containing the input data for tracking the geometry (see Section 3.4.2).

### 3.8.1 Data input for module **MOCC:**

Table 48: Structure (**descmoc**)

[ <b>EDIT</b> <i>iprint</i> ]
[ <b>EXAC</b> ]
[ <b>NBPN</b> <i>nl</i> ]

continued on next page

Structure (**descmoc**)

continued from last page

```

TYPE { N | S | K [ (descleak) ] | B [ (descleak) ] }
[ THER [ maxthr ] [ epsthr ] ]
[ EXTE [ maxout ] [ epsout ] ]
[ UNKT [ epsunk ] ]
[ NOBA ]
[ ACCE nlibre naccel ]

```

where

**EXAC** keyword used to specify that exact exponential functions are to be used for neutron path attenuation. By default, approximate values for the exponential function derived from second order local polynomials are considered.

**NBPN** keyword used to specify the expansion order in Legendre polynomial for the flux used in the calculation.

*nl* the expansion order in Legendre polynomial for the flux used in the calculation. By default *nl*=0.

and the remaining options are described in Section 3.7.1.

### 3.8.2 Data input for module MCU :

Table 49: Structure (**descmcu**)

```

[ EDIT iprint ]
TYPE { N | S | K [ (descleak) ] | B [ (descleak) ] }
[ THER [ maxthr ] [ epsthr ] ]
[ EXTE [ maxout ] [ epsout ] ]
[ NOBA ]
[ ACCE nlibre naccel ] [ SCR maxscr ] [ ETAB ON OFF ] [ ITLM ]

```

where

**SCR** keyword used to modify the number of iterations in the self-collision rebalancing procedure.

*maxscr* the number of iterations in the self-collision rebalancing procedure. The default value is *maxscr*=5.

**ETAB** keyword to specify the option for using exponential tables.

*ON* to specify that the exponential tables will be used.

*OFF* to specify that the exponential tables will not be used.

**ITLM** keyword to specify that the effective number of thermal iteration  $m$  at outer iteration  $n$  is  $m = \min(n, \text{maxthr})$  where  $\text{maxthr}$  is the maximum number of thermal iterations.

and the remaining options are described in Section 3.7.1.

### 3.9 The **EDI:** module

The **EDI:** module supplies the main editing options to DRAGON. It can be use to compute the reaction rates, average and condensed cross sections and to store the information on a file for further use. The calling specifications are:

Table 50: Structure (**EDI:**)

```
EDINAM := EDI: [ EDINAM ] FLUNAM LIBNAM TRKNAM [ REFGEOM REFPIJ [ { SPHGEOM | SPH-
TRK SPHLINE } ] ] :: (descedi)
```

where

<b>EDINAM</b>	character*12 name of the EDITION data structure where the edition results will be stored.
<b>FLUNAM</b>	character*12 name of the FLUXUNK data structure containing a transport solution (see Section 3.7).
<b>LIBNAM</b>	character*12 name of the MACROLIB or MICROLIB data structure that contains the macroscopic cross sections (see Sections 3.1 and 3.2).
<b>TRKNAM</b>	character*12 name of the TRACKING data structure containing the tracking (see Section 3.4).
<b>REFGEOM</b>	character*12 optional name of the GEOMETRY data structure that was used for the original flux calculation (see Section 3.3). Required for SPH homogenization calculations.
<b>REFPIJ</b>	character*12 optional name of the ASMPIJ data structure that was used for the original flux calculation (see Section 3.6). Required for involving SPH homogenization calculations.
<b>SPHGEOM</b>	character*12 optional name of the GEOMETRY data structure that can be used in the SPH equivalence procedure. In some cases the module <b>EDI:</b> can automatically build a macro geometry, however it is always preferable to specify explicitly the macro geometry or the macro tracking to be used.
<b>SPHTRK</b>	character*12 optional name of the TRACKING data structure that will be used in the SPH equivalence procedure.
<b>SPHLINE</b>	character*12 optional name of the tracking file to used in the SPH equivalence procedure.
<b>(descedi)</b>	structure containing the input data to this module (see Section 3.9.1).

#### 3.9.1 Data input for module **EDI:**

Table 51: Structure (**descedi**)

```

[ EDIT iprint ]
[ P1SCAT { FLUX | CURRENT | COHERENT | DIRECTION } ]
[ UPS ]
[ MERG { COMP | NONE | GEO |
        REGI (iregm(i), i = 1, Nr) |
        MIX (imixm(i), i = 1, Nm) } ]
[ TAKE {
        REGI (iregt(i), i = 1, Nr) |
        MIX (imixt(i), i = 1, Nm) } ]
[ { POW | P1W } ]
[ COND { NONE | ( { icond(g) | energy(g) }, g = 1, Ng) } ]
[ MICR [ ISOT ] { ALL | NONE | nis (HISO(i), i=1,nis) } ]
[ FLIB [ ISOT ] { ALL | NONE } ]
[ ACTI [ ISOT ] { NONE | (imixa(i), i = 1, Nm) } ]
[ SAVE [ ON { DIRN | idirn } ] ]
[ PERT ]
[ STAT { ALL | RATE | FLUX | DELS } [ REFE { DIRO | idiro } ] ]
[ NBAL ]
[ SPH (descsph) ]

```

where

**EDIT** keyword used to modify the print level *iprint*.

*iprint* index used to control the printing of this module. The *iprint* parameter is important for adjusting the amount of data that is printed by this calculation step:

- *iprint*=0 results in no output;
- *iprint*=1 results in the average and integrated flux being printed (floating default);
- *iprint*=2 results in the reaction rates being printed;
- *iprint*=3 is identical to the previous option, but the condensed and/or homogenized vector cross sections are also printed;
- *iprint*=4 is identical to the previous option, but the condensed and/or homogenized scattering cross sections are also printed.

**P1SCAT** keyword to specify the type of homogenization to be considered for the anisotropic component of the scattering cross section.

**FLUX** keyword to specify the flux/volume homogenization for the anisotropic component of the scattering cross section. This is the default option technique used when no leakage model is used.

**CURRENT** keyword to specify the current/volume homogenization for the anisotropic component of the scattering cross section. This is the default option technique used when an homogeneous leakage model is used.

**COHERENT** keyword to specify a coherent directional averaged current/volume homogenization for the anisotropic component of the scattering cross section.<sup>[72]</sup>

DIRECTION	keyword to specify a coherent directional current/volume homogenization for the anisotropic component of the scattering cross section. This is the default technique used when an heterogeneous leakage model is used. <sup>[73]</sup>
UPS	keyword to specify that the reaction rates and the condensed and/or homogenized cross sections are corrected so as to eliminate up-scattering. This option is useful for reactor analysis codes that cannot take into account such cross sections.
NONE	keyword to deactivate the effect of previous use of a the preceding keyword.
MERG	keyword to specify that the neutron flux is to be homogenized over specified regions or mixtures.
COMP	keyword to specify that a complete homogenization is to take place.
GEO	keyword to specify that the homogenization region will be selected by comparing a calculation geometry with an homogenization geometry. Only a reduced number of EXCELT: geometries can now be processed using this option.
REGI	keyword to specify that the homogenization of the neutron flux will take place over the specific regions. Here $N_r \leq \text{maxreg}$ with <i>maxreg</i> the maximum number of regions for which solutions were obtained.
<i>iregm</i>	array of homogenized region numbers to which are associated the regions used for the flux calculation. In the editing routines a value of <i>iregm</i> =0 allows the corresponding region to be neglected.
MIX	keyword to specify that the homogenization of the neutron flux will take place over the following mixtures. Here we must have $N_m \leq \text{maxmix}$ where <i>maxmix</i> is the maximum number of mixtures in the macroscopic cross section library.
<i>imixm</i>	array of homogenized region numbers to which are associated the isotopic mixtures. In the editing routines a value of <i>imixm</i> =0 allows the corresponding isotopic mixtures to be neglected. For a mixture in this library that is not used in the geometry one should insert a value of 0 for the new region number associated with this mixture.
TAKE	keyword to specify that the neutron flux is to be edited over specified regions or mixtures.
REGI	keyword to specify that the editing of the neutron flux will take place over the following regions. Here $N_r \leq \text{maxreg}$ with <i>maxreg</i> the maximum number of regions for which solutions were obtained.
<i>iregt</i>	regions where the editing will take place. The new region numbers associated with these editing regions are numbered sequentially.
MIX	keyword to specify that the homogenization of the neutron flux will take place over the following mixtures. Here we must have $N_m \leq \text{maxmix}$ where <i>maxmix</i> is the maximum number of mixtures in the macroscopic cross section library.
<i>imixt</i>	mixtures where the editing will take place. Each mixture used here must be used in the geometry on is considering.
POW	keyword to specify that the $P_1$ information is to be homogenized and condensed using the scalar flux. This is the default option.
P1W	keyword to specify that the $P_1$ information is to be homogenized and condensed using a current recovered from a consistent $P_1$ or from a consistent heterogeneous $B_1$ model.
COND	keyword to specify that a group condensation of the flux is to be performed.

<i>icond</i>	array of increasing energy group limits that will be associated with each of the $N_g$ condensed groups. The final value of <i>icond</i> will automatically be set to <i>ngroup</i> while <i>icond</i> > <i>ngroup</i> will be dropped from the condensation. We must have $N_g \leq ngroup$ .
<i>energy</i>	array of decreasing energy limits (in eV) that will be associated with each of the $N_g$ condensed groups. We must have $N_g \leq ngroup+1$ . Note that if an energy limit is located between two energy groups, the condensation group will include this associated energy group. In the case where two energy limits fall within the same energy group the lowest energy will be dropped. Finally the maximum and minimum energy limits can be skipped since they will be taken automatically from the information available in the library.
MICR	keyword to specify that the condensation and homogenization procedure will be used to associate microscopic cross sections to the isotopes present in the homogenized regions. The macroscopic cross sections and the diffusion coefficients are weighted by the multigroup flux appearing in the regions where the isotopes are present. The resulting nuclear properties are saved on <i>EDINAM</i> when the <i>SAVE</i> keyword is present.
FLIB	keyword similar MICR except that the burnup chain are also saved on <i>EDINAM</i> when the <i>SAVE</i> keyword is present. In addition one fission spectrum per fissile isotope is generated rather than the unique fission spectrum for all fissile isotopes generated when MICR is used. The use of this keyword is required if burnup using the condensed and homogenized library is to be considered since in this case the file <i>EDINAM</i> contains a MICROLIB.
ALL	keyword to specify that all the isotopes present in the homogenized region are to be processed.
<i>nis</i>	number of isotopes isotopes present in the homogenized region to be processed.
<i>HISO</i>	array of <i>character*8</i> isotopes names to be processed.
ACTI	keyword to specify that microscopic activation data will be edited for the isotopes associated with the specified mixture. This information correspond to the microscopic cross section associated with each isotope in a given macro group and macro region assuming a concentration for this isotope of $1.0 \text{ cm}^{-3}$ in each region. This keyword is followed by <i>nacti</i> material mixture indices, where $nacti \leq maxmix$ .
<i>imixa</i>	array of material mixture indices which contains the isotopes for which activation data is to be generated. $nmix \leq maxmix$ . Even mixture not used in the geometry can be considered here.
ISOT	keyword to specify that the set of microscopic cross section generated by the FLIB, MICR and ACTI command will also be saved on a microscopic group neutron cross section library in the ISOTXS-IV format. This will generate a file for each final region specified by the TAKE or MERG keyword, numbered consecutively (IFILE). The name of the file (NISOTXS) is built using the command  <pre>WRITE(NISOTXS, '(A6,I6.6)') 'ISOTXS', IFILE</pre>
SAVE	keyword to specify that the flux, the macroscopic and microscopic cross sections and the volumes corresponding to homogenized regions are to be saved on <i>EDINAM</i> . In the case where the FLIB option is activated, the saved information is in the form of a MICROLIB, otherwise a MACROLIB is store on a subdirectory of EDITION.
ON	keyword to specify on which directory of <i>EDINAM</i> this information is to be stored.
<i>DIRN</i>	name of the directory on which the above information is to be stored.
<i>idirn</i>	number associated with a directory of <i>EDINAM</i> on which the above information is to be stored. To each number <i>idirn</i> is associated a directory name CDIRN defined as

```
WRITE(CDIRN, '(A8,I4)') 'REF-CASE', idirn
```

<b>PERT</b>	keyword to specify that first order perturbations for the microscopic cross sections are to be saved on <i>EDINAM</i> .
<b>STAT</b>	keyword to specify that a comparison between the current and a reference set of reaction rates and/or integrated flux is to be performed.
<b>ALL</b>	keyword to specify that the relative differences in the reaction rates and the integrated flux are to be printed.
<b>RATE</b>	keyword to specify that the relative differences in the reaction rates are to be printed.
<b>FLUX</b>	keyword to specify that the relative differences in the integrated flux are to be printed.
<b>DELS</b>	keyword to specify that the absolute differences in the macroscopic cross section are to be printed.
<b>REFE</b>	keyword to specify the directory of <i>EDINAM</i> where the reference data requires for the comparison is stored. When this keyword is absent, the last reaction rates and integrated flux saved on <i>EDINAM</i> are used.
<b>DIRO</b>	name of the directory from which the reference information is taken.
<i>idiro</i>	number associated with an directory of <i>EDINAM</i> on which the reference information is stored. To each number <i>idirn</i> is associated a the directory <i>CDIRN</i> defined using:

```
WRITE(CDIRN, '(A8,I4)') 'REF-CASE', idirn
```

<b>NBAL</b>	keyword to specify the editing of the four factors computed from a group balance. In this case, the user must specify explicitly a three group condensation.
<b>SPH</b>	keyword to specify that an equivalence calculation, between the current micro geometry and a macro geometry to be specified, is to be performed using the SPH technique. The resulting SPH factors are automatically used for the flux and the microscopic and macroscopic cross sections homogenization and condensation.
<b>(descsph)</b>	structure used to specify the information required for the SPH calculations (see Section 3.9.2).

### 3.9.2 Description of the equivalence information

This structure is used to specify the type of equivalence calculation where the flux and the condensed and/or homogenized cross sections are corrected by SPH factors, in such a way as to respect a specified transport-transport or transport-diffusion equivalence criteria.<sup>[67,68,74]</sup> This structure is defined as:

Table 52: Structure (**descsph**)

```
[ SELE ] [ MGEO MACGEO ]
{ OFF | MTRK | SPRD SPHNAM | HOMO | ALBS |
  :: EXCELT: (desctrack) (descexcel) |
  :: NXT: (desctrack) (descnxt) |
  :: SYBILT: (desctrack) (descsybil) |
  :: JPMT: (desctrack) (descjpm) |
  :: BIVACT: (desctrack) (descbivac) }
```

where

<b>SELE</b>	keyword to specify the use of Selengut normalization. In all cases where this option is used it is necessary to define the geometry with <b>VOID</b> external boundary conditions (see Section 3.3.2) and to close the region for the collision probability calculations using the <b>ALBS</b> option (see Section 3.6.1).
<b>MGEO</b>	keyword to specify the macro geometry to be used. In some special cases where 2-D Cartesian assemblies are considered, a macro geometry named <b>SPH\$GEO</b> can be automatically constructed by homogenizing the sub-geometries in a geometry. However, for most problems this is not the case and the macro geometry should be specified explicitly.
<b>MACGEO</b>	<b>character*12</b> name of the macro geometry to use. This name should be identical to <b>SPH-GEO</b> .
<b>MTRK</b>	keyword to specify that the macro <b>TRACKING SPHTRK</b> and tracking file <b>SPHLINE</b> provided will be used for homogenization.
<b>OFF</b>	keyword to specify the SPH factors are all set to 1.0, meaning no correction. This is the floating default. This keyword is useful to get rid of a SPH correction which have been set by a previous <b>EDI:</b> call.
<b>SPRD</b>	keyword to specify the SPH factors are read on <b>EDINAM</b> .
<b>SPHNAME</b>	name of the directory from which the SPH factors are to be read.
<b>HOMO</b>	keyword to specify that the SPH factors are calculated assuming the macro geometry is equivalent to a complete homogenization of the current micro geometry. The options <b>MERG COMP</b> must then be specified. In this case the neutron flux (transport or diffusion) will be uniform, which allows the SPH factors to be obtained (one per macro group) using a direct strategy. For a given macro group the SPH factor will be equal to the ratio between the average flux of the region and the surface flux if the <b>SELE</b> option is used otherwise the SPH factor are all set equal to 1.0 (no correction). The <b>SELE</b> option allows an SPH factor equal to the inverse of the discontinuity factor to be calculated.
<b>ALBS</b>	keyword to specify that the albedo of the geometry are to be taken into account in the complete homogenization process. Thus the <b>MERG</b> and <b>COMP</b> options must be specified. The SPH factors are obtained using a transport-transport equivalence based on a calculation using the collision probabilities. This option requires a geometry with <b>VOID</b> (see Section 3.3.2) external boundary conditions to be closed using <b>ALBS</b> in modules <b>ASM:</b> and <b>FLU:</b> (see Sections 3.6.1 and 3.7.1). <sup>[68]</sup>
<b>EXCELT:</b>	keyword to specify that the SPH factors are obtained using a transport-transport equivalence calculation where the macro geometry is processed using the <b>EXCELT:</b> tracking module.
<b>NXT:</b>	keyword to specify that the SPH factors are obtained using a transport-transport equivalence calculation where the macro geometry is processed using the <b>NXT:</b> tracking module.
<b>SYBILT:</b>	keyword to specify that the SPH factors are obtained using a transport-transport equivalence calculation where the macro geometry is processed using the <b>SYBILT:</b> tracking module.
<b>JPMT:</b>	keyword to specify that the SPH factors are obtained using a transport-transport equivalence calculation where the macro geometry is processed using the <b>JPMT:</b> tracking module.
<b>BIVACT:</b>	keyword to specify that the SPH factors are obtained using a transport-diffusion equivalence calculation where the macro geometry is processed using the <b>BIVACT:</b> diffusion tracking module. This option requires to use one of the keywords <b>LKRD</b> , <b>P0</b> , <b>P1</b> , <b>B0</b> , <b>B1</b> or <b>B0TR</b> in the flux calculation (see Section 3.7.1) so as to supply diffusion coefficients.

<b>(desctrack)</b>	structure of the general tracking options (see Section 3.4.1).
<b>(descexcel)</b>	structure of the EXCELT: tracking options (see Section 3.4.2).
<b>(descnxt)</b>	structure of the NXT: tracking options (see Section 3.4.3).
<b>(descsybil)</b>	structure of the SYBILT: tracking options (see Section 3.4.4).
<b>(descjpm)</b>	structure of the JPMT: tracking options (see Section 3.4.5).
<b>(descbivac)</b>	structure of the BIVACT: tracking options (see Section 3.4.6).

### 3.10 The EVO: module

The EVO: module in DRAGON allows the isotopic densities and the macroscopic cross sections to be updated following a in-core (i.e., burnup) or out-of-core depletion. The general format of the data which is used to control the execution of the EVO: module is the following:

Table 53: Structure (EVO:)

```
BRNNAM MICNAM := EVO: [ BRNNAM ] { MICNAM | OLDMIC } TRKNAM [ FLUNAM ] ::
(descevo)
```

where

<b>BRNNAM</b>	character*12 name of the BURNUP data structure that will contain the depletion history as modified by the depletion module.
<b>MICNAM</b>	character*12 name of the MICROLIB that will contain the update macroscopic cross sections. If <i>MICNAM</i> appears on both LHS and RHS, it is updated; otherwise, the microcopic cross section library <i>OLDMIC</i> is copied in <i>MICNAM</i> and then updated.
<b>OLDMIC</b>	character*12 name of a read-only MICROLIB that is copied in <i>MICNAM</i> .
<b>TRKNAM</b>	character*12 name of a read-only TRACKING for the depleting geometry. This information is required both for in-core and out-of-core depletion cases.
<b>FLUNAM</b>	character*12 name of a read-only FLUXUNK. This information is used only for in-core depletion cases.
<b>(descevo)</b>	structure containing the input data to this module (see Section 3.10.1).

#### 3.10.1 Data input for module EVO:

Table 54: Structure (**evo**)

```

[ EDIT iprint ]
[ { SAVE xts { S | DAY | YEAR } [ { FLUX flux | POWR power | W/CC wcc } ] | NOSA } ]
[ EPS1 valeps1 ] [ EPS2 valeps2 ] [ EXPM valexp ] [ H1 valh1 ]
[ { SATOFF | NSAT | SAT } ] [ { NODI | DIRA } ]
[ { TIXS | TDXS | NOEX } ]
[ { GLOB | NOGL } ]
[ EXTR ]
[ { RUNG | KAPS } ]
[ DEPL { xti xtf | dxt } { S | DAY | YEAR } [ { COOL | FLUX flux | POWR power | W/CC wcc } ] ]
[ SET xtr { S | DAY | YEAR } ]

```

where

**EDIT** keyword used to modify the print level *iprint*.

*iprint* index used to control the printing of the module. The amount of output produced by this tracking module will vary substantially depending on the print level specified.

**SAVE** keyword to specify that the results of the last transport calculation and the current isotopic concentration must be stored on *BRNNAM* on a sub-directory corresponding to a specific time. By default this data is stored at a time corresponding to *xti*.

**NOSA** keyword to specify that the results of the last transport calculation and the current isotopic concentration will not be stored on *BRNNAM*. By default this data is stored at a time corresponding to *xti*.

**SET** keyword used to recover the isotopic concentration already stored on *BRNNAM* on a sub-directory corresponding to a specific time. By default this data is recovered from a time corresponding to *xtf*.

**DEPL** keyword to specify that a burnup calculation between an initial and a final time must be performed. In the case where the **SAVE** keyword is absent, the initial isotopic concentration will be stored on *BRNNAM* on a sub-directory corresponding to the initial time. If the **SET** keyword is absent, the isotopic concentration corresponding to the final burnup time will be recovered from the *FLUXUNK* structure.

*xti* initial time associated with the burnup calculation. By default *xti* is the final time reached at the last depletion step. If this is the first depletion step, *xti*=0. The name of the sub-directory *EVONAM* where this information is stored will be given by

```
WRITE(EVONAM, '(A8,I4)') 'DEPL-DAT', inn
```

where *inn* is an index associated with the time *xti*. The initial values are recovered from this sub-directory in *BRNNAM*.

*dxt* time interval for burnup calculation. The initial time *xti* in this case is taken as the final time reached at the last burnup step. If this is the first depletion step, *xti*=0.

*xtf* end of time for the burnup calculation. The results of the isotopic depletion calculations are stored in the tables associated with a sub-directory whose name is constructed in the same manner as the *xti* input. In the case where the time interval *dxt* is provided then *xtf*=*xti*+*dxt*.

<i>xts</i>	time associated with the last transport calculation. The name of the sub-directory where this information is to be stored is constructed in the same manner as the for <i>x<sub>ti</sub></i> input. By default (fixed default) <i>x<sub>ts</sub></i> = <i>x<sub>ti</sub></i> .
<i>xtr</i>	time associated with the next flux calculation. The name of the sub-directory where this information is to be stored is constructed in the same manner as for the <i>x<sub>ti</sub></i> input. By default (fixed default) <i>x<sub>tr</sub></i> = <i>x<sub>tf</sub></i> .
<b>S</b>	keyword to specify that the time is given in seconds.
<b>DAY</b>	keyword to specify that the time is given in days.
<b>YEAR</b>	keyword to specify that the time is given in years.
<b>COOL</b>	keyword to specify that a zero flux burnup calculation is to be performed.
<b>FLUX</b>	keyword to specify that isotopic a constant flux burnup calculation is to be performed.
<i>flux</i>	flux expressed in $\text{cm}^{-2}\text{s}^{-1}$ . In the case where <i>flux</i> ≤ 0.0, the calculations are performed as if the COOL option was used.
<b>POWR</b>	keyword to specify that a constant power burnup calculation in KW/Kg is to be performed.
<i>power</i>	power expressed in KW/Kg = MW/tonne. In the case where <i>power</i> ≤ 0.0, the calculations are performed as if the COOL option was used.
<b>W/CC</b>	keyword to specify that a constant assembly power depletion calculation is to be performed. The energy released outside the fuel is always taken into account in the flux normalization.
<i>wcc</i>	power expressed in W/cm <sup>3</sup> .
<b>EPS1</b>	keyword to specify the tolerance used in the algorithm for the solution of the depletion equations.
<i>valeps1</i>	the tolerance used in the algorithm for the solution of the depletion equations. The default value is 10 <sup>-5</sup> .
<b>EPS2</b>	keyword to specify the tolerance used in the search algorithm for a final fixed power (used if the POWR option is activated).
<i>valeps2</i>	the tolerance used in the search algorithm for a final fixed power. The default value is 10 <sup>-4</sup> .
<b>EXPM</b>	keyword to specify the selection criterion for non-fissile isotopes that are at saturation.
<i>valexp</i>	the isotopes for which $\lambda \times (x_{tf} - x_{ti}) \geq \text{valexp}$ will be treated by a saturation approximation. Here, $\lambda$ is the sum of the radioactive decay constant and microscopic neutron absorption rate. The default value is 80.0. In order to remove the saturation approximation for all isotopes set <i>valexp</i> to a very large number such as 10 <sup>5</sup> or use the keyword <b>SATOFF</b> .
<b>SATOFF</b>	keyword to specify that the saturation model for the non-fissile isotopes will not be used.
<b>NSAT</b>	keyword to specify that the saturation model for the non-fissile isotopes will not be used. This keyword has the same effect as keyword <b>SATOFF</b> .
<b>SAT</b>	keyword to specify that the saturation model for the non-fissile isotopes will be used. This is the default option.
<b>NODI</b>	keyword to specify that no Dirac delta function will be used in the saturation model, namely for isotope <i>k</i> at saturation one uses

$$N_k(t) = \frac{S_k(t)}{\Lambda_k(t)}$$

**DIRA** keyword to specify that a Dirac delta function will be used in the saturation model, namely for isotope  $k$  at saturation one uses

$$N_k(t) = \frac{1}{\Lambda_k(t)} [a\delta(t - t_0) + S_k(t) + b\delta(t - t_f)]$$

This is the default option.

**H1** keyword to specify an estimate of the relative width of the time step used in the solution of burnup equations.

**valh1** relative width of the time step used in the solution of burnup equations. An initial time step of  $\Delta_t = \text{valh1} \times (xtf - xti)$  is used. This value will be optimized inside DRAGON to ensure that the solution to the depletion equations converges. The default value is  $10^{-4}$ .

**RUNG** keyword to specify a solution of the depletion equations using the 5<sup>th</sup> order Runge–Kutta algorithm.

**KAPS** keyword to specify a solution of the depletion equations using the 4<sup>th</sup> order Kaps–Rentrop algorithm.<sup>[75]</sup> This is the default value.

**TIXS** keyword that specified that time independent cross sections will be used. A time dependent flux distribution will also be considered. This is the default option when no time dependent cross sections are provided.

**TDXS** keyword that specified that time dependent cross sections will be used if available. This is the default option when time dependent cross sections are provided.

**NOEX** keyword that specified that time independent cross sections and fluxed will be used.

**GLOB** keyword to specify that the global energy produced will be taken into account if available. This is the default option.

**NOGL** keyword to specify that only the energy produced in the fuel will be taken into account even if energy production outside the fuel is available.

**EXTR** keyword for power extrapolation when fixed power burnup is selected.

### 3.11 The CPO: module

The CPO: module is used to generate the reactor cross-section database required for a full core calculation using DONJON.<sup>[47]</sup> The calling specifications are:

Table 55: Structure (CPO:)

**CPONAM := CPO: [ CPONAM ] EDINAM [ BRNNAM ] :: (desccpo)**

where

**CPONAM** character\*12 name of the CPO data structure containing the reactor database. Additional contributions can be included in the reactor cross-section database if CPONAM appears on the RHS.

<i>EDINAM</i>	character*12 name of the read-only EDITION data structure.
<i>BRNNAM</i>	character*12 name of the read-only BURNUP data structure containing the depletion history. This information is given only if the reactor database is to contain burnup dependent data.
<b>(descppo)</b>	structure containing the input data to this module (see Section 3.11.1).

### 3.11.1 Data input for module CPO:

Table 56: Structure **(descppo)**

```
[ EDIT iprint ]
[ B2 ] [ NOTR ]
{ STEP NOMDIR | BURNUP PREFIX }
[ [ EXTRACT { ALL | NEWNAME (OLDNAME(i), i=1,niext) } ] ]
[ NAME NDIR ]
```

where

<b>EDIT</b>	keyword used to modify the print level <i>iprint</i> .
<i>iprint</i>	index used to control the printing of this module. The amount of output produced by this tracking module will vary substantially depending on the print level specified.
<b>B2</b>	keyword to specify that the buckling correction ( $dB^2$ ) is to be applied to the cross section to be stored on the reactor database. By default (fixed default), such a correction is not taken into account.
<b>NOTR</b>	keyword to specify that the cross section to be stored on the reactor database are not to be transport corrected. By default (fixed default), transport corrected cross section are considered when the <b>CTRA</b> option is activated in <b>MAC:</b> or <b>LIB:</b> (see Sections 3.1 and 3.2).
<b>STEP</b>	keyword to specify that a specific cross section directory stored in <i>EDINAM</i> via the <b>SAVE</b> option in the <b>EDI:</b> module is to be transferred to <i>CPONAM</i> .
<i>NOMDIR</i>	character*12 name of the specific cross section directory to be treated.
<b>BURNUP</b>	keyword to specify that a chain of cross section directory stored in <i>EDINAM</i> via the <b>SAVE</b> option in the <b>EDI:</b> module will be transferred to <i>CPONAM</i> .
<i>PREFIX</i>	character*8 prefix name of the cross section directory to be treated. DRAGON will transfer into the reactor database all the directories with full name <i>NAMDIR</i> created using

```
WRITE (NAMDIR, ' (A8,I4) ' ) PREFIX,nb
```

where *nb* is an integer greater than 0 indicating the depletion step index.

<b>EXTRACT</b>	keyword to specify that the contribution of some isotopes to the macroscopic cross sections associated with each homogenized mixture should be extracted before being stored on the reactor database. The microscopic cross sections and concentrations associated with these isotopes should also be generated and stored on the reactor database.
<b>ALL</b>	keyword to specify that all the isotopes processed using the MICR option of the <b>EDI:</b> module should be extracted from the macroscopic cross sections associated with each homogenized mixture.
<b>NEWNAME</b>	<code>character*12</code> name under which a given set of extracted isotope will be stored on the reactor database.
<b>OLDNAME</b>	array of <code>character*8</code> name of isotopes to be extracted from the macroscopic cross section associated with each homogenized mixture.
<b>NAME</b>	keyword to specify the prefix for the name of the sub-directory where the information corresponding to a single homogenized region will be stored. The fixed default is <code>NDIR = 'COMPO~~~'</code> .
<b>NDIR</b>	<code>character*8</code> prefix for the name of the sub-directory. The complete name is constructed by the concatenation of <code>NDIR</code> with a four digit integer value.

### 3.12 The **INFO:** module

The **INFO:** module is mainly used to compute the number densities for selected isotopes at specific local conditions. The module can also be used to compute the water density  $\rho(T, P)$  according to the assumed temperature  $T$  and purity  $P$ . In that case, the compound water density for a mix of light and heavy water is

$$\rho(T, P) = \frac{100 \times \rho_{H_2O}(T) \rho_{D_2O}(T)}{P \rho_{H_2O}(T) + (1 - P) \rho_{D_2O}(T)}$$

Temperature tabulations for  $\rho_{H_2O}(T)$  and  $\rho_{D_2O}(T)$  are the same as those of the WIMS-AECL code.<sup>[32]</sup> The calling specifications are:

Table 57: Structure (**INFO:**)

<b>INFO: :: (descinfo)</b>
----------------------------

where

**(descinfo)** structure containing the input data to this module (see Section 3.12.1).

#### 3.12.1 Data input for module **INFO:**

Table 58: Structure (**descinfo**)

```
[ EDIT iprint ]
[ LIB: { DRAGON | MATXS | MATXS2 | WIMSD4 | WIMS | WIMSAECL } FIL: NAMEFIL ]
[ TMP: temp { K | C } ]
[ PUR: purity { WGT% | ATM% } ]
[ CALC DENS WATER >>dens<< ]
[ ENR: enrichment { WGT% | ATM% } ]
[[ ISO: nbiso (ISONAM(i), i=1,nbiso)
  { GET MASS (>>mass(i)<<, i=1,nbiso) | CALC WGT% {
    D2O >>nh1<< >>hd2<< >>no16<< |
    UO2 >>nu5<< >>hu8<< >>no16<< |
    THO2 >>nth2<< >>nu3<< >>no16<< } } ]]
```

where

<b>EDIT</b>	keyword used to modify the print level <i>iprint</i> .
<i>iprint</i>	index used to control the printing of the module. The amount of output produced by this tracking module will vary substantially depending on the print level specified.
<b>LIB:</b>	keyword to specify the type of library from which the isotopic mass ratio is to be read.
<b>DRAGON</b>	keyword to specify that the isotopic depletion chain or the microscopic cross sections are in the DRAGLIB format.
<b>MATXS</b>	keyword to specify that the microscopic cross sections are in the MATXS format of NJOY-II and NJOY-89.
<b>MATXS2</b>	keyword to specify that the microscopic cross sections are in the MATXS format of NJOY-91.
<b>WIMSD4</b>	keyword to specify that the isotopic depletion chain or the microscopic cross sections are in the WIMS-D4 format.
<b>WIMS</b>	keyword to specify that the isotopic depletion chain or the microscopic cross sections are in the WIMS-AECL format.
<b>WIMSAECL</b>	keyword to specify that the isotopic depletion chain or the microscopic cross sections are in the WIMS-AECL format.
<b>FIL:</b>	keyword to specify the name of the file where is stored the mass ratio data.
<b>NAMEFIL</b>	character*8 name of the library where the mass ratio are stored.
<b>TMP:</b>	keyword to specify the isotopic temperature.
<i>temp</i>	temperature given in Kelvin (K) or Celsius (C).
<b>PUR:</b>	keyword to specify the water purity, that is fraction of heavy water in a mix of heavy and light water.
<i>purity</i>	water purity in weight percent (WGT%) or atomic percent (ATM%).
<b>ENR:</b>	keyword to specify the fuel enrichment.

<i>enrichment</i>	fuel enrichment in weight percent (WGT%) or atomic percent (ATM%).
ISO:	keyword to specify an isotope list. This list will be used either for getting mass values of isotopes or for computing number densities.
<i>nbiso</i>	number of isotopic names used for a calculation (limited to $nbiso \leq 3$ ).
ISONAM	character*12 name of an isotope.
GET MASS	keyword to recover the mass values as written in the library. It returns the mass value of each isotope in the output parameter <i>mass</i> .
CALC	keyword to ask the module to compute some parametric values. It returns one value in the output parameter <i>dens</i> .
DENS WATER	set of keywords to recover the water density as a function of its temperature and purity. This option requires the setting of temperature and purity, and it does not affect any given list of isotope names.
WGT% D2O	keywords to recover 3 number densities for a compound mixture of heavy and light water. The isotope list is assumed to contain $^1\text{H}$ , $^2\text{D}$ and $^{16}\text{O}$ . Temperature and purity are supposed to be available. It returns concentration of these isotopes in the output parameters <i>nh1</i> , <i>nd2</i> and <i>no16</i> .
WGT% UO2	keywords to recover 3 number densities for a compound mixture of Uranium oxide. The isotope list is assumed to contain $^{235}\text{U}$ , $^{238}\text{U}$ and $^{16}\text{O}$ . The $^{235}\text{U}$ enrichment is supposed to be available. Note that the number densities will sum to 100. It returns concentration of these isotopes in the output parameters <i>nu5</i> , <i>nu8</i> and <i>no16</i> .
WGT% THO2	keywords to recover 3 number densities for a compound mixture of Thorium/Uranium oxide. The isotope list is assumed to contain $^{232}\text{Th}$ , $^{233}\text{U}$ and $^{16}\text{O}$ . The $^{233}\text{U}$ enrichment is supposed to be available. Note that the number densities will sum to 100. It returns concentration of these isotopes in the output parameters <i>nth2</i> , <i>nu3</i> and <i>no16</i> .

The INFO: module works the following way. For a given isotope list, the mass is extracted from the library or a calculation process is expected. Once this calculation is has been performed, it is possible to list other isotopes and ask for further calculations. Finally note that the number of output parameters (denoted by >> *param*<<) parameters must be equal to the number of isotopes names given, plus the water density when a command CALC DENS WATER is issued.

### 3.13 The CFC: module

The CFC: module is used to generate a Feedback Model database required for a full core calculation in DONJON.<sup>[39–41]</sup> The general specifications of this module are:

Table 59: Structure (CFC:)

```
CFCNAM := CFC: [ CFCNAM ]
          (CPONAM(i), i=1,28) :: (descfc)
```

where

**CFCNAM**      character\*12 name of the FBMXSDB data structure containing the Feedback Model reactor

database. The reactor database can be updated if *CFCNAM* appears on the RHS.

**CPONAM**      `character*12` name of read only CPO data structures. There are 28 different CPO data structures required here each containing respectively

1. the reactor reference cross section.
2. cell cross section for the first fuel temperature.
3. cell cross section for the second fuel temperature.
4. cell cross section for the first coolant temperature.
5. cell cross section for the second coolant temperature.
6. cell cross section for the first moderator temperature.
7. cell cross section for the second moderator temperature.
8. cell cross section for the first coolant density.
9. cell cross section for the second coolant density.
10. cell cross section for the first moderator density.
11. cell cross section for the second moderator density.
12. cell cross section for a different concentration of boron.
13. cell cross section for a different moderator purity.
14. cell cross section for a different concentration of xenon.
15. cell cross section for a different concentration of samarium.
16. cell cross section for a different concentration of neptunium.
17. cell cross section for the spectral mixed effect fuel/coolant density.
18. cell cross section for the spectral mixed effect coolant density/temperature.
19. cell cross section for low power history.
20. cell cross section for intermediate power history.
21. cell cross section for high power history.
22. reactor reference moderator cross section.
23. moderator cross section for the first moderator temperature.
24. moderator cross section for the second moderator temperature.
25. moderator cross section for the first moderator density.
26. moderator cross section for the second moderator density.
27. moderator cross section for a different concentration of boron.
28. moderator cross section for a different moderator purity.

**(descfc)**      structure containing the input data to this module (see Section 3.13.1).

### 3.13.1 Data input for module CFC:

Table 60: Structure (**descfc**)

[ <b>INFOR</b> <i>TITLE</i> ] [ <b>DNAME</b> <i>RNAME</i> ]
--

where

<b>INFOR</b>	keyword which allows to set the title.
<b>TITLE</b>	<code>character*72</code> title associated to the reactor database generated.
<b>DNAME</b>	keyword that permits to set a specific database name in the data structure.
<b>RNAME</b>	<code>character*12</code> name of the feedback database.

### 3.14 The **MRG:** module

The **MRG:** module is used to pre-homogenize a geometry after it has been tracked with the **EXCELT:** tracking module (see SectandTRKDatadescexcel).<sup>[76,77]</sup> The general specifications of this module are:

Table 61: Structure (**MRG:**)

<b>TRKNEW</b> <i>TFILNEW</i> := <b>MRG:</b> <i>TRKOLD</i> <i>TFIOLD</i> :: ( <b>descmrg</b> )
--

where

<b>TRKNEW</b>	<code>character*12</code> name of the new TRACKING data structure that will contain region volume and surface area vectors in addition to region identification pointers and other tracking information after the pre-homogenization process.
<b>TFILNEW</b>	<code>character*12</code> name of the new sequential binary tracking file used to store the tracks lengths after the pre-homogenization process has take place.
<b>TRKOLD</b>	<code>character*12</code> name of the old TRACKING data structure that will contain region volume and surface area vectors in addition to region identification pointers and other tracking information before the pre-homogenization process.
<b>TFIOLD</b>	<code>character*12</code> name of the old sequential binary tracking file used to store the tracks lengths before the pre-homogenization process has take place.
<b>(descmrg)</b>	structure containing the input data to this module (see Section 3.14.1).

#### 3.14.1 Data input for module **MRG:**

Table 62: Structure (**descmrg**)

```
[ EDIT iprint ]
[ REGI (irmrg(i), i=1,nreg) ]
[ SURF (ismrg(i), i=1,nsur) ]
```

where

<b>EDIT</b>	keyword used to modify the print level <i>iprint</i> .
<i>iprint</i>	index used to control the printing in this module. It must be set to 0 if no printing on the output file is required.
<b>REGI</b>	keyword to specify that regions will be pre-homogenized.
<i>irmrg</i>	new region numbers associated with old region numbers. Two or more regions can be combined together only if they contain the same mixture. The number <i>nreg</i> of region is that printed after the execution of the <b>EXCELT:</b> module.
<b>SURF</b>	keyword to specify that surfaces will be pre-homogenized.
<i>ismrg</i>	new surface numbers associated with old surface numbers. Two or more surfaces can be combined together only if they are associated with the same albedo. The number <i>nsur</i> of surfaces is that printed after the execution of the <b>EXCELT:</b> module.

### 3.15 The **PSP:** module

The **PSP:** module is used to generate a graphical file in a PostScript ASCII format for a DRAGON 2-D geometry which can be analyzed using the **EXCELT:** tracking module (see Sections 3.4 and 3.4.2). The module **PSP:** is based on the PSLOT FORTRAN library from Nova Southeastern University.<sup>[78]</sup> Since only a few routines PSLOT routines were required and because additional PostScript routine not present in the original package were needed, the routines have been completely readapted to DRAGON. These routines are no longer machine dependent. The PostScript files generated by DRAGON can be viewed by any PostScript viewer, such as Ghostview<sup>[79]</sup> or sent to a printer compatible with this language. In DRAGON the **PSP:** module is activated using the following list of commands:

Table 63: Structure (**PSP:**)

```
PSGEO := PSP: PSGEO { GEONAM | TRKNAM } [ FLUNAM ] :: (descpsp)
```

where

<i>PSGEO</i>	<b>character*12</b> name of the file that will contain the graphical description in a POSTSCRIPT format. This file must have a sequential ASCII format.
<i>GEONAM</i>	<b>character*12</b> name of a read-only GEOMETRY (see Section 3.3). This option can be used only with geometries that can be processed using the <b>EXCELT:</b> module.

<b>TRKNAM</b>	character*12 name of an EXCELL type read-only TRACKING (see Section 3.4). This structure must have been created using the EXCELT:, EXCELL: or NXT: modules.
<b>FLUNAM</b>	character*12 name of an optional read-only FLUXUNK (see Section 3.7). It is required only if a flux mapping plot is requested.
<b>(descpsp)</b>	structure containing the input data to this module (see Section 3.15.1).

### 3.15.1 Data input for module PSP:

Table 64: Structure **(descpsp)**

```
[ EDIT iprint ]
[ FILL { NONE | GRAY | RGB | CMYK | HSB } [ NOCONTOUR ] ]
[ TYPE { REGION | MIXTURE | FLUX | MGFLUX } ]
```

where

<b>EDIT</b>	keyword used to modify the print level <i>iprint</i> .
<b><i>iprint</i></b>	index used to control the printing in this module. It must be set to 0 if no printing on the output file is required.
<b>FILL</b>	keyword to specify the drawing options.
<b>NONE</b>	keyword to specify that only region contour are to be drawn.
<b>GRAY</b>	keyword to specify that the regions will be filled with various levels of gray.
<b>RGB</b>	keyword to specify that the regions will be filled with various colors taken using the RGB color scheme.
<b>CMYK</b>	keyword to specify that the regions will be filled with various colors taken using the CMYK color scheme.
<b>HSB</b>	keyword to specify that the regions will be filled with various colors taken using the HSB color scheme. This is the default option.
<b>NOCONTOUR</b>	keyword to specify that the contour lines delimiting each region will not be drawn.
<b>TYPE</b>	keyword to specify the type of graphics generated.
<b>REGION</b>	keyword to specify that different colors or gray levels will be associated with each region. This is the default option.
<b>MIXTURE</b>	keyword to specify that different colors or gray levels will be associated with each mixture.
<b>FLUX</b>	keyword to specify that the group integrated flux is to be drawn.
<b>MGFLUX</b>	keyword to specify that the group flux is to be drawn.

### 3.16 The SAD: module

The SAD: module is used to compute the generalized adjoint fluxes associated with the homogenized and condensed cross-sections.<sup>[42–46]</sup> The calling specifications are:

Table 65: Structure (SAD:)

*FLUNAM EDINAM := SAD: PIJNAM LIBNAM TRKNAM :: (descsad)*

where

<i>FLUNAM</i>	character*12 name of the FLUXUNK data structure containing the generalized adjoint fluxes solution.
<i>EDINAM</i>	character*12 name of the EDITION data structure where the homogenized and condensed properties and the generalized adjoint sources will be stored.
<i>PIJNAM</i>	character*12 name of the ASMPIJ data structure containing the group dependent system matrices (see Section 3.6).
<i>LIBNAM</i>	character*12 name of the MACROLIB or MICROLIB data structure that contains the macroscopic cross sections (see Sections 3.1 and 3.2).
<i>TRKNAM</i>	character*12 name of the TRACKING data structure containing the tracking (see Section 3.4).
(descsad)	structure containing the input data to this module (see Section 3.16.1).

#### 3.16.1 Data input for module SAD:

Table 66: Structure (descsad)

```
[ EDIT iprint ]
[ INIT { OFF | ON ((fluxes(i, g), i=1,nregion ), g=1,ngroup ) } ]
[ { FLX | PAF | AF } ]
TYPE { N | S | K }
[ THER [ maxthr ] [ epsthr ] ]
[ EXTE [ maxout ] [ epsout ] ]
[ UNKT [ epsunk ] ]
[ REBA [ OFF ] ]
[ ACCE nlibre naccel ]
[ EGPA ] [ CGPA ]
[ SAVE ] [ NCOR ]
[ COND { NONE | ( { icond(g) | energy(g) }, g = 1, Ng) } ] ]
[ MERG { COMP | NONE | MIX (imixt(i), i = 1, Nm) | REGI (ireg(i), i = 1, Nr) } ] ]
[ TAKE { MIX (imixt(i), i = 1, Nm) | REGI (ireg(i), i = 1, Nr) } ] ]
[ SELE { NONE | ALL | TOTAL | TRANC | NUSIGF | NFTOT | SCAD } ]
```

where

EDIT	keyword used to modify the print level <i>iprint</i> .
<i>iprint</i>	index used to control the printing of this module. The amount of output produced by this tracking module will vary substantially depending on the print level specified.
INIT	keyword to specify the neutron flux initialization option used.
OFF	keyword to specify that the initial neutron flux distribution is not to be initialized.
ON	keyword to specify that the initial neutron flux distribution follows.
<i>fluxes</i>	array of average flux per region and per group.
FLX	keyword to specify that a flux solution is to be considered. This is the default option.
PAF	keyword to specify that a pseudo-adjoint flux solution is to be considered.
AF	keyword to specify that a pseudo-adjoint flux solution is to be considered and that both the pseudo-adjoint and adjoint flux are to be saved on the FLUXUNK data structure.
TYPE	keyword to specify the type of flux flux calculation to be performed.
N	keyword to specify that no flux calculation is to be performed. This option is usually activated when one simply wishes to initialize the neutron flux distribution and to store this information in <i>SADNAM</i> (see ON parameter above).
S	keyword to specify that a fixed source problem is to be treated. Such problem can also include fission source contributions.
K	keyword to specify that a fission source eigenvalue problem is to be treated. The eigenvalue is then the effective multiplication factor with a fixed buckling. In this case, the fixed source, if any is present on the MACROLIB or MICROLIB data structure, is not used.
THER	keyword to specify that the control parameters for the thermal iterations are to be modified.
<i>maxthr</i>	maximum number of thermal iterations. The fixed default value is $2 \times n_{group} - 1$ (using scattering modified CP) or $4 \times n_{group} - 1$ (using standard CP).
<i>epsthr</i>	convergence criterion for the thermal iterations. The fixed default value is $5.0 \times 10^{-5}$ .
EXTE	keyword to specify that the control parameters for the external iteration are to be modified.
<i>maxout</i>	maximum number of external iterations. The fixed default value for a case with no leakage model is $2 \times n_f - 1$ where $n_f$ is the number of regions containing fuel. The fixed default value for a case with a leakage model is $10 \times n_f - 1$ .
<i>epsout</i>	convergence criterion for the external iterations. The fixed default value is $5.0 \times 10^{-5}$ .
UNKT	keyword to specify that the flux/current error tolerance in the outer iteration.
<i>epsunk</i>	convergence criterion for flux/current in the outer iteration. The fixed default value is <i>epsunk=epsthr</i> .
REBA	keyword used to specify that the flux rebalancing option is to be turned on or off in the thermal iteration. By default (floating default) the flux rebalancing option is initially activated. This keyword is required to toggle between the on and off position of the flux rebalancing option.

OFF	keyword used to deactivate the flux rebalancing option. When this keyword is absent the flux rebalancing option is reactivated.
ACCE	keyword used to modify the variational acceleration parameters. This option is active by default (floating default) with <i>nlibre</i> =3 free iterations followed by <i>naccel</i> =3 accelerated iterations.
<i>nlibre</i>	number of free iterations per cycle of <i>nlibre</i> + <i>naccel</i> iterations.
<i>naccel</i>	number of accelerated iterations per cycle of <i>nlibre</i> + <i>naccel</i> iterations. Variational acceleration may be deactivated by using <i>naccel</i> =0. This is required when the NOR2 is used in the ASM: module (see Section 3.6.1).
EGPA	Error relaxation factor, the generalized adjoint fluxes convergence criteria are multiplied by this factor. The fixed default value is 10.0.
CGPA	Contamination factor, the generalized adjoint flux is initialization is proportional to the adjoint flux. The fixed default value is 100.0.
SAVE	The generalized adjoint sources are saved on EDINAM.
NCOR	The correction matrix associated with the high order components of the flux is not computed.
MERG	keyword to specify that the neutron flux is to be homogenized over specified regions or mixtures.
COND	keyword to specify that a group condensation of the flux is to be performed.
<i>icond</i>	array of increasing energy group limits that will be associated with each of the $N_g$ condensed groups. The final value of <i>icond</i> will automatically be set to <i>ngroup</i> while <i>icond</i> > <i>ngroup</i> will be dropped from the condensation. We must have $N_g \leq ngroup$ .
<i>energy</i>	array of decreasing energy limits (in eV) that will be associated with each of the $N_g$ condensed groups. We must have $N_g \leq ngroup+1$ . Note that if an energy limit is located between two energy groups, the condensation group will include this associated energy group. In the case where two energy limits fall within the same energy group the lowest energy will be dropped. Finally the maximum and minimum energy limits can be skipped since they will be taken automatically from the information available in the library.
MIX	keyword to specify that the homogenization of the neutron flux will take place over the following mixtures. Here we must have $N_m \leq maxmix$ where <i>maxmix</i> is the maximum number of mixtures in the macroscopic cross section library.
<i>imixm</i>	array of homogenized mixture numbers to which are associated the homogenized mixtures. In the SAD: module a value of <i>imixm</i> =0 allows the corresponding mixture to be neglected. For a mixture in this library that is not used in the geometry one should insert a value of 0 for the new region number associated with this mixture.
REGI	keyword to specify that the homogenization of the neutron flux will take place over the following regions. Here we must have $N_r \leq maxreg$ where <i>maxreg</i> is the maximum number of regions in the tracking data structure.
<i>ireg</i>	array of homogenized region numbers to which are associated the homogenized mixtures. In the SAD: module a value of <i>ireg</i> =0 allows the corresponding region to be neglected.
COMP	keyword to specify that a complete homogenization is to take place.
TAKE	keyword to specify that the neutron flux is to be edited over specified regions or mixtures.

<b>MIX</b>	keyword to specify that the homogenization of the neutron flux will take place over the following mixtures. Here we must have $N_m \leq \text{maxmix}$ where <i>maxmix</i> is the maximum number of mixtures in the macroscopic cross section library.
<i>imixt</i>	mixtures where the editing will take place. Each mixture used here must be used in the geometry one is considering.
<b>REGI</b>	keyword to specify that the homogenization of the neutron flux will take place over the following regions. Here we must have $N_r \leq \text{maxreg}$ where <i>maxreg</i> is the maximum number of regions in the tracking data structure.
<i>ireg</i>	regions where the editing will take place. Each mixture used here must be used in the geometry one is considering.
<b>SELE</b>	keyword to specify the homogenized and condensed cross section to take into account for the generalized adjoint fluxes computation.

### 3.17 The **PER:** module

The **PER:** module is used to perform generalized perturbation theory calculations in DRAGON.<sup>[42–46]</sup> The calling specifications are:

Table 67: Structure (**PER:**)

*EDINAM* := **PER:** *EDINAM LIBNAM TRKNAM FLUNAM LIBNAP* [ *FLUNAP* ] :: (**descper**)

where

<i>EDINAM</i>	character*12 name of the EDITION data structure containing the perturbed homogenized and condensed cross sections. <i>EDINAM</i> must appears on the RHS after being computed with <b>SAD:</b> for the reference state.
<i>LIBNAM</i>	character*12 name of the MACROLIB or MICROLIB data structure that contains the macroscopic cross sections (see Sections 3.1 and 3.2).
<i>TRKNAM</i>	character*12 name of the TRACKING data structure containing the tracking (see Section 3.4).
<i>FLUXNAM</i>	character*12 name of the FLUXUNK data structure containing the reference flux(see Section 3.16).
<i>LIBNAP</i>	character*12 name of the MACROLIB or MICROLIB data structure that contains the macroscopic perturbed cross sections (see Sections 3.1 and 3.2).
<i>FLUXNAP</i>	character*12 name of the FLUXUNK data structure containing the pertubed flux (see Section 3.7).
<b>(descper)</b>	structure containing the input data to this module (see Section 3.17.1).

#### 3.17.1 Data input for module **PER:**

Table 68: Structure (**descper**)

```
[ SAVE ON NAMREC ]
[ TYPE DIR | CALC | PER ]
[ LIN ]
```

where

<b>NAMREC</b>	character*12 name of the record where the perturbed homogenized and condensed cross sections are to be saved.
<b>TYPE</b>	keyword to specify the type of perturbation to be performed.
<b>DIR</b>	keyword to specify the neutron reference flux is to be used in the perturbation formulas.
<b>PER</b>	keyword to specify the perturbed reference flux is to be used in the perturbation formulas.
<b>CALC</b>	keyword to specify the perturbed homogenized and condensed cross sections are to be explicitly calculated. In this case, the perturbed flux <i>FLUXNAP</i> is required.
<b>LIN</b>	keyword to specify that the linear perturbation formulas are used. In this case the perturbed flux stored in <i>FLUXNAP</i> is required. This can be used for sensitivity coefficients calculation.

### 3.18 The **HST:** module

The **HST:** module has been designed to manage a full reactor execution in DONJON using explicit DRAGON calculations for each cell.<sup>[48-51]</sup> This module saves in an **HISTORY** data structure the information available in **BURNUP** data structures generated by DRAGON. It can also read **MAP** data structure generated by DONJON<sup>[47]</sup> to prepare the **HISTORY** data structure for a new series of cell calculations in DRAGON. The **HISTORY** data structure can also be used to update the **MAP** data structure. Finally, the module **HST:** can be used to create an initial **BURNUP** data structure that can be used to evolve the cell another time step in DRAGON.

The **HST:** module can be used to create or update an **HISTORY** data structure. The possible options are:

Table 69: Updating an **HISTORY** structure using a **MAP** structure

```
HISTORY := HST: [ HISTORY ] MAP [ : : [ (hstdim) ] [ GET (hstpar) ] ]
```

Table 70: Updating an **HISTORY** structure using a **BURNUP** structure

```
HISTORY := HST: [ HISTORY ] [ BURNUP ] [ : : [ (hstdim) ]
[ GET (hstpar) ] [ CELLID icha ibun [ idfuel ] [ GET (hstpar) ] ] ]
```

It can also be used to create a **BURNUP** data structure from the information available on an **HISTORY**:

Table 71: Updating a BURNUP structure using an HISTORY structure

```

BURNUP := HST: HISTORY [ :: [ (hstdim) ]
    [ PUT (hstpar) ]
    CELLID icha ibun
    [ PUT { BREFL (hstbrn) (hstpar) AREFL (hstbrn) (hstpar) | [ AREFL ] (hstbrn) (hstpar) } ] ]

```

It can also be used to update a MAP data structure from the information available on anHISTORY:

Table 72: Updating an HISTORY structure using a MAP structure

```

MAP := HST: MAP HISTORY

```

where

<i>HISTORY</i>	character*12 name of an HISTORY data structure.
<i>BURNUP</i>	character*12 name of a BURNUP data structure.
<i>MAP</i>	character*12 name of a MAP data structure.
<b>(hstdim)</b>	structure containing the dimensions for the HISTORY data structure.
<b>CELLID</b>	keyword to identify the cell for which history information is to be processed.
<i>icha</i>	channel number for which history information is to be processed.
<i>ibun</i>	bundle number for which history information is to be processed.
<i>idfuel</i>	fuel type number associated with this cell. One can associate to each fuel cell a different fuel type. By default a single fuel type is defined and it fills every fuel cell. Only the initial properties of each fuel type are saved. These properties are used for refueling.
<b>GET</b>	keyword to specify that the values of the parameters selected in <b>(brnpar)</b> will be read from the input stream or CLE-2000 local variables and stored on the HISTORY data structure.
<b>PUT</b>	keyword to specify that the values of the parameters selected in <b>(brnpar)</b> will be read from the HISTORY data structure and transferred to local CLE-2000 variables.
<b>BREFL</b>	to specify that the information to extract from the HISTORY data base is related to the properties of the cell before refueling takes place.
<b>AREFL</b>	to specify that the information to extract from the HISTORY data base is related to the properties of the cell after refueling took place.
<b>(hstbrn)</b>	structure containing the burnup options.
<b>(hstpar)</b>	structure containing the local parameters options.

The **(hstdim)** input structure is required for general dimensioning purpose. It is generally used only when creating the HISTORY data structure. However, the number of global and local parameters used in a HISTORY data structure can be increased at all time. The number of channels, bundles and the refueling scheme must be defined at the creation of the HISTORY data structure. This information can be provided manually or extracted from a MAP data structure. The general form of the **(hstdim)** input structure follows:

Table 73: Structure **(hstdim)**

```
[ EDIT iprint ]
[ DIMENSIONS [ GLOBAL nglo ] [ LOCAL nloc ] [ BUNDLES nbun bunl ] [ CHANNELS ncha ] ]
```

where

<b>EDIT</b>	keyword used to modify the print level <i>iprint</i> .
<i>iprint</i>	index used to control the printing in this module. It must be set to 0 if no printing on the output file is required.
<b>DIMENSIONS</b>	keyword used to indicate that the general dimensioning of the HISTORY data structure will be modified.
<b>GLOBAL</b>	keyword used to modify the number of global parameters on the HISTORY data structure.
<i>nglo</i>	the number of global parameters. Note that the history module will use the maximum value between the current <i>nglob</i> and the value, if any, defined on the HISTORY data structure.
<b>LOCAL</b>	keyword used to modify the number of local parameters on the HISTORY data structure.
<i>nloc</i>	the number of local parameters. Note that the history module will use the maximum value between the current <i>nloc</i> and the value, if any, defined on the HISTORY data structure.
<b>BUNDLES</b>	keyword used to specify the number of bundles per channels for the reactor model considered in the HISTORY data structure.
<i>nbun</i>	the number of bundles per channels for the reactor model. Note that if <i>nbun</i> is different from the value already defined on the HISTORY data structure or the MAP data structure, the execution will be aborted.
<i>bunl</i>	bundle length in cm. This information is required to compute initial fuel weight.
<b>CHANNELS</b>	keyword used to specify the number of fuel channels for the reactor model considered in the HISTORY data structure.
<i>ncha</i>	the number of fuel channels for the reactor model. Note that if <i>ncha</i> is different from the value already defined on the HISTORY data structure or the MAP data structure, the execution will be aborted.

The **(hstbrn)** serves a unique purpose, mainly to extract from the HISTORY file the information required to process a burnup evaluation in DRAGON using the EVO: module. The information must be stored inside CLE-2000 variables. The general form of this output structure is:

Table 74: Structure (**hstbrn**)

BURN <i>period power</i>
--------------------------

where

**BURN** keyword to indicate that burnup information follows.

*period* the burnup period (in days) that will be transferred to a real CLE-2000 variable.

*power* the power density (in kW/kg) that will be transferred to a real CLE-2000 variable.

The (**hstpar**) serves two purposes. First, it is used to define the names of the local and global parameters that may be used in our calculations as well as the values of these local parameters. It can also be used to extract from a HISTORY data structure the values of these parameters. The general form of this structure is:

Table 75: Structure (**hstpar**)

[[ <i>NAMPAR valpar</i> ]]
----------------------------

where

**NAMPAR** name of a local or global parameter to process. The parameters specified before the keyword *CELLID* is read will be considered global otherwise they will be considered local.

*valpar* real value for the local or global parameter to process. In the case where the GET option is activated, the history module will extract this parameter from the input data stream. In the case where the PUT option is activated, the history module will try to transfer this information into a real CLE-2000 variable.

### 3.19 The **TLM:** module

The **TLM:** module has been designed to generate a Matlab<sup>[52]</sup> *m-file* (in an ASCII format) that contains the instructions for plotting the tracking lines generated by the **NXT:** module (**EDIT -1000** option).<sup>[53]</sup> The **TLM:** module is activated using the following list of commands:

Table 76: Structure (**TLM:**)

<i>MFILE</i> := <b>TLM:</b> <i>MFILE TRKNAM TRKFIL</i> :: ( <b>desctlm</b> )
--

where

**MFILE** character\*12 name of the ASCII Matlab *m-file* data structure that will contain the instructions for plotting the tracking lines.

<b>TRKNAM</b>	character*12 name of the TRACKING data structure that will contain region volume and surface area vectors in addition to region identification pointers and other tracking information.
<b>TRKFIL</b>	character*12 name of the sequential binary tracking file used to store the tracks lengths. <sup>[6]</sup>
<b>(desctlm)</b>	structure describing the type of graphics generated (see Section 3.19.1).

### 3.19.1 Data input for module TLM:

Table 77: Structure **(desctlm)**

```
[ EDIT iprint ]
[ NTPO nplots ]
( {
  POINTS [ NoPause ] |
  DIRECTIONS [ NoPause ] DIR idir [ PLAN iplan { U iuv | V iuv } ] |
  PLANP [ NoPause ] DIR idir DIST dist [ PLAN iplan ] |
  PLANA [ NoPause ] A a B b [ C c ] D d
} , iplot=1, nplots )
```

where

<b>EDIT</b>	keyword used to modify the print level <i>iprint</i> .
<i>iprint</i>	index used to control the printing in this module. It must be set to 0 if no printing on the output file is required.
<b>NTPO</b>	keyword to specify the number of figures to draw.
<i>nplots</i>	integer value for the number of figures to draw.
<b>POINTS</b>	keyword to specify that the figure will illustrate the intersection points between the lines and the external faces of the geometry.
<b>DIRECTIONS</b>	keyword to specify that the figure will illustrate the lines crossing each region as well as the intersection points between the lines and the external faces of the geometry.
<b>PLANP</b>	keyword to specify that the figure will illustrate the points crossing a plane normal to the line direction.
<b>PLANA</b>	keyword to specify that the figure will illustrate the points crossing an arbitrary surface in 3-D or line in 2-D. The equation for the surface in 3-D is :

$$aX + bY + cZ = d$$

while the equation for the line in 2-D is :

$$aX + bY = d$$

<b>NoPause</b>	keyword to specify that all the lines must be drawn without Matlab pause. By default, there is a pause after all the points associated with an external surface and all the lines associated with a region are drawn.
<b>DIR</b>	keyword to specify line direction to draw.
<i>idir</i>	integer value to identify the track direction to draw. In the case where <i>idir</i> =0, all the directions will be drawn. A value of <i>idir</i> =0 for 2-D geometry is generally acceptable. However, for 3-D geometry the number of lines generated is such that the figure becomes a mess and it is generally more convenient to draw the lines direction per direction.
<b>PLAN</b>	keyword to specify which of the three planes normal to the specified direction in 3-D will be considered for drawing. This plane is defined by the axes $U - V$ . Used only for 3-D geometries.
<i>iplan</i>	integer value to identify which of the three planes normal to the specified direction in 3-D will be considered for drawing. the only values permitted are 0, 1, 2 or 3. When a value of 0 is specified (default) all three planes will be drawn. Used only for 3-D geometries.
<b>U</b>	keyword to specify that the all the lines in the $V$ axis associated with a position on the $U$ axis will be drawn. Used only for 3-D geometries.
<b>V</b>	keyword to specify that the all the lines in the $U$ axis associated with a position on the $V$ axis will be drawn. Used only for 3-D geometries.
<i>iuu</i>	integer value to identify the position on the $U$ or $V$ axis to be drawn. Used only for 3-D geometries.
<b>DIST</b>	keyword to specify the distance between the plane normal to the line direction and the origin.
<i>dist</i>	real or double precision value for the distance of the plane from the origin.
<b>A</b>	keyword to specify the value of $a$ for an arbitrary plane or line.
<i>a</i>	real or double precision value $a$ .
<b>B</b>	keyword to specify the value of $b$ for an arbitrary plane or line.
<i>b</i>	real or double precision value $b$ .
<b>C</b>	keyword to specify the value of $c$ for an arbitrary plane.
<i>c</i>	real or double precision value $c$ .
<b>D</b>	keyword to specify the value of $d$ for an arbitrary plane or line.
<i>d</i>	real or double precision value $d$ .

## 4 EXAMPLES

We will now present a few examples of DRAGON input structures in such a way as to clarify and illustrate some of the options presented in Section 3.

### 4.1 Scattering cross sections

In DRAGON, the angular dependence of the scattering cross section is expressed in a Legendre series expansion of the form:

$$\Sigma_s(\Omega \cdot \Omega') = \Sigma_s(\mu) = \sum_{l=0}^L \frac{(2l+1)}{4\pi} \Sigma_{s,l} P_l(\mu).$$

Since the Legendre polynomials satisfy the following orthogonality conditions:

$$\int_{-1}^1 d\mu P_l(\mu) P_m(\mu) = \frac{2\delta_{l,m}}{(2l+1)},$$

we will have

$$\Sigma_{s,l} = \int_{-1}^1 d\mu \int_0^{2\pi} d\varphi \Sigma_s(\mu) P_l(\mu) = 2\pi \int_{-1}^1 d\mu \Sigma_s(\mu) P_l(\mu).$$

Let us now consider the following three group ( $ngroup=3$ ) isotropic and linearly anisotropic scattering cross sections ( $L=naniso=2$ ) given by:

$l$	$g$	$\Sigma_{s,l}^{g \rightarrow 1} (\text{cm}^{-1})$	$\Sigma_{s,l}^{g \rightarrow 2} (\text{cm}^{-1})$	$\Sigma_{s,l}^{g \rightarrow 3} (\text{cm}^{-1})$
0	1	0.90	0.80	0.00
	2	0.00	0.70	0.60
	3	0.00	0.30	0.40
1	1	0.09	0.05	0.08
	2	0.00	0.07	0.06
	3	0.03	0.00	0.04

In DRAGON this scattering cross section must be entered as

```
SCAT    1 1  0.90
        3 3  0.30  0.70  0.80
        2 3  0.40  0.60
        3 3  0.03  0.00  0.09
        2 2  0.07  0.05
        3 3  0.04  0.06  0.08
```

### 4.2 Geometries

In order to illustrate the use of the various geometries presented in Section 3.3, let's consider a few examples that can be treated by DRAGON.

- 1-D Slab geometry (see Figure 10):

This geometry can be analyzed using the **JPMT:** and **SYBILT:** tracking modules:

```

PLATE := GEO: :: CAR1D 6
X- VOID X+ ALBE 1.2
MESHX 0.0 0.1 0.3 0.5 0.6 0.8 1.0
SPLITX 2 2 2 1 2 1
MIX 1 2 3 4 5 6 ;

```

- 2-D Cartesian geometry containing micro structures (see figure Figure 11):

This geometry can be analyzed only using SYBILT: tracking modules:

```

CARNSG := GEO: :: CAR2D 3 3
X- DIAG X+ REFL Y- SYME Y+ DIAG
CELL C1 C1 C2
      C3 C2
      C3
BIHET SPHE 2 2
          3 3
          0.0 0.1 0.2 0.3 0.0 0.2 0.4 0.5
          4 5 1 1 0.4 0.0 3 1 3 0.2 0.1
          1 2 1 2 3 1
::: C1 := GEO: CAR2D 1 1
MESHX 0.0 1.45 MESHY 0.0 1.45 MIX 4 ;
::: C2 := GEO: C1
MIX 1 ;
::: C3 := GEO: CARCEL 2
MESHX 0.0 1.45 MESHY 0.0 1.45
RADIUS 0.0 0.6 0.7
MIX 5 2 1 ; ;

```

- Cylindrical and Cartesian cluster geometry (see Figure 12):

The first two geometry, namely ANNPIN and CARPIN can be analyzed using both the JPMT:, EXCELT: and NXT: tracking modules since the pins in the clusters are all located between annular region. For the last two geometries, ANNSPIN and CARSPIN, which are based on ANNPIN and CARPIN respectively, they can only be treated by the EXCELT: and NXT: tracking modules since the pins in the clusters intersect the annular regions defined by the SPLITR option. This later option was selected to ensure a uniform thickness of 0.25 cm for each the annular region in the final geometries.

```

ANNPIN := GEO: :: TUBE 3
R+ REFL RADIUS 0.0 0.75 2.75 4.75
MIX 2 1 3
CLUSTER C1 C2
::: C1 := GEO: TUBE 2
MIX 2 4 RADIUS 0.0 0.3 0.6
NPIN 4 RPIN 1.75 APIN 0.523599 ;
::: C2 := GEO: C1
NPIN 2 RPIN 3.75 APIN 1.570796 ; ; CARPIN := GEO: :: CARCEL 3
X- REFL X+ REFL Y- REFL Y+ REFL
MESHX 0.0 10.0 MESHY -5.0 5.0
RADIUS 0.0 0.75 2.75 4.75
MIX 2 1 3 3
CLUSTER C1 C2
::: C1 := GEO: TUBE 2
MIX 2 4 RADIUS 0.0 0.3 0.6

```

```

      NPIN 4  RPIN 1.75  APIN 0.523599 ;
      ::: C2 := GEO: C1
      NPIN 2  RPIN 3.75  APIN 1.570796 ; ; ANNSPIN := GEO: ANNPIN ::
      SPLITR 3 8 8 ; CARSPIN := GEO: CARPIN ::
      SPLITR 3 8 8 ;

```

Note that even if MESHX and MESHY differ in CARPIN, the annular regions and pins will still be localized with respect to the center of the cell located at  $(x, y) = (5.0, 0.0)$  cm.

- 2-D hexagonal geometry (see Figure 13):

This geometry can be analyzed using the JPMT:, SYBILT: and EXCELT: tracking modules:

```

HEXAGON := GEO: :: HEX 12
HBC S30 ALBE 1.6
SIDE 1.3
MIX 1 1 1 2 2 2 3 3 3 4 5 6 ;

```

- 3-D Cartesian supercell (see Figure 14):

This geometry can only be analyzed using the EXCELT: and NXT: tracking modules:

```

SUPERCELL := GEO: :: CAR3D 4 4 3
X- REFL    X+ REFL
Y- REFL    Y+ REFL
Z- REFL    Z+ REFL
CELL A1 C1 D1 A3      A2 C2 D2 D2      A2 C2 C2 C2      A2 C2 C2 C2
      C3 C3 D3 A4      C4 C4 D4 D4      C4 C4 C4 C4      C4 C4 C4 C4
      C3 C3 D3 A4      C4 C4 D4 D4      C4 C4 C4 C4      C4 C4 C4 C4
::: C1 := GEO: CAR3D 1 1 1
  MESHX 0.0 1.0 MESHY 0.0 1.5 MESHZ 0.0 2.0
  MIX 1 ;
::: C2 := GEO: C1 MESHY 0.0 1.0 ;
::: C3 := GEO: C1 MESHZ 0.0 1.0 ;
::: C4 := GEO: C2 MESHZ 0.0 1.0 ;
::: D1 := GEO: C1 MIX 2 ;
::: D2 := GEO: C2 MIX 2 ;
::: D3 := GEO: C3 MIX 2 ;
::: D4 := GEO: C4 MIX 2 ;
::: A1 := GEO: CARCELY 2 1
  MESHX 0.0 1.0 MESHY 0.0 1.5 MESHZ 0.0 2.0
  RADIUS 0.0 0.4 0.45
  MIX 3 4 1 ;
::: A2 := GEO: A1 MESHY 0.0 1.0 ;
::: A3 := GEO: CARCELZ 2 1
  MESHX 0.0 1.0 MESHY 0.0 1.5 MESHZ 0.0 2.0
  RADIUS 0.0 0.3 0.35
  MIX 5 6 1 ;
::: A4 := GEO: A3 MESHZ 0.0 1.0 ; ;

```

- Multicell geometry in a 2-D hexagonal lattice (see Figure 15).

Here we are considering an infinite lattice having two types of cells such that

$$\begin{pmatrix} \text{pource}(1) \\ \text{pource}(2) \end{pmatrix} = \begin{pmatrix} 1/3 \\ 2/3 \end{pmatrix}$$

and

$$\begin{pmatrix} \text{procel}(1,1) & \text{procel}(1,2) \\ \text{procel}(2,1) & \text{procel}(2,2) \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ 1/2 & 1/2 \end{pmatrix}$$

This lattice, can be represented either in a *do-it-yourself* type geometry (HEXDIY) or directly (HEXDIR):

```

HEXDIY := GEO: :: GROUP 2
POURCE 0.3333333 0.66666667
PROCEL 0.0      1.0
        0.5      0.5
CELL    C1 C2
::: C1 := GEO: TUBE 1
      RADIUS 0.0 1.1822093 MIX 1 ;
::: C2 := GEO: C1 MIX 2 ; ; HEXDIR := GEO: :: HEX 2
HBC S30 SYME SIDE 1.3 MIX 1 2 ;

```

The first lattice can only be analyzed using SYBILT: and JPMT: while the second lattice can be analyzed using all the tracking modules of DRAGON.

### 4.3 Macroscopic cross sections examples

The sample test cases we will consider here use the MAC: module to enter macroscopic cross sections directly into DRAGON. They are numbered successively from **TCM01** to **TCM12**.

#### 4.3.1 TCM01 – Annular region

This sample input is used to analyze the annular cell presented in Figure 16. It uses two groups macroscopic cross sections provided directly by the user. Two types of solutions are provided here, one with a complete collision probability calculation (SYBILT:) and one using the  $J_{\pm}$  method (JPMT:). Note that for the second flux calculation the initial flux distribution is taken from the existing FLUXUNK structure which already contains the flux distribution from the SYBILT: calculation.

Input data for test case: **TCM01.x2m**

```

*-----
* TEST CASE TCM01
* MACROSCOPIC CROSS SECTIONS
* FISSION SOURCE PROBLEM
* 1-D ANNULAR CELL
*
* REF: none
*
*-----
* Define STRUCTURES and MODULES used
*-----
LINKED_LIST
  MACRO ANGeo TRACK SYS FLUX EDITION ;
SEQ_ASCII
  res ;
MODULE
  GEO: SYBILT: JPMT: MAC: ASM: FLU: EDI: DELETE: END: ;

```

```

*-----
*   Macroscopic XS
*-----
MACRO := MAC: ::
    NGRO 2 NMIX 2 NIFI 1
    READ INPUT
    MIX 1    TOTAL 0.222222 0.833333
        SCAT   1 1  0.19222      2 2 0.75333 0.02
        NUSIGF 0.0  0.135 CHI 1.0 0.0
    MIX 2    TOTAL 0.166667 1.111111
        SCAT   2 2  0.00015 0.126667 2 2 1.10111 0.04
    ;
*-----
*   Geometry :   ANGIO - Annular 2 regions
*-----
ANGIO := GEO: :: TUBE 2
    R+ REFL
    RADIUS 0.0 0.19653 1.0
    MIX      1      2
    SPLITR   1      4    ;
*-----
*   Tracking : SYBILT
*   Solution : PIJ
*   1- KEFF WITHOUT BUCKLING
*   2- BUCKLING WITH KEFF=1
*   3- LEAKAGE WITH KEFF=1
*-----
TRACK := SYBILT: ANGIO ::
    TITLE 'TCM01: ANNULAR GEOMETRY WITH MACROSCOPIC XS (SYBIL)'
    EDIT 1 MAXR 5 QUA1 5 ;
SYS := ASM: MACRO TRACK ;
FLUX := FLU:      SYS MACRO TRACK ::
    TYPE K ;
EDITION := EDI:      FLUX MACRO TRACK ::
    EDIT 3 SAVE ;
FLUX := FLU: FLUX SYS MACRO TRACK ::
    TYPE B B0 ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
    EDIT 3 SAVE ;
FLUX := FLU: FLUX SYS MACRO TRACK ::
    TYPE L B0 ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
    EDIT 3 SAVE ;
FLUX SYS TRACK := DELETE: FLUX SYS TRACK ;
*-----
*   Tracking : JPMT
*   Solution : ASM
*   1- KEFF WITHOUT BUCKLING
*   2- BUCKLING WITH KEFF=1
*   3- LEAKAGE WITH KEFF=1
*-----
TRACK := JPMT: ANGIO ::

```

```

      TITLE 'TCM01: ANNULAR GEOMETRY WITH MACROSCOPIC XS (JPM)'
      EDIT 1 MAXR 5 IP01 QUA1 5 ;
      SYS := ASM: MACRO TRACK ::
      ARM ;
      FLUX := FLU:          SYS MACRO TRACK ::
      TYPE K ;
      EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 3 SAVE STAT ALL REFE 1 ;
      FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE B B0 PNL EXTE 5.0E-5 ;
      EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 3 SAVE STAT ALL REFE 2 ;
      FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE L B0 ;
      EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 3 SAVE STAT ALL REFE 3 ;
      FLUX SYS := DELETE: FLUX SYS ;
      *-----
      *   Tracking : JPMT
      *   Solution : PIJ
      *   1- KEFF WITHOUT BUCKLING
      *   2- BUCKLING WITH KEFF=1
      *   3- LEAKAGE WITH KEFF=1
      *-----
      SYS := ASM: MACRO TRACK ;
      FLUX := FLU:          SYS MACRO TRACK ::
      TYPE K ;
      EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 3 SAVE STAT ALL REFE 4
      ;
      FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE B B0 ;
      EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 3 SAVE STAT ALL REFE 5 ;
      FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE L B0 ;
      EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 3 SAVE STAT ALL REFE 6 ;
      res := EDITION ;
      END: ;
      QUIT "LIST" .

```

#### 4.3.2 TCM02 – The Stankovski test case

This test case represents a one group calculation of a  $7 \times 7$  PWR assembly. The reaction rates obtained from DRAGON can be compared with those obtained using the MARSYAS code.<sup>[20,21,80]</sup> The corresponding geometry is shown in Figure 17 where the cell numbers generated by DRAGON are shown.

Input data for test case: **TCM02.x2m**

```

*-----
*   TEST CASE TCM02
*   MACROSCOPIC CROSS SECTIONS
*   FIXED SOURCE PROBLEM
*   FOR 1/8 7X7 PWR ASSEMBLY
*
*   REF: Z. Stankovski, Nucl. Sci. Eng. 92, 255 (1986)
*         R. Roy et al. Advances in Mathematics, Computation
*         and Reactor Physics, April 28 - May 2 1991, Pittsburgh
*
*-----
*   Define STRUCTURES and MODULES used
*-----
LINKED_LIST
  PWR TRACK MACRO SYS FLUX EDITION ;
SEQ_BINARY
  PWRTRK ;
MODULE
  GEO: EXCELT: MAC: ASM: FLU: EDI: END: DELETE: ;
*-----
*   Macroscopic XS
*-----
MACRO := MAC: ::
  NGRO 1 NMIX 3
  READ INPUT
  MIX 1 TOTAL 1.250 SCAT 1 1 1.242 FIXE 1.000
  MIX 2 TOTAL 0.625 SCAT 1 1 0.355 FIXE 0.000
  MIX 3 TOTAL 14.000 SCAT 1 1 0.000 FIXE 0.000
  ;
*-----
*   Geometry : PWR - Cartesian 4X4
*   Tracking : EXCELT
*-----
PWR := GEO: :: CAR2D 4 4
  X- DIAG  X+ REFL Y- SYME  Y+ DIAG
  CELL    P F F F
          F F F
          F F
          F
  ::: F := GEO: CARCEL 1
  RADIUS 0.000 0.450 MIX 2 1
  MESHX -0.625 0.625 SPLITX 2
  MESHY -0.625 0.625 SPLITY 2
  ;
  ::: P := GEO: F
  MIX 3 1 SPLITR 3
  ;
  ;
TRACK PWRTRK := EXCELT: PWR ::
  TITLE 'TCM02: STANKOVSKI PWR ASSEMBLY'

```

```

MAXR 58 CUT 1.E-4 TRAK TSPC 12 8.0
;
*-----
*   Solution : FIXED SOURCE PROBLEM
*   Editing  : Absorption rates taken from STANKOVSKI
*   cell 1 = 0.83799 0.00689 cell 2 = 0.73979 0.03571
*   cell 3 = 0.82218 0.03991 cell 4 = 0.85166 0.04104
*   cell 5 = 0.78722 0.03824 cell 6 = 1.67049 0.08092
*   cell 7 = 1.71199 0.08252 cell 8 = 0.85350 0.04120
*   cell 9 = 1.72122 0.08328 cell 10= 0.86023 0.04174
*   NOTE: There is a factor 4.0 with the EDI: results of DRAGON
*-----
SYS := ASM: MACRO TRACK PWRTRK :: ;
FLUX := FLU:          SYS MACRO TRACK ::
TYPE S ;
EDITION := EDI: FLUX MACRO TRACK ::
EDIT 2 SAVE
MERGE REGION  1  1  1  2  3  4  3  4  5  6  5  6  7  8  7  8
9 10  9 10  9 10 11 12 11 12 11 12 11 12 13 14 13 14 13 14
15 16 15 16 15 16 17 18 17 18 17 18 17 18
19 20 19 20 19 20
;
PWRTRK := DELETE: PWRTRK ;
END: ;
QUIT "LIST" .

```

#### 4.3.3 TCM03 – Watanabe and Maynard problem with a void region

This test case is a one group problem with a central void region (see Figure 18). This benchmark was first proposed by Watanabe and Maynard. Akroyd and Riyait used it to analyze the performance of various codes.<sup>[20,21,81]</sup>

Input data for test case: **TCM03.x2m**

```

*-----
*   TEST CASE TCM03
*   MACROSCOPIC CROSS SECTIONS
*   FIXED SOURCE PROBLEM
*   CARTESIAN 3 X 3 ASSEMBLY
*
*   REF: Akroyd and Riyait, Ann. Nucl. Energy 16, 1 (1989)
*         R. Roy et al. Advances in Mathematics, Computation
*         and Reactor Physics, April 28 - May 2 1991, Pittsburgh
*         R. Roy, Ann. Nucl. Energy 18, 511 (1991)
*
*-----
*   Define STRUCTURES and MODULES used
*-----
LINKED_LIST
WATA WAT08 WAT16 WAT24 TRACK MACRO SYS FLUX EDITION ;
SEQ_BINARY
WATATRK ;

```

```

MODULE
  GEO: EXCELT: MAC: ASM: FLU: EDI: DELETE: END: ;
*-----
* Macroscopic XS
*-----
MACRO := MAC: ::
  NGRO 1 NMIX 3
  READ INPUT
  MIX 1 TOTAL 0.2 SCAT 1 1 0.19 FIXE 6.4
  MIX 2 TOTAL 0.2 SCAT 1 1 0.19
  MIX 3 TOTAL 0.0 SCAT 1 1 0.00
  ;
*-----
* Geometry : WATA - 3 X 3 REGIONS
*             WAT08 - 8 X 8 REGIONS
*             WAT16 - 16 X 16 REGIONS
*             WAT24 - 24 X 24 REGIONS
* Tracking : EXCELT
*-----
WATA := GEO: :: CAR2D 3 3
  X- DIAG X+ VOID Y- REFL Y+ DIAG
  MESHX 0.00 1.25 5.00 10.00 MESHY 0.00 1.25 5.00 10.00
  MIX 1 3 2
        3 2
        2
  ;
WAT08 := GEO: WATA ::
  SPLITX 1 3 4 SPLITY 1 3 4
  ;
WAT16 := GEO: WATA ::
  SPLITX 2 6 8 SPLITY 2 6 8
  ;
WAT24 := GEO: WATA ::
  SPLITX 3 9 12 SPLITY 3 9 12
  ;
*-----
* Tracking : EXCELT - WAT08
* Solution : FIXED SOURCE PROBLEM
* Editing : 1- UPPER QUADRANT FLUX
*           2- FLUX AT X=5.625CM
*-----
TRACK WATATRK := EXCELT: WAT08 ::
  TITLE 'TCM03: WATANABE-MAYNARD 8X8 '
  MAXR 300 CUT 1.E-4 TRAK TSPC 12 4.0
  ;
SYS := ASM: MACRO TRACK WATATRK ::
  SKIP
  ;
FLUX := FLU: SYS MACRO TRACK ::
  TYPE S THER 1.E-6 100 EXTE 1.E-6 100
  ;
EDITION := EDI: FLUX MACRO TRACK ::

```

```

EDIT 2 SAVE
MERGE REGION
0 0 0 0 0 0 0 0
  0 0 0 0 0 0 0
    0 0 0 0 0 0
      0 0 0 0
        1 2 3 4
          5 6 7
            8 9
              10
;
EDITION := EDI: EDITION  FLUX MACRO TRACK ::
EDIT 2 SAVE
MERGE REGION
0 0 0 0 1 0 0 0
  0 0 0 2 0 0 0
    0 0 3 0 0 0
      0 4 0 0 0
        5 6 7 8
          0 0 0
            0 0
              0
;
TRACK WATATRK SYS FLUX := DELETE: TRACK WATATRK SYS FLUX ;
*-----
* Tracking : EXCELT - WAT16
* Solution : FIXED SOURCE PROBLEM
* Editing : 1- UPPER QUADRANT FLUX
*           2- FLUX AT X=5.625CM
*-----
TRACK WATATRK := EXCELT: WAT16 ::
TITLE 'TCM03: WATANABE-MAYNARD 16X16 '
MAXR 300 CUT 1.E-4 TRAK TSPC 12 8.0
;
SYS := ASM: MACRO TRACK WATATRK ::
SKIP
;
FLUX := FLU: SYS  MACRO TRACK ::
TYPE S THER 1.E-6 100 EXTE 1.E-6 100
;
EDITION := EDI: EDITION  FLUX  MACRO TRACK ::
EDIT 2 SAVE
MERGE REGION
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
  0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0
      0 0 0 0 0 0 0 0 0 0 0 0 0
        0 0 0 0 0 0 0 0 0 0 0 0
          0 0 0 0 0 0 0 0 0 0 0
            0 0 0 0 0 0 0 0 0
              1 1 2 2 3 3 4 4

```

```

      1  2  2  3  3  4  4
        5  5  6  6  7  7
          5  6  6  7  7
            8  8  9  9
              8  9  9
                10 10
                  10
;
EDITION := EDI: EDITION FLUX  MACRO TRACK ::
EDIT 2 SAVE
MERGE REGION
0 0 0 0 0 0 0 0 1 1 0 0 0 0 0 0
 0 0 0 0 0 0 0 2 2 0 0 0 0 0 0 0
   0 0 0 0 0 0 3 3 0 0 0 0 0 0 0
    0 0 0 0 0 4 4 0 0 0 0 0 0 0
     0 0 0 0 5 5 0 0 0 0 0 0 0
      0 0 0 6 6 0 0 0 0 0 0 0
       0 0 7 7 0 0 0 0 0 0 0
        0 8 8 0 0 0 0 0 0 0
          9 10 12 13 14 15 16 17
           11 12 13 14 15 16 17
            0 0 0 0 0 0 0
             0 0 0 0 0
              0 0 0 0
               0 0 0
                0 0
                 0
;
TRACK WATATRK SYS FLUX := DELETE: TRACK WATATRK SYS FLUX ;
*-----
* Tracking : EXCELT - WAT24
* Solution : FIXED SOURCE PROBLEM
* Editing  : 1- UPPER QUADRANT FLUX
*           2- FLUX AT X=5.625CM
*-----
TRACK WATATRK := EXCELT: WAT24 ::
  TITLE 'TCM03: WATANABE-MAYNARD 24X24 '
  MAXR 300 CUT 1.E-4 TRAK TSPC 12 12.0
;
SYS := ASM: MACRO TRACK WATATRK ::
SKIP
;
FLUX := FLU: SYS  MACRO TRACK ::
  TYPE S THER 1.E-6 100 EXTE 1.E-6 100
;
EDITION := EDI: EDITION  FLUX  MACRO TRACK ::
EDIT 2 SAVE
MERGE REGION
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
  0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

```



QUIT "LIST" .

#### 4.3.4 TCM04 – Adjuster rod in a CANDU type supercell

This test case represents a two group calculation of incremental cross sections resulting from the insertion of stainless steel adjuster rods in a CANDU-6 supercell (see Figure 19).

Input data for test case: **TCM04.x2m**

```
*-----
*   TEST CASE TCM04
*   MACROSCOPIC CROSS SECTIONS
*   FISSION SOURCE PROBLEM
*   CANDU 3-D ADJUSTER ROD 1/8-ASSEMBLY
*
*   REF: none
*
*-----
*   Define STRUCTURES and MODULES used
*-----
LINKED_LIST
  BC TRACK  MACRO SYS  FLUX  EDITION
    TRACK2          SYS2 FLUX2 EDITION2      ;
SEQ_BINARY
  BCTRK ;
MODULE
  GEO: EXCELT: EXCELL: MAC: ASM: FLU: EDI:  DELETE: END: ;
*-----
*   Macroscopic XS
*-----
MACRO := MAC: ::
NGRO 2 NMIX 4 NIFI 1
READ INPUT
MIX 1  TOTAL      3.22798014E-1 3.81341100E-1
      NUSIGF      5.46564534E-3 7.17375278E-2
      CHI         1.0           0.0
      SCAT 2 2    3.13575147E-4 3.11233580E-1
              2 2    3.24143648E-1 2.19577667E-3
MIX 2  TOTAL      1.49818063E-1 1.59792125E-1
      SCAT 2 2    7.40572286E-5 1.47693634E-1
              2 2    1.57371104E-1 1.30506000E-3
MIX 3  TOTAL      2.60458171E-1 3.77224326E-1
      SCAT 2 2    5.98954648E-5 2.49342978E-1
              2 2    3.77127469E-1 1.11155845E-2
MIX 4  TOTAL      2.60458171E-1 3.77224326E-1
      SCAT 2 2    5.98954648E-5 2.49342978E-1
              2 2    3.77127469E-1 1.11155845E-2
;
*-----
*   Geometry : BC - 3D Cartesian assembly with annular regions
*   Tracking  : 1) EXCELT
```

```

*                2) EXCELL (includes ASM and does not require track file)
*-----
BC := GEO: :: CAR3D 3 2 2
  X- REFL X+ SYME Y- REFL Y+ SYME Z- REFL Z+ SYME
  CELL  M    MX  MX MX  FXY MXY    M    MX  BX MX  FXY BXY
  TURN  A    A  A  F  A  A    A    A  A  F  A  A
  ::: M := GEO: CAR3D 1 1 1
    MESHX 0.0 7.14375 MESHY 0.0 7.14375 MESHZ -8.25500 +8.25500
    SPLITZ 2 MIX 3
  ;
  ::: MX := GEO: M
    MESHX -7.14375 +7.14375 SPLITX 2
  ;
  ::: MXY := GEO: MX
    MESHY -7.14375 +7.14375 SPLITY 2
  ;
  ::: BX := GEO: CARCELY 2 1
    MESHX -7.14375 +7.14375 SPLITX 2
    MESHY 0.0 +7.14375
    MESHZ -8.25500 +8.25500 SPLITZ 2
    RADIUS 0.0 3.5100 3.8100
    MIX 3 4 3
  ;
  ::: BXY := GEO: BX
    MESHY -7.14375 +7.14375 SPLITY 2
  ;
  ::: FXY := GEO: CARCELZ 2 1
    MESHX -7.14375 +7.14375 SPLITX 2
    MESHY -7.14375 +7.14375 SPLITY 2
    MESHZ -8.25500 +8.25500 SPLITZ 2
    RADIUS 0.0 5.16890 6.58750
    MIX 1 2 3
  ;
  ;
TRACK BCTRK := EXCEL: BC ::
  TITLE 'TCM04: TWO GROUPS CANDU 3-D ADJUSTER ROD ASSEMBLY '
  MAXR 40 TRAK TISO 4 2.5
  ;
SYS := ASM: MACRO TRACK BCTRK :: ;
SYS2 TRACK2 := EXCELL: BC MACRO ::
  TITLE 'TCM04: TWO GROUPS CANDU 3-D ADJUSTER ROD ASSEMBLY '
  MAXR 40 TRAK NORM TISO 4 2.5
  ;
*-----
* Solution : K-EFFECTIVE
* Editing : Compute reference reaction rates
*-----
FLUX := FLU: SYS MACRO TRACK ::
  TYPE K
  ;
EDITION := EDI: FLUX MACRO TRACK ::
  EDIT 3 UPS MERG COMP SAVE ON 'NOROD'

```

```

;
FLUX := FLU: FLUX SYS2 MACRO TRACK2 ::
  TYPE K
;
EDITION := EDI: EDITION FLUX MACRO TRACK2 ::
  EDIT 3 UPS  MERG COMP STAT ALL REFE 'NOROD'
;
EDITION2 := EDI: FLUX MACRO TRACK2 ::
  EDIT 3 UPS  MERG COMP SAVE ON 'NOROD'
;
SYS SYS2 TRACK2 := DELETE: SYS SYS2 TRACK2 ;
*-----
*  Modify Macrolib for adjuster rod material
*  Solution : K-EFFECTIVE
*  Editing  : Compute Delta-Sigma
*-----
MACRO := MAC: MACRO ::
  READ INPUT
  MIX 4  TOTAL      6.96358740E-1 1.12379551E+0
          SCAT 2 2   2.55611958E-4 6.77430272E-1
          2 2   9.55488145E-1 3.16311372E-3
;
SYS := ASM: MACRO TRACK BCTRK ::
;
SYS2 TRACK2 := EXCELL: BC MACRO ::
  TITLE 'TCM04: TWO GROUPS CANDU 3-D ADJUSTER ROD ASSEMBLY '
  MAXR 40 TRAK NORM TISO 4 2.5
;
FLUX := FLU: FLUX SYS MACRO TRACK ::
  TYPE K
;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
  EDIT 3 UPS  MERG COMP STAT DELS REFE 'NOROD'
;
FLUX := FLU: FLUX SYS2 MACRO TRACK2 ::
  TYPE K
;
EDITION2 := EDI: EDITION2 FLUX MACRO TRACK2 ::
  EDIT 3 UPS  MERG COMP STAT DELS REFE 'NOROD'
;
BCTRK := DELETE: BCTRK ;
END: ;
QUIT "LIST" .

```

#### 4.3.5 TCM05 – Comparison of leakage models

This test presents various homogeneous and heterogeneous leakage models on a simple cell (see Figure 20).<sup>[82]</sup>

Input data for test case: **TCM05.x2m**

```

*-----
*   TEST CASE TCM05
*   MACROSCOPIC CROSS SECTIONS
*   FISSION SOURCE PROBLEM
*   2-D CARTESIAN/ANNULAR CELL
*   Validating leakage options
*   TYPE K B L FOR MOSTELC (NO VOID)
*   TYPE K B L FOR MOSTELCV (MOSTELC WITH VOID)
*
*-----
*   Define STRUCTURES and MODULES used
*-----
LINKED_LIST
  MOSTELC MOSTELCV TRACK MACRO SYS FLUX EDITION ;
SEQ_BINARY
  TRKSPC ;
MODULE
  GEO: EXCELT: MAC: ASM: FLU: EDI: DELETE: END: ;
*-----
*   Macroscopic XS
*-----
MACRO := MAC: ::
  NGRO 2 ANIS 2 NMIX 2 NIFI 1
  READ INPUT
  MIX 1   TOTAL           0.222222  0.833333
    SCAT   1 1  0.19222 2 2  0.75333  0.02
          1 1  0.1    2 2  0.5      0.01
    NUSIGF    0.0      0.135  CHI          1.0      0.0
  MIX 2   TOTAL           0.166667  1.111111
    SCAT   2 2  0.00015  0.126667 2 2  1.10111  0.04
          2 2  0.0001   0.1      2 2  0.5      0.01
  ;
*-----
*   Geometry : MOSTELC  - Cartesian 2D cell without void region
*               MOSTELCV - Cartesian 2D cell with void region
*-----
MOSTELC := GEO: :: CARCEL 2
  X- REFL X+ REFL   Y- REFL Y+ REFL
  MESHX 0.0 1.26209  MESHY 0.0 1.26209
  RADIUS 0.0 0.39306 0.45802 SPLITR 2 1
  MIX 1 2 2 ;
MOSTELCV := GEO: MOSTELC ::
  MIX 1 0 2 ;
*-----
*   Tracking : EXCELT - MOSTELC
*               ANIS 2 for adequate dimensions in PIJK
*   Solution : TYPE K, B or L
*   Leakage  : B1 PNL, B1 HETE
*-----
TRACK TRKSPC := EXCELT: MOSTELC ::

```

```

      TITLE 'TCM05: ANNULAR GEOMETRY WITH MACROSCOPIC XS'
      MAXR 5 ANIS 2 TRAK TISO 12 20.0 ;
      SYS := ASM: MACRO TRACK TRKSPC ::
      PIJK ;
      FLUX := FLU:          SYS MACRO TRACK ::
      TYPE K ;
      EDITION := EDI:          FLUX MACRO TRACK ::
      EDIT 2 SAVE ;
      FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE K B1 PNL BUCK 1.51429E-03 ;
      EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 2 SAVE ;
      FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE B B1 PNL KEFF 1.199538 ;
      EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 2 SAVE ;
      FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE B B1 PNL ;
      EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 2 SAVE ;
      FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE L B1 PNL ;
      EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 2 SAVE ;
      FLUX := DELETE: FLUX ;
      FLUX := FLU:          SYS MACRO TRACK ::
      TYPE K B1 HETE BUCK 1.50298E-03 ;
      EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 2 SAVE ;
      FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE B B1 HETE KEFF 1.199538 ;
      EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 2 SAVE ;
      FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE B B1 HETE R BUCK Z 5.00993E-04 ;
      EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 2 SAVE ;
      FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE B B1 HETE Z BUCK R 1.001986E-03 ;
      EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 2 SAVE ;
      FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE B B1 HETE ;
      EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 2 SAVE ;
      FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE L B1 HETE R BUCK Z 5.00993E-04 ;
      EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 2 SAVE ;
      FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE L B1 HETE Z BUCK R 1.001986E-03 ;
      EDITION := EDI: EDITION FLUX MACRO TRACK ::

```

```

EDIT 2 SAVE ;
FLUX := FLU: FLUX SYS MACRO TRACK ::
  TYPE L B1 HETE ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
  EDIT 2 SAVE ;
FLUX SYS := DELETE: FLUX SYS ;
*-----
*   Tracking : EXCELT - MOSTELCV only update TRACK TRKSPC files
*               since only change is in one material
*   Solution : TYPE K, B or L
*   Leakage  : B1 PNL, B1 HETE
*-----
TRACK TRKSPC := EXCELT: TRACK TRKSPC MOSTELCV ::
  TITLE 'TCM05: ANNULAR GEOMETRY WITH MACROSCOPIC XS (VOID)' ;
SYS := ASM: MACRO TRACK TRKSPC ::
  PIJK ;
FLUX := FLU:          SYS MACRO TRACK ::
  TYPE K ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
  EDIT 2 SAVE ;
FLUX := FLU: FLUX SYS MACRO TRACK ::
  TYPE K B1 PNL BUCK 1.40181E-03 ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
  EDIT 2 SAVE ;
FLUX := FLU: FLUX SYS MACRO TRACK ::
  TYPE B B1 PNL KEFF 1.228007 ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
  EDIT 2 SAVE ;
FLUX := FLU: FLUX SYS MACRO TRACK ::
  TYPE B B1 PNL ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
  EDIT 2 SAVE ;
FLUX := FLU: FLUX SYS MACRO TRACK ::
  TYPE L B1 PNL ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
  EDIT 2 SAVE ;
FLUX := DELETE: FLUX ;
FLUX := FLU:          SYS MACRO TRACK ::
  TYPE K B1 HETE BUCK 1.40181E-03 ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
  EDIT 2 SAVE ;
FLUX := FLU: FLUX SYS MACRO TRACK ::
  TYPE B B1 HETE KEFF 1.228007 ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
  EDIT 2 SAVE ;
FLUX := FLU: FLUX SYS MACRO TRACK ::
  TYPE B B1 HETE R BUCK Z 5.00993E-04 ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
  EDIT 2 SAVE ;
FLUX := FLU: FLUX SYS MACRO TRACK ::
  TYPE B B1 HETE Z BUCK R 1.001986E-03 ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::

```

```

      EDIT 2 SAVE ;
FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE B B1 HETE ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 2 SAVE ;
FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE L B1 HETE R BUCK Z 5.00993E-04 ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 2 SAVE ;
FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE L B1 HETE Z BUCK R 1.001986E-03 ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 2 SAVE ;
FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE L B1 HETE ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 2 SAVE ;
TRKSPC := DELETE: TRKSPC ;
END: ;
QUIT "LIST" .

```

#### 4.3.6 TCM06 – Buckling search without fission source

This test is for an homogeneous water cell. A buckling eigenvalue problem is solved in the absence of fission source for the neutron flux distribution inside this cell.

Input data for test case: **TCM06.x2m**

```

*-----
*   TEST CASE TCM06
*   MACROSCOPIC CROSS SECTIONS
*   BUCKLING SEARCH PROBLEM WITHOUT FISSION SOURCE
*   HOMOGENEOUS GEOMETRY
*
*   REF: none
*
*-----
*   Define STRUCTURES and MODULES used
*-----
LINKED_LIST
      WATER TRACK MACRO SYS FLUX EDITION ;
MODULE
      GEO: SYBILT: MAC: ASM: FLU: EDI: END: ;
*-----
*   Macroscopic XS
*-----
MACRO := MAC: ::
      EDIT 2 NGRO 1 ANIS 2 NMIX 1 NIFI 0
      READ INPUT
      MIX 1 TOTAL 3.59 SCAT 1 1 3.57 1 1 2.38
      ;

```

```

*-----
*   Geometry :   WATER - Homogeneous geometry
*   Tracking  : SYBILT
*-----
WATER := GEO: :: HOMOG
      MIX 1
      ;
TRACK := SYBILT: WATER ::
      TITLE 'TCM06: ENE6101 EXAM'
      MAXR 1
      ;
*-----
*   Solution : TYPE  L
*   Leakage  : B0 PNL, P0 PNL, B1 PNL, P1 PNL
*-----
SYS := ASM: MACRO TRACK :: ;
FLUX := FLU: SYS MACRO TRACK ::
      TYPE L B0 SIGS EXTE 5 1.0E-5 BUCK -0.07 ;
EDITION := EDI: FLUX MACRO TRACK ::
      EDIT 3 SAVE ;
FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE L P0 SIGS EXTE 5 1.0E-5 BUCK -0.07 ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 3 SAVE ;
FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE L B1 SIGS EXTE 5 1.0E-5 BUCK -0.07 ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 3 SAVE ;
FLUX := FLU: FLUX SYS MACRO TRACK ::
      TYPE L P1 SIGS EXTE 5 1.0E-5 BUCK -0.07 ;
EDITION := EDI: EDITION FLUX MACRO TRACK ::
      EDIT 3 SAVE ;
END: ;
QUIT "LIST" .

```

#### 4.3.7 TCM07 – Test of boundary conditions

This test is for a 2-D Cartesian cell with reflective and void boundary conditions.

Input data for test case: **TCM07.x2m**

```

*-----
*   TEST CASE TCM07
*   MACROSCOPIC CROSS SECTIONS
*   FISSION SOURCE PROBLEM
*   2-D CARTESIAN CELL
*   REFLECTIVE AND VOID BOUNDARY CONDITIONS
*
*   REF: none
*-----
*   Define STRUCTURES and MODULES used

```

```

*-----
LINKED_LIST
  MACRO LATGEOR LATREGR SYSR FLUXR EDITR
    LATGEOV LATREGV SYSV FLUXV EDITV ;
SEQ_BINARY
  TRKR TRKV ;
MODULE
  MAC: GEO: EXCELT: ASM: FLU: EDI: DELETE: END: ;
*-----
* Macroscopic XS
*-----
MACRO := MAC: ::
  NGRO 1 NMIX 2 NIFI 1
  READ INPUT
  MIX 1 TOTAL 0.75 SCAT 1 1 0.50 NUSIGF 1.00 CHI 1.0
  MIX 2 TOTAL 0.75 SCAT 1 1 0.50
  ;
*-----
* Geometry : LATGEOR - Cartesian 2D with reflection BC
*             LATGEOV - Cartesian 2D with void BC
* Tracking : EXCELT
*-----
LATGEOR := GEO: :: CAR2D 2 2
  X- REFL X+ REFL MESHX 0.00 1.0 2.00 SPLITX 4 4
  Y- REFL Y+ REFL MESHY 0.00 1.0 2.00 SPLITX 4 4
  MIX 1 2 2 2 ;
LATGEOV := GEO: LATGEOR ::
  X- VOID X+ VOID Y- VOID Y+ VOID ;
LATREGR TRKR := EXCELT: LATGEOR ::
  TITLE 'LATHROP *** P1 ANISOTROPE '
  MAXR 64 TRAK TISO 49 20.0 ;
LATREGV TRKV := EXCELT: LATGEOV ::
  TITLE 'LATHROP *** P1 ANISOTROPE '
  MAXR 64 TRAK TISO 49 20.0 ;
*-----
* Solution : TYPE K
*-----
SYSR := ASM: MACRO LATREGR TRKR :: ;
FLUXR := FLU: SYSR MACRO LATREGR ::
  TYPE K ACCE 3 0 ;
EDITR := EDI: FLUXR MACRO LATREGR ::
  EDIT 1 ;
SYSV := ASM: MACRO LATREGV TRKV :: ;
FLUXV := FLU: SYSV MACRO LATREGV ::
  TYPE K ACCE 3 0 ;
EDITV := EDI: FLUXV MACRO LATREGV ::
  EDIT 1 ;
LATGEOR LATREGR SYSR FLUXR EDITR TRKR
  LATGEOV LATREGV SYSV FLUXV EDITV TRKV := DELETE:
LATGEOR LATREGR SYSR FLUXR EDITR TRKR
  LATGEOV LATREGV SYSV FLUXV EDITV TRKV ;
MACRO := DELETE: MACRO ;

```

```
END: ;
QUIT "LIST" .
```

#### 4.3.8 TCM08 – Fixed source problem with fission

This test is for a 2-D Cartesian cell that contains both a fission and a fixed source.

Input data for test case: **TCM08.x2m**

```
*-----
*   TEST CASE TCM08
*   MACROSCOPIC CROSS SECTIONS
*   FIXED SOURCE PROBLEM WITH FISSILE MATERIAL
*   FOR 1/8 7X7 PWR ASSEMBLY
*
*   REF: TCM02
*-----
*   Define STRUCTURES and MODULES used
*-----
LINKED_LIST
  PWRF TRCF SYSF FLUXF EDITF PWRS TRACS SYSS FLUXS EDITS MACRO ;
SEQ_BINARY
  PWRTRKF PWRTRKS ;
MODULE
  GEO: EXCELT: MAC: ASM: FLU: EDI: DELETE: END: ;
*-----
*   Macroscopic XS
*-----
MACRO   :=          MAC:      ::
  NGRO 1 NMIX 4 NIFI 1
  READ INPUT
  MIX 1 TOTAL  1.250  SCAT 1 1  1.242
        NUSIGF 0.15  CHI 1.0
  MIX 2 TOTAL  0.625  SCAT 1 1  0.355
        FIXE 0.000
  MIX 3 TOTAL 14.000  SCAT 1 1  0.000
        FIXE 1.000
  MIX 4 TOTAL  1.250  SCAT 1 1  1.242
        FIXE 0.000
;
*-----
*   Geometry : PWRF  - Cartesian 2D assembly with fission
*               PWRS  - Cartesian 2D assembly without fission
*   Tracking  : EXCELT
*-----
PWRF     :=          GEO:      :: CAR2D 4 4
X- DIAG  X+ REFL Y- SYME  Y+ DIAG
CELL     P F F F
          F F F
          F F
          F
```

```

::: F := GEO: CARCEL 1
  RADIUS 0.000 0.450
  MIX 2 1
  MESHX -0.625 0.625 SPLITX 2
  MESHY -0.625 0.625 SPLITY 2 ;
::: P := GEO: F
  MIX 3 1
  SPLITR 3 ;
;
PWRS := GEO: :: CAR2D 4 4
X- DIAG X+ REFL Y- SYME Y+ DIAG
CELL P F F F
      F F F
      F F
      F
::: F := GEO: CARCEL 1
  RADIUS 0.000 0.450
  MIX 2 4
  MESHX -0.625 0.625 SPLITX 2
  MESHY -0.625 0.625 SPLITY 2 ;
::: P := GEO: F
  MIX 3 4
  SPLITR 3 ;
;
TRACF PWRTRKF := EXCELT: PWRF ::
  TITLE 'TCM08: STANKOVSKI PWR ASSEMBLY'
  MAXR 58 TRAK TISO 12 8.0 ;
SYSF := ASM: MACRO TRACF PWRTRKF :: ;
TRACS PWRTRKS := EXCELT: PWRS ::
  TITLE 'TCM08: STANKOVSKI PWR ASSEMBLY'
  MAXR 58 TRAK TISO 12 8.0 ;
SYSS := ASM: MACRO TRACS PWRTRKS :: ;
*-----
* Solution : TYPE K to test if k < 1.0
*             TYPE S to include fixed source
*-----
FLUXF := FLU: SYSF MACRO TRACF ::
  TYPE K ;
EDITF := EDI: FLUXF MACRO TRACF ::
  EDIT 2 SAVE
  MERGE REGION
    1 1 1 2 3 4 3 4 5 6 5 6 7 8 7 8
    9 10 9 10 9 10 11 12 11 12 11 12 11 12 13 14 13 14 13 14
    15 16 15 16 15 16 17 18 17 18 17 18 17 18
    19 20 19 20 19 20 ;
EDITF := DELETE: EDITF ;
*-----
* SINCE KEFF < 1 DO FIXED SOURCE PROBLEM
* (FIXED AND FISSION SOURCES TAKEN INTO ACCOUNT)
*-----
FLUXF := FLU: FLUXF SYSF MACRO TRACF ::
  TYPE S ;

```

```

EDITF := EDI: FLUXF MACRO TRACF ::
  EDIT 2 SAVE
  MERGE REGION
    1 1 1 2 3 4 3 4 5 6 5 6 7 8 7 8
    9 10 9 10 9 10 11 12 11 12 11 12 11 12 13 14 13 14 13 14
    15 16 15 16 15 16 17 18 17 18 17 18 17 18
    19 20 19 20 19 20 ;
*-----
*   Solution : TYPE S only since no fission
*-----
*
*   IF KEFF < 1 DO FIXED SOURCE PROBLEM PROBLEM
*   (FIXED AND FISSION SOURCES TAKEN INTO ACCOUNT)
*
FLUXS := FLU: SYSS MACRO TRACS ::
  TYPE S ;
EDITS := EDI: FLUXS MACRO TRACS ::
  EDIT 2 SAVE
  MERGE REGION
    1 1 1 2 3 4 3 4 5 6 5 6 7 8 7 8
    9 10 9 10 9 10 11 12 11 12 11 12 11 12 13 14 13 14 13 14
    15 16 15 16 15 16 17 18 17 18 17 18 17 18
    19 20 19 20 19 20 ;
PWRTRKS PWRTRKF := DELETE: PWRTRKS PWRTRKF ;
END: ;
QUIT "LIST" .

```

#### 4.3.9 TCM09 – Solution of a 2-D problem using the MOCC: module

This test case is for a  $3 \times 3$  Cartesian assembly in 2-D similar to TCM03. It is solved using the method of cyclic characteristics.

Input data for test case: **TCM09.x2m**

```

*-----
* TEST CASE TCM09
* MACROSCOPIC CROSS SECTIONS
* FIXED SOURCE PROBLEM
* CARTESIAN 3 X 3 ASSEMBLY
* WATANABE-MAYNARD PROBLEM SIMILAR TO TCM03
*
* REF: R. Roy, "The Cyclic Characteristics Method,"
*       Int. Conf. Physics of Nuclear Science and Technology,
*       Long Island, NY, October 1998, pp. 407-414.
*-----
*
LINKED_LIST WATA WAT24 TRACK MACRO FLUX EDITION ;
SEQ_BINARY WATATRK ;
STRING PolarAng := "CACB" ;
MODULE GEO: EXCELT: MAC: MOCC: EDI: DELETE: END: ;
* MACROSCOPIC CROSS SECTIONS

```

[illegible]

```

                                0  0  0  0
                                0  0  0
                                10  0
                                0

;
* FLUX AT X=5.625CM FOR 24X24
EDITION := EDI: EDITION  FLUX MACRO TRACK ::
EDIT 2 SAVE
MERGE REGION
0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0
  0 0 0 0 0 0 0 0 0 0 0 0 0 0 2 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 3 0 0 0 0 0 0 0 0 0 0 0 0 0
      0 0 0 0 0 0 0 0 0 0 0 0 0 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0
        0 0 0 0 0 0 0 0 0 0 0 0 0 0 5 0 0 0 0 0 0 0 0 0 0 0 0 0
          0 0 0 0 0 0 0 0 0 0 0 0 0 0 6 0 0 0 0 0 0 0 0 0 0 0 0 0
            0 0 0 0 0 0 0 0 0 0 0 0 0 0 7 0 0 0 0 0 0 0 0 0 0 0 0 0
              0 0 0 0 0 0 0 0 0 0 0 0 0 0 8 0 0 0 0 0 0 0 0 0 0 0 0 0
                0 0 0 0 0 0 0 0 0 0 0 0 0 0 9 0 0 0 0 0 0 0 0 0 0 0 0 0
                  0 0 0 0 0 0 0 0 0 0 0 0 0 0 10 0 0 0 0 0 0 0 0 0 0 0 0 0
                    0 0 0 0 0 0 0 0 0 0 0 0 0 0 11 0 0 0 0 0 0 0 0 0 0 0 0 0
                      0 0 0 0 0 0 0 0 0 0 0 0 0 0 12 0 0 0 0 0 0 0 0 0 0 0 0 0

                                0 13  0  0  0  0  0  0  0  0  0  0  0  0
                                14 15 16 17 18 19 20 21 22 23 24
                                    0  0  0  0  0  0  0  0  0  0  0
                                        0  0  0  0  0  0  0  0  0  0
                                            0  0  0  0  0  0  0  0
                                                0  0  0  0  0  0  0  0
                                                    0  0  0  0  0  0  0  0
                                                        0  0  0  0  0  0  0  0
                                                            0  0  0  0  0  0  0  0
                                                                0  0
                                                                    0

;
WATATRK := DELETE: WATATRK ;
END: ;
QUIT "LIST" .

```

#### 4.3.10 TCM10 – Solution of a 2-D problem using the MOCC: module

This test is for a 2-D Cartesian assembly that contains a fixed source. It is solved using the method of cyclic characteristics.

Input data for test case: **TCM10.x2m**

```

*
* TEST CASE TCM11
* MACROSCOPIC CROSS SECTIONS
* FIXED SOURCE PROBLEM
* CARTESIAN 2 X 2 ASSEMBLY

```

```

* TSAI-LOYALKA SEMI-INFINITE PROBLEM
*
* REF: R. Roy, "The Cyclic Characteristics Method,"
*       Int. Conf. Physics of Nuclear Science and Technology,
*       Long Island, NY, October 1998, pp. 407-414.
*
LINKED_LIST LOYA LOY25 TRACK FLUX EDITION
          MACRO MACRO100 MACRO050 MACRO010 MACRO005 MACRO000 ;
SEQ_BINARY LOYATRK ;
STRING PolarAng := "CACB" ;
MODULE GEO: EXCELT: MAC: MOCC: EDI: DELETE: END: ;
INTEGER i n := 1 1 ;
*
* MACROSCOPIC CROSS SECTIONS
MACRO100 := MAC: ::
  NGRO 1 NMIX 2
  READ INPUT
    MIX 1 TOTAL 1.0 SCAT 1 1 1.00 FIXE 1.0
    MIX 2 TOTAL 1.0 SCAT 1 1 1.00 ;
MACRO050 := MAC: ::
  NGRO 1 NMIX 2
  READ INPUT
    MIX 1 TOTAL 1.0 SCAT 1 1 0.50 FIXE 1.0
    MIX 2 TOTAL 1.0 SCAT 1 1 0.50 ;
MACRO010 := MAC: ::
  NGRO 1 NMIX 2
  READ INPUT
    MIX 1 TOTAL 1.0 SCAT 1 1 0.10 FIXE 1.0
    MIX 2 TOTAL 1.0 SCAT 1 1 0.10 ;
MACRO005 := MAC: ::
  NGRO 1 NMIX 2
  READ INPUT
    MIX 1 TOTAL 1.0 SCAT 1 1 0.05 FIXE 1.0
    MIX 2 TOTAL 1.0 SCAT 1 1 0.05 ;
MACRO000 := MAC: ::
  NGRO 1 NMIX 2
  READ INPUT
    MIX 1 TOTAL 1.0 SCAT 1 1 0.00 FIXE 1.0
    MIX 2 TOTAL 1.0 SCAT 1 1 0.00 ;
* GEOMETRIES ENTERED WITH SYMMETRIES
* LOYA - 2 X 2 REGIONS
* LOY25 - 25 X 25 REGIONS
LOYA := GEO: :: CAR2D 2 2
  X- REFL X+ VOID
  MESHX 0.00 0.52 1.00
  Y- REFL Y+ REFL
  MESHY 0.00 0.52 1.00
  MIX      1      2
          2      2      ;
LOY25 := GEO: LOYA ::
  SPLITX 13 12
  SPLITY 13 12      ;

```

```

* SOLUTION FOR LOY25
TRACK LOYATRK := EXCELT: LOY25 ::
    TITLE 'TCM03: LOYANABE-MAYNARD 24X24 '
    MAXR 625
    TRAK TSPC 12 100.0 ;
REPEAT
IF i 1 = THEN
    MACRO := MACRO100 ;
ENDIF ;
IF i 2 = THEN
    MACRO := MACRO050 ;
ENDIF ;
IF i 3 = THEN
    MACRO := MACRO010 ;
ENDIF ;
IF i 4 = THEN
    MACRO := MACRO005 ;
ENDIF ;
IF i 5 = THEN
    MACRO := MACRO000 ;
ENDIF ;
FLUX := MOCC: MACRO TRACK LOYATRK ::
    <<PolarAng>> TYPE S ;
* SOLUTION FOR LOY25
* FLUX AT X=Y= 0.50, 0.70 AND 0.98
* SEE TABLE 2. (ref. p. 412)
EDITION := EDI: FLUX MACRO TRACK ::
    EDIT 2 SAVE
    MERGE REGION
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 2 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

```

```

0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 3
;
FLUX MACRO EDITION := DELETE: FLUX MACRO EDITION ;
EVALUATE i := i 1 + ;
UNTIL i 6 = ;
LOYATRK := DELETE: LOYATRK ;
END: ;
QUIT "LIST" .

```

#### 4.3.11 **TCM11** – Solution of a 2-D problem using the MOCC: module

This test case is for a  $4 \times 4$  Cartesian assembly in 2-D. It is solved using the method of cyclic characteristics and the method of collision probabilities using specular (mirror like) boundary conditions.

Input data for test case: **TCM11.x2m**

```

*
* TEST CASE TCM12
* MACROSCOPIC CROSS SECTIONS
* FIXED SOURCE PROBLEM
* CARTESIAN 4 X 4 ASSEMBLY WITH FUEL RODS AND POISON
* KAVENOKY BENCHMARK
*
* REF: R. Roy, "The Cyclic Characteristics Method,"
*      Int. Conf. Physics of Nuclear Science and Technology,
*      Long Island, NY, October 1998, pp. 407-414.
*
STRING Polar_Ang := "CACB" ;
INTEGER  Nazimuth  := 8 ;
REAL     DenTrak   := 100. ;
INTEGER  Nsplit    := 5 ;
REAL     Tolerance := 5.E-6 ;
LINKED_LIST PWR TRACK MACRO SYS FLUX EDITION ;
SEQ_BINARY PWRTRK ;
MODULE GEO: EXCELT: MAC: MOCC: EDI: END: DELETE: GREP: ;
REAL ou := 100. ;
REAL
  f1 f2 f3 f8 f9 f10 f11 f12 f13 f14 f15
  v1 v2 v3 v8 v9 v10 v11 v12 v13 v14 v15 ;
REAL
  r1      r2      r3
              r8      r9      r10
  r11     r12     r13     r14     r15 :=
  5.166   3.699   4.183
              3.178  3.617  0.2847
  2.913   3.441   3.937   3.225   3.673 ;

```

```

REAL
  e1      e2      e3
          e8      e9      e10
  e11     e12     e13     e14     e15  :=
  0.11    0.08    0.07
          0.04    0.05    0.002
  0.03    0.03    0.04    0.05    0.05 ;

EVALUATE
  e1      e2      e3
          e8      e9      e10
  e11     e12     e13     e14     e15  :=
  e1 r1 / e2 r2 / e3 r3 /
          e8 r8 / e9 r9 / e10 r10 /
  e11 r11 / e12 r12 / e13 r13 / e14 r14 / e15 r15 / ;

EVALUATE
  e1      e2      e3
          e8      e9      e10
  e11     e12     e13     e14     e15  :=
  e1 ou * e2 ou * e3 ou *
          e8 ou * e9 ou * e10 ou *
  e11 ou * e12 ou * e13 ou * e14 ou * e15 ou * ;

*-----
* Macroscopic XS
*-----
MACRO := MAC: ::
  NGRO 1 NMIX 19
  READ INPUT
  MIX 1 TOTAL 1.250 SCAT 1 1 1.242 FIXE 1.000
  MIX 2 TOTAL 0.625 SCAT 1 1 0.355 FIXE 0.000
  MIX 3 TOTAL 1.250 SCAT 1 1 1.242 FIXE 1.000
  MIX 4 TOTAL 0.625 SCAT 1 1 0.355 FIXE 0.000
  MIX 5 TOTAL 1.250 SCAT 1 1 1.242 FIXE 1.000
  MIX 6 TOTAL 0.625 SCAT 1 1 0.355 FIXE 0.000
  MIX 7 TOTAL 1.250 SCAT 1 1 1.242 FIXE 1.000
  MIX 8 TOTAL 0.625 SCAT 1 1 0.355 FIXE 0.000
  MIX 9 TOTAL 1.250 SCAT 1 1 1.242 FIXE 1.000
  MIX 10 TOTAL 14.000 SCAT 1 1 0.000 FIXE 0.000
  MIX 11 TOTAL 1.250 SCAT 1 1 1.242 FIXE 1.000
  MIX 12 TOTAL 0.625 SCAT 1 1 0.355 FIXE 0.000
  MIX 13 TOTAL 1.250 SCAT 1 1 1.242 FIXE 1.000
  MIX 14 TOTAL 0.625 SCAT 1 1 0.355 FIXE 0.000
  MIX 15 TOTAL 1.250 SCAT 1 1 1.242 FIXE 1.000
  MIX 16 TOTAL 0.625 SCAT 1 1 0.355 FIXE 0.000
  MIX 17 TOTAL 1.250 SCAT 1 1 1.242 FIXE 1.000
  MIX 18 TOTAL 0.625 SCAT 1 1 0.355 FIXE 0.000
  MIX 19 TOTAL 1.250 SCAT 1 1 1.242 FIXE 1.000
  ;

*-----
* Geometry : PWR - Cartesian 7x7
* Tracking : EXCELT
*-----
PWR := GEO: :: CAR2D 4 4

```

```

X- DIAG  X+ REFL Y- SYME  Y+ DIAG
CELL  WA  F2  F4  F6
        F8  P10 F12
        F14 F16
        F18
::: WA := GEO: CAR2D 1 1
  MESHX -0.625  0.625 SPLITX <<Nsplitt>>
  MESHY -0.625  0.625 SPLITX <<Nsplitt>>
  MIX      1      ;
::: F2 := GEO: CARCEL 1
  MESHX -0.625  0.625 SPLITX <<Nsplitt>>
  MESHY -0.625  0.625 SPLITX <<Nsplitt>>
  RADIUS 0.000 0.450
  MIX      2      3      ;
::: F4 := GEO: F2
  MIX      4      5      ;
::: F6 := GEO: F2
  MIX      6      7      ;
::: F8 := GEO: F2
  MIX      8      9      ;
::: P10 := GEO: F2
  MIX      10     11 SPLITR 3 ;
::: F12 := GEO: F2
  MIX      12     13     ;
::: F14 := GEO: F2
  MIX      14     15     ;
::: F16 := GEO: F2
  MIX      16     17     ;
::: F18 := GEO: F2
  MIX      18     19     ;
;
TRACK PWRTRK := EXCELT: PWR ::
  MAXR 300 TRAK TSPC <<Nazimuth>> <<DenTrak>> ;
FLUX := MOCC: MACRO TRACK PWRTRK ::
  <<Polar_Ang>> TYPE S
  THER <<Tolerance>> 100 EXTE <<Tolerance>> 100 ;
EDITION := EDI: FLUX MACRO TRACK ::
  EDIT 2 SAVE
  MERGE MIX 1 2 3 0 0 0 0 4 5 6 7 8 9 10 11 0 0 0 0 ;
GREP: EDITION ::
  STEP UP 'REF-CASE 1' STEP UP MACROLIB
  GETVAL VOLUME 1 11
  >>v1<< >>v2<< >>v3<< >>v8<< >>v9<< >>v10<<
  >>v11<< >>v12<< >>v13<< >>v14<< >>v15<<
  STEP UP 'GROUP 1/ 1'
  GETVAL FLUX-INTG 1 11
  >>f1<< >>f2<< >>f3<< >>f8<< >>f9<< >>f10<<
  >>f11<< >>f12<< >>f13<< >>f14<< >>f15<<
  STEP DOWN
  STEP DOWN STEP DOWN ;
EVALUATE f1 f2 f3 f8 f9 f10 f11 f12 f13 f14 f15 :=
          f1 v1 / r1 - r1 / ou *

```

```

      f2 v2 / r2 - r2 / ou *
      f3 v3 / r3 - r3 / ou *
      f8 v8 / r8 - r8 / ou *
      f9 v9 / r9 - r9 / ou *
      f10 v10 / r10 - r10 / ou *
      f11 v11 / r11 - r11 / ou *
      f12 v12 / r12 - r12 / ou *
      f13 v13 / r13 - r13 / ou *
      f14 v14 / r14 - r14 / ou *
      f15 v15 / r15 - r15 / ou *

      ;
* SOLUTION FOR KAVENORY BENCHMARK
* FLUX VALUES COMPARED TO MONTE-CARLO RESULTS
* SEE TABLE 3. (ref. p. 412)
ECHO "DF( 1/ 3)%=" f1 f2 f3 ;
ECHO "DF( 8/ 9)%="      f8 f9 ;
ECHO "DF(10/12)%=" f10 f11 f12 ;
ECHO "DF(13/15)%=" f13 f14 f15 ;
ECHO "ACCEPT=" f1 ABS e1 <= f2 ABS e2 <= f3 ABS e3 <= ;
ECHO "ACCEPT="      f8 ABS e8 <= f9 ABS e9 <= ;
ECHO "ACCEPT=" f10 ABS e10 <= f11 ABS e11 <= f12 ABS e12 <= ;
ECHO "ACCEPT=" f13 ABS e13 <= f14 ABS e14 <= f15 ABS e15 <= ;
PWRTRK := DELETE: PWRTRK ;
END: ;
QUIT .

```

#### 4.3.12 **TCM12** - Solution of a 3-D problem using the **MCU:** module

This test is for a simplified 3-D Cartesian assembly analyzed using the **EXCELT:**. A collisions probability solution is generated as well as two solutions using the method of characteristics.

Input data for test case: **TCM12.x2m**

```

*-----
* TEST CASE TCM12
* MACROSCOPIC CROSS SECTIONS
* 3-D CARTESIAN ASSEMBLY
* USE the 3-D CHARACTERISTICS MODULE MCU:
* 1) TEST1: USE TRACKING FILE
* 2) TEST2: USE EXCELL TRACKING TYPE
*-----
* Define STRUCTURES and MODULES used
*-----
MODULE   MAC: GEO: MCU: END: EXCELT: DELETE: EXCELL: FLU: ASM: ;
LINKED_LIST MACRO GEOM T3D FLUXA PIJMatrix ;
SEQ_BINARY IntLine      ;

```

```

REAL      DenTra := 10.0      ;
INTEGER   AngTra := 4        ;
STRING    Itlm   ;
EVALUATE  Itlm := "ITLM"     ;
STRING    Prll   := "STRD"   ;
INTEGER   Merg   ;
EVALUATE  Merg := 0          ;
STRING    Etab   ;
EVALUATE  Etab := "OFF"      ;
STRING    jacc   ;
EVALUATE  jacc := "JACC"     ;
* Validate input options
IF Itlm "ITLM" = NOT THEN
    EVALUATE Itlm := " "      ;
ENDIF ;
*
*-----
* Macroscopic cross sections
*-----
MACRO := MAC: ::
EDIT 0 NGRO 7 NMIX 7 NIFI 1
ENER 1.0E7 1.0E5 1.0E3 10.0 4.0 0.625 0.025 0.001
READ INPUT
MIX      1
  EFISS  200.0
  NFTOT  7.21206E-03 8.19301E-04 6.45320E-03 1.85648E-02
        1.78084E-02 8.30348E-02 2.16004E-01
  NUSIGF 2.00600E-02 2.02730E-03 1.57060E-02 4.51830E-02
        4.33421E-02 2.02090E-01 5.25711E-01
  CHI    5.87910E-01 4.11760E-01 3.39060E-04 1.17610E-07
        0.00000E+00 0.00000E+00 0.00000E+00
  TOTAL  1.77949E-01 3.29805E-01 4.80388E-01 5.54367E-01
        3.11801E-01 3.95168E-01 5.64406E-01
  SCAT   1      1 1.27537E-01
        2      2 3.24456E-01 4.23780E-02
        3      3 4.50940E-01 1.63140E-03 9.43740E-06
        5      5 1.25250E-04 4.52565E-01 2.67920E-03
        3      6 1.29680E-03 2.71401E-01 5.56640E-03
        3      7 8.54580E-03 2.65802E-01 1.02550E-02
        3      7 2.73080E-01 1.68090E-02 1.00210E-08
MIX      2
  EFISS  200.0
  NFTOT  8.25446E-03 1.32565E-03 8.42156E-03 3.28730E-02
        1.59636E-02 3.23794E-01 3.62803E-01
  NUSIGF 2.38140E-02 3.85869E-03 2.41340E-02 9.43662E-02
        4.57699E-02 9.28181E-01 1.04320E+00
  CHI    5.87910E-01 4.11760E-01 3.39060E-04 1.17610E-07
        0.00000E+00 0.00000E+00 0.00000E+00
  TOTAL  1.81323E-01 3.34368E-01 4.93785E-01 5.91216E-01
        4.74198E-01 8.33601E-01 8.53603E-01
  SCAT   1      1 1.30457E-01

```

```

      2      2 3.28428E-01 4.17920E-02
      3      3 4.58371E-01 1.64360E-03 8.51050E-06
      5      5 1.76190E-04 4.63709E-01 2.53310E-03
          2.20170E-09 5.13290E-09
      3      6 2.27600E-03 2.82313E-01 5.47660E-03
      3      7 8.86450E-03 2.49751E-01 8.72890E-03
      3      7 2.59529E-01 1.31140E-02 9.00160E-09

MIX      3
TOTAL    1.26032E-01 2.93160E-01 2.84240E-01 2.80960E-01
          3.34440E-01 5.65640E-01 1.17215E+00
SCAT     1      1 6.61659E-02
          2      2 2.40377E-01 5.90700E-02
          3      3 1.83297E-01 5.24350E-02 2.83340E-04
          5      5 3.73330E-05 7.88511E-02 9.23970E-02
          2.49900E-04 1.46220E-06
          6      6 9.17260E-04 9.97372E-02 1.70140E-01
          6.94460E-03 1.92390E-05 2.06420E-08
          6      7 4.97920E-02 3.16765E-01 2.06790E-01
          2.58810E-02 1.08030E-03 2.98750E-06
          6      7 1.09912E+00 2.38770E-01 2.44780E-02
          4.92970E-03 2.05670E-04 4.21400E-07

MIX      4
TOTAL    1.59206E-01 4.12970E-01 5.90310E-01 5.84350E-01
          7.18000E-01 1.25445E+00 2.65038E+00
SCAT     1      1 4.44777E-02
          2      2 2.82334E-01 1.13400E-01
          3      3 3.45256E-01 1.29940E-01 7.23470E-04
          5      5 7.14370E-05 9.10284E-02 2.24570E-01
          6.23400E-04 3.74990E-06
          6      6 2.21570E-03 1.39138E-01 4.15510E-01
          1.69990E-02 4.80020E-05 5.31840E-08
          6      7 1.32440E-01 6.99913E-01 5.11820E-01
          6.37320E-02 2.64430E-03 7.44860E-06
          6      7 2.48070E+00 5.37320E-01 6.12290E-02
          1.21390E-02 5.03440E-04 1.04550E-06

;
*-----
* Geometry
*-----
GEOM := GEO: :: CAR3D 4 4 2
X- DIAG X+ REFL Y- DIAG Y- SSYM Z- SSYM Z+ REFL
CELL
C1 C1 C1 C1
C6 C6 C6
C6 C6
C6
C7 C7 C7 C7
C7 C7 C7
C7 C7
C7
::: C1 := GEO: CARCELZ 1 1

```

```

    MESHX 0.0 1.26  MESHY 0.0 1.26  MESHZ 0.0 1.26
    RADIUS 0.0 0.54  MIX 1 2 ;
    ::: C6 := GEO: C1  MIX 3 3 ;
    ::: C7 := GEO: C1  MESHZ 0.0 1.26
        MIX 4 4 ;
;
*-----
* Use EXCELL
*-----
PIJMatrix T3D := EXCELL: GEOM  MACRO ::
    MAXR 400
    TRAK SUBG 1 TISO 4 10.0 ;
FLUXA := FLU: MACRO PIJMatrix T3D ::
    TYPE K ;
FLUXA T3D PIJMatrix := DELETE: FLUXA T3D PIJMatrix ;
*-----
* Use EXCELt to track then ASM+FLU or MCU
*-----
T3D  IntLine := EXCELt: GEOM  MACRO ::
    EDIT 0 MAXR 400
        TRAK TISO <<AngTra>> <<DenTra>> ;
PIJMatrix := ASM: MACRO T3D  IntLine ;
FLUXA := FLU: PIJMatrix MACRO T3D ::
    TYPE K ;
FLUXA := DELETE: FLUXA ;
FLUXA := MCU: T3D  IntLine  MACRO ::
    TYPE K
    ETAB <<Etab>>
    CURR DIRT <<Itlm>> ;
FLUXA T3D IntLine := DELETE: FLUXA T3D IntLine ;
*-----
* MCU: Use EXCELL tracking option
*-----
FLUXA T3D := MCU: GEOM  MACRO ::
    TYPE K
    ETAB <<Etab>>
    CURR DIRT <<Itlm>>
    MAXR 400
    TRAK TISO <<AngTra>> <<DenTra>> ;
FLUXA T3D := DELETE: FLUXA T3D ;
GEOM MACRO := DELETE: GEOM MACRO ;
END: ;
QUIT .

```

#### 4.4 WLUP microscopic cross section examples

The test cases we will consider here use the **LIB:** module to enter microscopic cross sections taken from a WIMS-D4 format library. We will assume that this library is located in file **iaea** downloaded from the web site.<sup>[31]</sup> The test cases are numbered successively from **TCWU01** to **TCWU14**.

## 4.4.1 TCWU01 – The Mosteller benchmark

This benchmark uses both a cartesian 2-D cell with a central annular pin and an equivalent annular cell (see Figure 20).<sup>[82]</sup> No depletion information is required in this case since the module EVO: will not be executed. A comparison between various calculation options is provided here. We first consider the annular geometry with a JPMT: self-shielding and a SYBILT: transport calculation. This is then repeated for the cartesian 2-D cell. Finally, we used an isotropic (TISO) and a specular (TSPC) EXCELT: tracking successively for the self-shielding and transport calculations.

Input data for test case: TCWU01.x2m

```
*-----
* TEST CASE TCWU01
* MOSTELLER BENCHMARK: 1-D ANNULAR CELL AND 2-D CARTESIAN CELL
* WIMSD4 69 GROUPS LIBRARY FILE iaea from WLUP
*
* REF: R. Mosteller et al. Nucl. Sci. Eng. 107, 265 (1991)
*
*-----
* Define STRUCTURES and MODULES used
*-----
LINKED_LIST
  MOSTELA MOSTELC DISCR1 DISCR2 LIBRARY CP CALC OUT ;
SEQ_BINARY
  TRKSPC ;
MODULE
  LIB: GEO: JPMT: SYBILT: EXCELT: SHI: ASM: FLU: EDI:
  DELETE: END: ;
*-----
* Microscopic cross sections from file iaea format WIMSD4
*-----
LIBRARY := LIB: ::
  NMIX 3 CTRA WIMS
  MIXS LIB: WIMSD4 FIL: iaea
  MIX 1 600.0
    U235 = '2235' 1.66078E-4 1
    U238 = '8238' 2.28994E-2 1
  MIX 2 600.0
    Zr91 = '91' 3.83243E-2
  MIX 3 600.0
    H1H2O = '3001' 4.42326E-2 O16H2O = '6016' 2.21163E-2
    BNat = '1011' 1.02133E-5
  ;
*-----
* Geometry MOSTELA : annular 3 region geometry
* MOSTELC : Cartesian 3 region geometry
*-----
MOSTELA := GEO: :: TUBE 3
  R+ REFL RADIUS 0.0 0.39306 0.45802 0.71206 SPLITR 2 1 1
  MIX 1 2 3 ;
MOSTELC := GEO: :: CARCEL 2
  X- REFL X+ REFL MESHX 0.0 1.26209
```

```

Y- REFL Y+ REFL MESHY 0.0 1.26209
RADIUS 0.0 0.39306 0.45802 SPLITR 2 1
MIX 1 2 3 ;
*-----
* Case 1 -- annular
* Self-Shielding calculation JPM
* Transport calculation SYBIL
* Flux calculation for K no leakage
*-----
DISCR1 := JPMT: MOSTELA ::
  TITLE 'TCWU01: MOSTELLER BENCHMARK (JPM / SYBIL)'
  MAXR 4 IP01 QUA1 5 ;
LIBRARY := SHI: LIBRARY DISCR1 :: ;
DISCR2 := SYBILT: MOSTELA ::
  TITLE 'TCWU01: MOSTELLER BENCHMARK (JPM / SYBIL)'
  MAXR 4 QUA1 5 ;
CP := ASM: LIBRARY DISCR2 :: ;
CALC := FLU: CP LIBRARY DISCR2 ::
  TYPE K ;
OUT := EDI: CALC LIBRARY DISCR2 ::
  EDIT 4 MERG MIX 1 2 3 COND 4.0 SAVE ;
DISCR1 DISCR2 CP := DELETE: DISCR1 DISCR2 CP ;
*-----
* Case 2 -- Cartesian
* Self-Shielding calculation JPM
* Transport calculation SYBIL
* Flux calculation for K no leakage
*-----
DISCR1 := JPMT: MOSTELC ::
  TITLE 'TCWU01: MOSTELLER BENCHMARK (JPM / SYBIL)'
  MAXR 4 IP01 QUA1 5 QUA2 12 5 ;
LIBRARY := SHI: LIBRARY DISCR1 :: ;
DISCR2 := SYBILT: MOSTELC ::
  TITLE 'TCWU01: MOSTELLER BENCHMARK (JPM / SYBIL)'
  MAXR 4 QUA1 5 QUA2 12 5 ;
CP := ASM: LIBRARY DISCR2 :: ;
CALC := FLU: CALC CP LIBRARY DISCR2 ::
  TYPE K ;
OUT := EDI: OUT CALC LIBRARY DISCR2 ::
  EDIT 1 MERG MIX 1 2 3 COND 4.0 STAT ALL REFE 1 ;
DISCR1 DISCR2 CP := DELETE: DISCR1 DISCR2 CP ;
*-----
* Case 3 -- annular
* Self-Shielding calculation EXCEL-ISO
* Transport calculation EXCEL-ISO
* Flux calculation for K no leakage
*-----
DISCR1 TRKSPC := EXCELT: MOSTELC ::
  TITLE 'TCWU01: MOSTELLER BENCHMARK (EXCELL)'
  MAXR 4 TRAK TISO 12 20.0 ;
LIBRARY := SHI: LIBRARY DISCR1 TRKSPC :: ;
CP := ASM: LIBRARY DISCR1 TRKSPC :: ;

```

```

CALC := FLU: CALC CP LIBRARY DISCR1 ::
  TYPE K ;
OUT := EDI: OUT CALC LIBRARY DISCR1 ::
  EDIT 1 MERG MIX 1 2 3 COND 4.0 STAT ALL REFE 1 ;
DISCR1 TRKSPC CP := DELETE: DISCR1 TRKSPC CP ;
*-----
* Case 4 -- Cartesian
* Self-Shielding calculation EXCEL-SPC
* Transport calculation EXCEL-SPC
* Flux calculation for K no leakage
*-----
DISCR1 TRKSPC := EXCEL: MOSTELC ::
  TITLE 'TCWU01: MOSTELLER BENCHMARK (EXCELL)'
  MAXR 4 TRAK TSPC 12 20.0 ;
LIBRARY := SHI: LIBRARY DISCR1 TRKSPC :: ;
CP := ASM: LIBRARY DISCR1 TRKSPC :: ;
CALC := FLU: CALC CP LIBRARY DISCR1 ::
  TYPE K ;
OUT := EDI: OUT CALC LIBRARY DISCR1 ::
  EDIT 1 MERG MIX 1 2 3 COND 4.0 STAT ALL REFE 1 ;
DISCR1 TRKSPC CP := DELETE: DISCR1 TRKSPC CP ;
END: ;
QUIT "LIST" .

```

#### 4.4.2 TCWU02 – A $17 \times 17$ PWR type assembly

This test case represents a production calculation of a normal PWR assembly with cell grouping (MERGE and TURN options). Its configuration is shown in Figure 21.

Input data for test case: **TCWU02.x2m**

```

*-----
* TEST CASE TCWU02
* 17 X 17 PWR ASSEMBLY WITHOUT POISON
*
* REF: none
*
*-----
* Define STRUCTURES and MODULES used
*-----
LINKED_LIST
  ASSMB DISCR1 DISCR2 LIBRARY CP CALC OUT COMPO ;
SEQ_ASCII
  res ;
MODULE
  LIB: GEO: JPMT: SYBILT: SHI: ASM: FLU: EDI: CPO:
  DELETE: END: ;
*-----
* Microscopic cross sections from file iaea format WIMSD4
*-----
LIBRARY := LIB: ::

```

```

NMIX 8 CTRA WIMS
MIXS LIB: WIMSD4 FIL: iaea
MIX 1 579.9
  H1H2O   = '3001'   4.76690E-2   O16H2O   = '6016'   2.38345E-2
  BNat     = '1011'   2.38103E-5
MIX 2 579.9
  Cr52     = '52'     7.54987E-5   O16       = '6016'   3.06711E-4
  Zr91     = '91'     4.18621E-2   Fe56      = '2056'   1.47624E-4
MIX 3 579.9
  H1H2O   = '3001'   4.65292E-2   O16H2O   = '6016'   2.32646E-2
  Fe56     = '2056'   4.45845E-5   Cr52      = '52'     4.79927E-5
  Mn55     = '55'     4.15901E-7   Ni58      = '58'     1.13521E-4
  BNat     = '1011'   2.32761E-5   MoNat     = '96'     4.03755E-6
  Zr91     = '91'     8.92427E-4   Al27      = '27'     2.35231E-6
MIX 4 579.9
  Cr52     = '52'     7.07291E-5   O16       = '6016'   2.87335E-4
  Zr91     = '91'     3.92175E-2   Fe56      = '2056'   1.38298E-4
MIX 5 579.9
  H1H2O   = '3001'   4.71346E-2   O16H2O   = '6016'   2.35673E-2
  Fe56     = '2056'   2.09013E-5   Cr52      = '52'     2.24991E-5
  Mn55     = '55'     1.94976E-7   Ni58      = '58'     5.32188E-5
  BNat     = '1011'   2.35598E-5   MoNat     = '96'     1.89281E-6
  Zr91     = '91'     4.18372E-4   Al27      = '27'     1.10277E-6
MIX 6 579.9
  H1H2O   = '3001'   4.71676E-2   O16H2O   = '6016'   2.35838E-2
  Fe56     = '2056'   1.96130E-5   Cr52      = '52'     2.11122E-5
  Mn55     = '55'     1.82957E-7   Ni58      = '58'     4.99383E-5
  BNat     = '1011'   2.35753E-5   MoNat     = '96'     1.77614E-6
  Zr91     = '91'     3.92583E-4   Al27      = '27'     1.03479E-6
MIX 7 579.9
  H1H2O   = '3001'   4.72020E-2   O16H2O   = '6016'   2.36010E-2
  Fe56     = '2056'   1.82630E-5   Cr52      = '52'     1.96591E-5
  Mn55     = '55'     1.70365E-7   Ni58      = '58'     4.65011E-5
  BNat     = '1011'   2.35914E-5   MoNat     = '96'     1.65389E-6
  Zr91     = '91'     3.65562E-4   Al27      = '27'     9.63569E-7
MIX 8 933.6
  U235     = '2235'   7.39237E-4 1
  U238     = '8238'   2.17285E-2 1

```

;
\*----

```

* Geometry ASSMB : a 17 X 17 normal PWR assembly
* contains C1 : cell without fuel
*           C2 : normal fuel cell
*           C3 : peripheral cell
*           C4 : corner cell
*-----
ASSMB := GEO: :: CAR2D 9 9
X- DIAG X+ REFL Y- SYME Y+ DIAG
CELL C1 C2 C2 C1 C2 C2 C1 C2 C3
      C2 C2 C2 C2 C2 C2 C2 C3
        C2 C2 C2 C2 C2 C2 C3
          C1 C2 C2 C1 C2 C3
            C2 C2 C2 C2 C3
              C1 C2 C2 C3
                C2 C2 C3
                  C2 C3
                    C4
MERGE 1  3 12 11 12 12 11 12 15
        4  6  5  6  6  5  6  8
          13  5  6  6  5  6  8
            2  5  5 10  5  8
              13  5  5  6  8
                2  5  7  8
                  13  7  8
                    14  8
                      9
TURN  H  H  B  H  H  B  H  H  A
      H  G  G  H  G  G  H  A
        A  E  E  F  E  E  A
          H  H  F  H  H  A
            H  E  G  H  A
              H  H  A  A
                H  A  A
                  A  A
                    A
::: C1 := GEO: CARCEL 2
  MESHX 0.0 1.26472 MESHY 0.0 1.26472
  RADIUS 0.0 0.572435 0.613142 MIX 1 2 3 ;
::: C2 := GEO: C1 RADIUS 0.0 0.412660 0.474364 MIX 8 4 5 ;
::: C3 := GEO: C2 MESHX 0.0 1.31472 MIX 8 4 6 ;
::: C4 := GEO: C3 MESHY 0.0 1.31472 MIX 8 4 7 ;
;
*-----
* Self-Shielding calculation JPM
* Transport calculation SYBIL
* Flux calculation for B1 homogeneous leakage
* Editing using SPH model for transport-diffusion
*-----
DISCR1 := JPMT: ASSMB ::
  TITLE 'TCWU02: 17 X 17 MULTICELL PWR BENCHMARK WITHOUT POISON'
  MAXR 400 OLD ;
  LIBRARY := SHI: LIBRARY DISCR1 :: ;

```

```

DISCR2 := SYBILT: ASSMB ::
  TITLE 'TCWU02: 17 X 17 MULTICELL PWR BENCHMARK WITHOUT POISON'
  MAXR 400 ;
CP := ASM: LIBRARY DISCR2 :: ;
CALC := FLU: CP LIBRARY DISCR2 ::
  TYPE B B1 ;
OUT := EDI: CALC LIBRARY DISCR2 ASSMB ::
  EDIT 3 UPS SAVE COND 4.0 SPH
  ::: BIVACT: PRIM 1 2 EDIT 0 ;
  ;
COMPO := CPO: OUT ::
  EDIT 1 STEP 'REF-CASE 1' EXTRACT ALL NAME COMPO ;
res := COMPO ;
END: ;
QUIT "LIST" .

```

#### 4.4.3 TCWU03 – An hexagonal assembly

This test case represents a production calculation of a typical hexagonal control assembly. Its configuration is presented in Figure 22.

Input data for test case: **TCWU03.x2m**

```

*-----
*  TEST CASE TCWU03
*  MULTICELL HEXAGONAL ASSEMBLY WITH POISON
*  iaea WLUP Library
*
*  REF: none
*
*-----
*  Define STRUCTURES and MODULES used
*-----
LINKED_LIST
  ASSMBH DISCR1 DISCR2 LIBRARY CP CALC OUT COMPO ;
SEQ_ASCII
  res ;
MODULE
  GEO: JPMT: SYBILT: LIB: SHI: ASM: FLU: EDI: CPO:
  DELETE: END: ;
*-----
*  Microscopic cross sections from file iaea format WIMSD4
*-----
LIBRARY := LIB: ::
  NMIX 11 CTRA WIMS
  MIXS LIB: WIMSD4 FIL: iaea
  MIX 1 579.9
    H1H2O   = '3001'    4.76690E-2   O16H2O   = '6016'    2.38345E-2
    BNat    = '1011'    2.38103E-5
  MIX 2 579.9
    Cr52    = '52'      7.54987E-5   Fe56     = '2056'    1.47624E-4

```

Zr91	= '91'	4.18621E-2			
MIX 3 579.9					
H1H2O	= '3001'	4.65292E-2	O16H2O	= '6016'	2.32646E-2
			Cr52	= '52'	4.79927E-5
Fe56	= '2056'	4.45845E-5	Ni58	= '58'	1.13521E-4
			MoNat	= '96'	4.03755E-6
			Al27	= '27'	2.35231E-6
Mn55	= '55'	4.15901E-7			
BNat	= '1011'	2.32761E-5			
Zr91	= '91'	8.92427E-4			
MIX 4 933.6			O16	= '6016'	4.49355E-2
U235	= '2235'	7.39237E-4			
U238	= '8238'	2.17285E-2			
MIX 5 579.9			In115	= '2115'	7.57464E-3
Cd113	= '2113'	2.62493E-3			
Ag109	= '3109'	4.49188E-2			
MIX 6 579.9			Cr52	= '52'	1.52702E-2
Fe56	= '2056'	5.57670E-2	Ni58	= '58'	7.51418E-3
Mn55	= '55'	8.02943E-4			
MIX 7 579.9					
H1H2O	= '3001'	3.06466E-2	O16H2O	= '6016'	1.53233E-2
Fe56	= '2056'	5.27485E-5	Cr52	= '52'	2.69769E-5
BNat	= '1011'	1.53077E-5			
Zr91	= '91'	1.49580E-2			
MIX 8 579.9					
H1H2O	= '3001'	4.65292E-2	O16H2O	= '6016'	2.32646E-2
			Cr52	= '52'	4.79927E-5
Fe56	= '2056'	4.45845E-5	Ni58	= '58'	1.13521E-4
			MoNat	= '96'	4.03755E-6
			Al27	= '27'	2.35231E-6
Mn55	= '55'	4.15901E-7			
BNat	= '1011'	2.32761E-5			
Zr91	= '91'	8.92427E-4			
MIX 9 579.9			O16	= '6016'	2.87335E-4
Cr52	= '52'	7.07291E-5	Fe56	= '2056'	1.38298E-4
Zr91	= '91'	3.92175E-2			
MIX 10 579.9					
H1H2O	= '3001'	4.71346E-2	O16H2O	= '6016'	2.35673E-2
			Cr52	= '52'	2.24991E-5
Fe56	= '2056'	2.09013E-5	Ni58	= '58'	5.32188E-5
			MoNat	= '96'	1.89281E-6
			Al27	= '27'	1.10277E-6
Mn55	= '55'	1.94976E-7	BNat	= '1011'	2.35598E-5
Zr91	= '91'	4.18372E-4			
MIX 11 579.9					
H1H2O	= '3001'	4.71676E-2	O16H2O	= '6016'	2.35838E-2
			Cr52	= '52'	2.11122E-5
Fe56	= '2056'	1.96130E-5	Ni58	= '58'	4.99383E-5
			MoNat	= '96'	1.77614E-6
			Al27	= '27'	1.03479E-6
Mn55	= '55'	1.82957E-7			
BNat	= '1011'	2.35753E-5			

```

      Zr91      = '91'      3.92583E-4
    ;
*-----
*  Geometry ASSMBH : hexagonal assembly with poison
*  contains C1 : cell without fuel
*             C2 : poison cell
*             C3 : normal fuel cell
*             C4 : peripheral cell
*-----
ASSMBH := GEO: :: HEX 36
HBC S30 REFL
CELL C1 C3 C3 C3 C3 C3 C2 C3 C3 C3 C2 C3 C3 C3 C3 C3 C3 C2
    C3 C3 C2 C3 C3 C3 C3 C3 C3 C3 C3 C3 C4 C4 C4 C4 C4 C4
TURN  A  A  A  A  A  A  A  A  A  B  D  A  I  A  C  F  J  B  A
      F  A  A  E  E  A  A  E  A  A  A  A  A  A  A  A  A  A
MERGE  1  2  3  4  5  4  6  7  8  7  9  8 10  7  7  4  7 11
      12 13 14 15 12 16 17 12 16 18 18 19 20 21 21 22 22 23
::: C1 := GEO: HEXCEL 2
    SIDE 0.707297 RADIUS 0.0 0.412282 0.475917
    MIX 1 2 3 ;
::: C2 := GEO: HEXCEL 5
    SIDE 0.707297 RADIUS 0.0 0.25057 0.354359 0.436 0.486 0.6125
    MIX 5 5 5 6 7 8 ;
::: C3 := GEO: C1 MIX 4 9 10 ;
::: C4 := GEO: C3 MIX 4 9 11 ;
;
*-----
*  Self-Shielding calculation JPM
*  Transport calculation SYBIL
*  Flux calculation for B1 homogeneous leakage
*  Editing using SPH model for transport-diffusion
*-----
DISCR1 := JPMT: ASSMBH ::
    TITLE 'TCWU03: MULTICELL HEXAGONAL ASSEMBLY WITH POISON'
    MAXR 400 MAXZ 15000 OLD ;
LIBRARY := SHI: LIBRARY DISCR1 :: ;
DISCR2 := SYBILT: ASSMBH ::
    TITLE 'TCWU03: MULTICELL HEXAGONAL ASSEMBLY WITH POISON'
    MAXR 400 MAXZ 15000 ;
CP := ASM: LIBRARY DISCR2 :: ;
CALC := FLU: CP LIBRARY DISCR2 ::
    TYPE B B1 ;
OUT := EDI: CALC LIBRARY DISCR2 ASSMBH ::
    EDIT 3 UPS SAVE COND 4.0 SPH
    ::: BIVACT: PRIM 1 2 1 ;
;
COMPO := CPO: OUT ::
    STEP 'REF-CASE 1' EXTRACT ALL NAME COMPO ;
res := COMPO ;
END: ;
QUIT "LIST" .

```

## 4.4.4 TCWU04 – A Cylindrical cell with burnup

This test case represents a burnup calculation for the mosteller annular geometry (see Figure 20).

Input data for test case: **TCWU04.x2m**

```

*-----
*  TEST CASE TCWU04
*  iaea WLUP Library
*  ANNULAR MOSTELLER BENCHMARK WITH BURNUP
*
*  REF: R. Mosteller et al. Nucl. Sci. Eng. 107, 265 (1991)
*
*-----
*  Define variables
*-----
INTEGER
  istep := 1 ;
REAL
  evobeg evoend ;
REAL
  step2 step3  step4  step5 :=
  1.0  27.1739 67.9348 135.8696 ;
*-----
*  Define STRUCTURES and MODULES used
*-----
LINKED_LIST
  LIBRARY MOSTELAS MOSTELA TRACKS TRACK SYS FLUX BURNUP
  EDITION COMPO ;
SEQ_ASCII
  res ;
MODULE
  GEO: SYBILT: LIB: SHI: ASM: FLU: EVO: EDI: CPO:
  DELETE: END: ;
*-----
*  Depletion data from file iaea format WIMSD4
*  Microscopic cross sections from file iaea format WIMSD4
*-----
LIBRARY := LIB: ::
  NMIX 3 CTRA WIMS
  DEPL LIB: WIMSD4 FIL: iaea
  MIXS LIB: WIMSD4 FIL: iaea
  MIX 1 600.0
    U235      = '2235'    1.66078E-4 1
    U238      = '8238'    2.28994E-2 1
    U236      = '236'     0.0         1
    Pu239     = '6239'    0.0         1
  MIX 2 600.0
    Zr91      = '91'      3.83243E-2
  MIX 3 600.0
    H1H2O     = '3001'    4.42326E-2  O16H2O  = '6016'    2.21163E-2
    BNat      = '1011'    1.02133E-5

```

```

;
*-----
*   Geometry MOSTELAS : 3 regions annular cell for self-shielding
*           MOSTELA   : 4 regions annular cell for transport
*-----
MOSTELAS := GEO: :: TUBE 3
R+ REFL RADIUS 0.0 0.39306 0.45802 0.71206
MIX 1 2 3 ;
MOSTELA := GEO: MOSTELAS ::
SPLITR 2 1 1 ;
*-----
*   Self-Shielding calculation SYBIL
*   Transport calculation          SYBIL
*   Flux calculation for keff with imposed buckling
*   using B1 homogeneous leakage model
*-----
TRACKS := SYBILT: MOSTELAS ::
TITLE 'TCWU04: MOSTELLER BENCHMARK WITH BURNUP'
EDIT 1 MAXR 3 ;
LIBRARY := SHI: LIBRARY TRACKS :: ;
TRACK := SYBILT: MOSTELA ::
TITLE 'TCWU04: MOSTELLER BENCHMARK WITH BURNUP'
EDIT 1 MAXR 4 ;
SYS := ASM: LIBRARY TRACK :: ;
FLUX := FLU: SYS LIBRARY TRACK ::
TYPE K B1 PNL BUCK 0.2948E-2 ;
EDITION := EDI: FLUX LIBRARY TRACK ::
EDIT 3 MERG COMP COND 4.0 SAVE ;
*-----
*   Burnup loop: for first step BURNUP is created
*   while for other steps it is modified
*   two burnup per step:
*   1) get a first approximation of final composition followed
*       by a transport calculation
*   2) use approximation for final flux distribution to get a
*       better approximation for final composition
*-----
EVALUATE evoend := 0.0 ;
WHILE evoend step2 < DO
  EVALUATE evobeg := evoend ;
  EVALUATE evoend := step2 ;
  IF istep 1 = THEN
    BURNUP LIBRARY := EVO: LIBRARY FLUX TRACK ::
    SAVE <<evobeg>> DAY
    DEPL <<evobeg>> <<evoend>> DAY POWER 36.8
    SET <<evoend>> DAY ;
  ELSE
    BURNUP LIBRARY := EVO: BURNUP LIBRARY FLUX TRACK ::
    SAVE <<evobeg>> DAY
    DEPL <<evobeg>> <<evoend>> DAY POWER 36.8
    SET <<evoend>> DAY ;
ENDIF ;

```

```

LIBRARY := SHI: LIBRARY TRACKS :: ;
SYS := DELETE: SYS ;
SYS := ASM: LIBRARY TRACK :: ;
FLUX := FLU: FLUX SYS LIBRARY TRACK ::
    TYPE K B1 PNL BUCK 0.2948E-2 ;
BURNUP LIBRARY := EVO: BURNUP LIBRARY FLUX TRACK ::
    SAVE <<evoend>> DAY
    DEPL <<evobeg>> <<evoend>> DAY POWR 36.8
    SET <<evoend>> DAY ;
LIBRARY := SHI: LIBRARY TRACKS :: ;
SYS := DELETE: SYS ;
SYS := ASM: LIBRARY TRACK :: ;
FLUX := FLU: FLUX SYS LIBRARY TRACK ::
    TYPE K B1 PNL BUCK 0.2948E-2 ;
EDITION := EDI: EDITION FLUX LIBRARY TRACK ::
    EDIT 3 SAVE ;
EVALUATE step2 step3 step4 step5 :=
    step3 step4 step5 step2 ;
EVALUATE istep := istep 1 + ;
ENDWHILE ;
COMPO := CPO: EDITION BURNUP ::
    BURNUP REF-CASE NAME COMPO ;
res := COMPO ;
END: ;
QUIT "LIST" .

```

#### 4.4.5 TCWU05 – A CANDU-6 type annular cell with burnup

This test case represents the typical CANDU type cell with an annular moderator region defined in Figure 23. Both its cross section and depletion data are taken from the same WIMS-D4 file. Depletion calculations are performed for 50 days at a fixed power.<sup>[2]</sup> This test case uses the embedded DRAGON procedure stored in the TCWU05Lib.c2m file.

Input data for test case: **TCWU05.x2m**

```

*-----
*  TEST CASE TCWU05
*  CANDU-6 ANNULAR CELL
*  iaea WLUP Library
*  POWER (KW)           = 615.00000
*  BURN POWER (KW/KG)   = 31.97130
*  URANIUM MASS         = 19.23600
*  UO2 REAL DENSITY     = 10.59300
*  UO2 EFF DENSITY      = 10.43750
*  UO2 TEMPERATURE      = 941.28998
*  ENRICHMENT           = 0.71140
*  COOLANT D2 AT %      = 99.222
*  MODERATOR D2 AT %    = 99.911
*  NUMBER OF DAYS       = 50
*
*-----

```

```

*   Define variables and initialize
*   Burnup paremeters
*   a) Power
*       = 31.9713 kw/kg for    0.0 to 300.0 days
*   b) Burnup time interval Delt
*       = 1 day for    0 to    1 day
*       = 4 days for    1 to    5 days
*       = 5 days for    5 to   10 days
*       = 10 days for   10 to   50 days
*       = 20 days for   50 to  150 days
*       = 50 days for  150 to  300 days
*   c) Days with burnup interval changes
*       = 1.0, 5.0, 10.0, 50.0, 150.0 and 300.0 days
*   d) Burnup control time variables Timei, Timef
*       Timei = initial time
*       Timef = final time
*-----
REAL
    Power    Delt Timec Timei Timef :=
    31.9713  1.0  1.0   0.0   0.0 ;
*-----
*   Define STRUCTURES and MODULES used
*-----
LINKED_LIST
    LIBRARY CANDU6S CANDU6F VOLMATS VOLMATF PIJ FLUX BURNUP EDITION
    COMPO1 COMPO2 ;
SEQ_BINARY
    INTLINS INTLINF ;
SEQ_ASCII
    fuel mode ;
MODULE
    GEO: EXCEL: SHI: ASM: FLU: EVO: EDI: CPO:
    DELETE: END: ;
*-----
*   Depletion data from file iaea format WIMSD4
*   Microscopic cross sections from file iaea format WIMSD4
*-----
PROCEDURE TCWU05Lib ;
INTEGER    iedit := 1 ;
LIBRARY := TCWU05Lib :: <<iedit>> ;
*-----
*   Geometry CANDU6S : 13 regions annular cluster for self-shielding
*   CANDU6F : 31 regions annular cluster for transport
*-----
CANDU6S := GEO: :: TUBE 5
R+ REFL RADIUS  0.00000 5.16890 5.60320  6.44780 6.58750 16.12171
MIX  1 2 3 4 5
CLUSTER ROD1 ROD2 ROD3 ROD4
::: ROD1 := GEO: TUBE 2 MIX 6 10 NPIN  1 RPIN 0.0000 APIN 0.0000
    RADIUS 0.00000 0.6122 0.6540 ;
::: ROD2 := GEO: ROD1    MIX 7 10 NPIN  6 RPIN 1.4885 APIN 0.0000 ;
::: ROD3 := GEO: ROD1    MIX 8 10 NPIN 12 RPIN 2.8755 APIN 0.261799 ;

```

```

      ::: ROD4 := GEO: ROD1    MIX 9 10 NPIN 18 RPIN 4.3305 APIN 0.0 ;
    ;
CANDU6F := GEO: CANDU6S :: SPLITR 6 1 1 1 10
      ::: ROD1 := GEO: ROD1 SPLITR 2 1 ;
      ::: ROD2 := GEO: ROD2 SPLITR 2 1 ;
      ::: ROD3 := GEO: ROD3 SPLITR 2 1 ;
      ::: ROD4 := GEO: ROD4 SPLITR 2 1 ;
    ;
*-----
*   Self-Shielding calculation EXCEL
*   Transport calculation      EXCEL
*   Flux calculation for keff
*-----
VOLMATS INTLINS := EXCELT: CANDU6S ::
  TITLE 'TCWU05: CANDU-6 ANNULAR POWER= 31.971 FUEL TEMP= 941.29'
  EDIT 0 MAXR 13 TRAK TISO 5 10.0 SYMM 12 ;
LIBRARY := SHI: LIBRARY VOLMATS INTLINS ::
  EDIT 0 ;
VOLMATF INTLINF := EXCELT: CANDU6F ::
  TITLE 'TCWU05: CANDU-6 ANNULAR POWER= 31.971 FUEL TEMP= 941.29'
  EDIT 0 MAXR 31 TRAK TISO 5 10.0 SYMM 12 ;
PIJ := ASM: LIBRARY VOLMATF INTLINF :: ;
FLUX := FLU: PIJ LIBRARY VOLMATF ::
  TYPE K ;
EDITION := EDI: FLUX LIBRARY VOLMATF ::
  COND 4.0 MERGE MIX 0 0 0 0 1 0 0 0 0 0 SAVE ON 'EDITMOD' ;
EDITION := EDI: EDITION FLUX LIBRARY VOLMATF ::
  COND 4.0 MERGE COMP MICR 1 Xe135 SAVE ;
*-----
*   Burnup loop: for first step BURNUP is created
*   while for other steps it is modified
*-----
WHILE Timei Timec < DO
  EVALUATE Timef := Timei Delt + ;
  IF Timei 0.0 = THEN
    BURNUP LIBRARY := EVO: LIBRARY FLUX VOLMATF ::
      DEPL <<Timei>> <<Timef>> DAY POWR <<Power>> ;
  ELSE
    BURNUP LIBRARY := EVO: BURNUP LIBRARY FLUX VOLMATF ::
      DEPL <<Timei>> <<Timef>> DAY POWR <<Power>> ;
  ENDIF ;
LIBRARY := SHI: LIBRARY VOLMATS INTLINS ::
  EDIT 0 ;
PIJ := DELETE: PIJ ;
PIJ := ASM: LIBRARY VOLMATF INTLINF :: ;
FLUX := FLU: FLUX PIJ LIBRARY VOLMATF ::
  TYPE K ;
EDITION := EDI: EDITION FLUX LIBRARY VOLMATF ::
  SAVE ;
*-----
*   change delta t for burnup and final time if required
*-----

```

```

      IF Timef Timec = THEN
        IF Timec 150.0 = THEN
          EVALUATE Delt Timec := 50.0 300.0 ;
        ENDIF ;
        IF Timec 50.0 = THEN
          EVALUATE Delt Timec := 20.0 150.0 ;
        ENDIF ;
        IF Timec 10.0 = THEN
          EVALUATE Delt Timec := 10.0 50.0 ;
        ENDIF ;
        IF Timec 5.0 = THEN
          EVALUATE Delt Timec := 5.0 10.0 ;
        ENDIF ;
        IF Timec 1.0 = THEN
          EVALUATE Delt Timec := 4.0 5.0 ;
        ENDIF ;
      ENDIF ;
      EVALUATE Timei := Timef ;
    ENDWHILE ;
    *-----
    *   Save calculation results in CPO format file
    *-----
    COMPO1 := CPO: BURNUP EDITION ::
      BURNUP REF-CASE EXTRACT Xe135 Xe135  NAME MIXTRXE ;
    fuel := COMPO1 ;
    COMPO2 := CPO: EDITION ::
      STEP 'EDITMOD' NAME MIXTMOD ;
    mode := COMPO2 ;
    INTLINF INTLINS := DELETE: INTLINF INTLINS ;
    END: ;
    QUIT "LIST" .

```

Input data for test case: **TCWU05Lib.c2m**

```

*-----
*   Procedure TCWU05Lib
*   Create Library for test CASE TCWU05
*   Calling :
*       LIBRARY := TCWU05Lib :: iedit ;
*   with :
*       LIBRARY = Linked list containing the result of LIB: for
*               TCWU05
*       iprint  = print level for LIB: module
*-----
*   Define PARAMETERS,STRUCTURES and MODULES used
*-----
PARAMETER  LIBRARY  ::  ::: LINKED_LIST LIBRARY ; ;
MODULE     LIB: DELETE: END: ;
*-----
*   Define and read LIB: EDIT option
INTEGER iedit  ;
:: >>iedit<<  ;

```

```

*-----
* Depletion data from file iaea format WIMSD4
* Microscopic cross sections from file iaea format WIMSD4
*-----
LIBRARY := LIB: ::
  EDIT <<iedit>>
  NMIX 17 CTRA WIMS
  DEPL LIB: WIMSD4 FIL: iaea
  MIXS LIB: WIMSD4 FIL: iaea
  MIX 1 560.66 0.81212 O16 = '6016' 7.99449E-1
    D2D2O = '3002' 1.99768E-1 H1H2O = '3001' 7.83774E-4
  MIX 2 560.66 6.57 Nb93 = '93' 2.50000
    BNat = '1011' 2.10000E-4
    Zr91 = '91' 9.75000E+1
  MIX 3 345.66 0.0014 He4 = '4' 1.00000E+2
  MIX 4 345.66 6.44 Fe56 = '2056' 1.60000E-1
    Ni58 = '58' 6.00000E-2 Cr52 = '52' 1.10000E-1
    BNat = '1011' 3.10000E-4
    Zr91 = '91' 9.97100E+1
  MIX 5 345.66 1.082885 O16 = '6016' 7.98895E-1
    D2D2O = '3002' 2.01016E-1 H1H2O = '3001' 8.96000E-5
  MIX 6 941.29 10.4375010 O16 = '6016' 1.18473E+1
    Xe135 = '4135' 0.0
    U235 = '2235' 6.27118E-1 1
    U238 = '8238' 8.75256E+1 1
    U236 = '236' 0.0 1
    Pu239 = '6239' 0.0 1
  MIX 7 COMB 6 1.0
  MIX 8 COMB 6 1.0
  MIX 9 COMB 6 1.0
  MIX 10 560.66 6.44 Fe56 = '2056' 1.60000E-1
    Ni58 = '58' 6.00000E-2 Cr52 = '52' 1.10000E-1
    BNat = '1011' 3.10000E-4
    Zr91 = '91' 9.97100E+1
  MIX 11 COMB 10 1.0
  MIX 12 COMB 10 1.0
  MIX 13 COMB 10 1.0
  MIX 14 COMB 1 1.0
  MIX 15 COMB 1 1.0
  MIX 16 COMB 1 1.0
  MIX 17 COMB 1 1.0
;
END: ;
QUIT "LIST" .

```

#### 4.4.6 TCWU06 – A CANDU-6 type supercell with control rods

This test case treats both the CANDU cell with a cartesian moderator region (similar to the cell described in defined Figure 23) and the supercell containing a stainless steel rod which can be either in the inserted or extracted position (see Figure 19). Two groups incremental cross sections corresponding to the rod in the inserted and

extracted position with respect to the original supercell containing only 3-D fuel elements are computed.<sup>[2]</sup> This test case also uses the embedded DRAGON procedure stored in the TCWU05Lib.c2m file.

Input data for test case: **TCWU06.x2m**

```
*-----
*   TEST CASE TCWU06
*   CANDU-6 CARTESIAN CELL
*   iaea WLUP Library
*   STAINLESS STELL RODS IN 3D SUPERCELL
*
*-----
*   Define STRUCTURES and MODULES used
*-----
LINKED_LIST
  LIBRARY LIBRARY2 CANDU6F CANDU6S TRACK SYS FLUX EDITION BCO BCI ;
SEQ_BINARY
  INTLIN ;
MODULE
  GEO: JPMT: EXCELT: LIB: SHI: ASM: FLU: EDI:
  DELETE: UTL: END: ;
*-----
*   Depletion data from file iaea format WIMSD4
*   Microscopic cross sections from file iaea format WIMSD4
*-----
PROCEDURE TCWU05Lib ;
INTEGER   iedit := 1 ;
LIBRARY := TCWU05Lib :: <<iedit>> ;
*-----
*   CELL CALCULATION
*   Geometry CANDU6S : 14 regions Cartesian cluster for self-shielding
*                   CANDU6F : 32 regions Cartesian cluster for transport
*                   BCO      : 48 regions 3D Cartesian geometry
*                   BCI      : 48 regions 3D Cartesian geometry
*-----
CANDU6S := GEO: :: CARCEL 5
  X+ REFL X- REFL MESHX -14.2875 14.2875
  Y+ REFL Y- REFL MESHY -14.2875 14.2875
  RADIUS 0.00000 5.16890 5.60320 6.44780 6.58750 14.00
  MIX 1 2 3 4 5 5
  CLUSTER ROD1 ROD2 ROD3 ROD4
  ::: ROD1 := GEO: TUBE 2 MIX 6 10 NPIN 1 RPIN 0.0000 APIN 0.0000
    RADIUS 0.00000 0.6122 0.6540 ;
  ::: ROD2 := GEO: ROD1 MIX 7 10 NPIN 6 RPIN 1.4885 APIN 0.0000 ;
  ::: ROD3 := GEO: ROD1 MIX 8 10 NPIN 12 RPIN 2.8755 APIN 0.261799 ;
  ::: ROD4 := GEO: ROD1 MIX 9 10 NPIN 18 RPIN 4.3305 APIN 0.0 ;
  ;
CANDU6F := GEO: CANDU6S :: SPLITR 6 1 1 1 10
  ::: ROD1 := GEO: ROD1 SPLITR 2 1 ;
  ::: ROD2 := GEO: ROD2 SPLITR 2 1 ;
  ::: ROD3 := GEO: ROD3 SPLITR 2 1 ;
  ::: ROD4 := GEO: ROD4 SPLITR 2 1 ;
```

```

;
*-----
* Self-Shielding calculation EXCEL
* Transport calculation EXCEL
* Flux calculation for keff
*-----
TRACK INTLIN := EXCEL: CANDU6S ::
  TITLE 'TCWU06: CANDU-6 CARTESIAN FUEL TEMP= 941.29'
  EDIT 0 MAXR 14 TRAK TISO 29 20.0 SYMM 4 ;
LIBRARY := SHI: LIBRARY TRACK INTLIN ::
  EDIT 0 ;
TRACK INTLIN := DELETE: TRACK INTLIN ;
TRACK INTLIN := EXCEL: CANDU6F ::
  TITLE 'TCWU06: CANDU-6 CARTESIAN FUEL TEMP= 941.29'
  EDIT 0 MAXR 32 TRAK TISO 29 20.0 SYMM 4 ;
SYS := ASM: LIBRARY TRACK INTLIN ::
  EDIT 0 ;
FLUX := FLU: SYS LIBRARY TRACK ::
  TYPE K ;
*-----
* Microscopic cross sections from WIMSLIB for stainless steel
* MIX 1,2,3 from EDI: : fuel, structure material and moderator
* MIX 4 stainless steel rods
*-----
EDITION := EDI: FLUX LIBRARY TRACK ::
  EDIT 0 MERGE MIX 1 2 2 2 3 1 1 1 1 1 SAVE ON SSRODS ;
EDITION := UTL: EDITION :: STEP UP SSRODS ;
LIBRARY2 := LIB: EDITION ::
  EDIT 0 NMIX 4 CTRA WIMS
  MIXS LIB: WIMSD4 FIL: iaea
  MIX 4 345.66 Fe56 = '2056' 6.19027E-2
    Cr52 = '52' 1.56659E-3 Ni58 = '58' 6.83337E-3
    Si29 = '29' 7.79072E-4 C12 = '2012' 1.46552E-4
    Mn55 = '55' 1.25431E-3
;
EDITION TRACK INTLIN SYS FLUX := DELETE:
  EDITION TRACK INTLIN SYS FLUX ;
*-----
* SUPERCELL CALCULATION
* Geometry BCO : 27 regions 3D Cartesian geometry with rods out
* BCI : 27 regions 3D Cartesian geometry with rods in
*-----
BCO := GEO: :: CAR3D 3 2 2
X- REFL X+ SYME Y- REFL Y+ SYME Z- REFL Z+ SYME
CELL M MX MX MX FXY MXY M MX BX MX FXY BXY
TURN A A A F A A A A A F A A
::: M := GEO: CAR3D 1 1 1 MIX 3
  MESHX 0.0 7.14375
  MESHY 0.0 7.14375
  MESHZ -8.25500 8.25500 SPLITZ 2 ;
::: MX := GEO: M MESHX -7.14375 +7.14375 SPLITX 2 ;
::: MXY := GEO: MX MESHY -7.14375 +7.14375 SPLITY 2 ;

```

```

::: BX := GEO: CARCELY 2 1 MIX 3 3 3
  MESHX -7.14375 7.14375 SPLITX 2
  MESHY 0.0 7.14375
  MESHZ -8.25500 8.25500 SPLITZ 2
  RADIUS 0.0 3.5100 3.8100 ;
::: BXY := GEO: BX MESHY -7.14375 +7.14375 SPLITY 2 ;
::: FXY := GEO: CARCELZ 2 1 MIX 1 2 3
  MESHX -7.14375 7.14375 SPLITX 2
  MESHY -7.14375 7.14375 SPLITY 2
  MESHZ -8.25500 8.25500 SPLITZ 2
  RADIUS 0.0 5.16890 6.58750 ;
;
BCI := GEO: BCO ::
  ::: BX := GEO: BX MIX 3 4 3 ;
  ::: BXY := GEO: BXY MIX 3 4 3 ;
;
*-----
* Transport calculation          EXCEL
* Flux calculation for keff
* Homogenized properties for rod out
*-----
TRACK INTLIN := EXCELT: BCO ::
  EDIT 0 MAXR 40 TRAK TISO 2 1.0 ;
SYS := ASM: LIBRARY2 TRACK INTLIN ::
  EDIT 0 ;
FLUX := FLU: SYS LIBRARY2 TRACK ::
  TYPE K ;
EDITION := EDI: FLUX LIBRARY2 TRACK ::
  EDIT 2 MERG COMP COND 4.0 SAVE ON 'NOBC' ;
SYS TRACK INTLIN := DELETE: SYS TRACK INTLIN ;
*-----
* Transport calculation          EXCEL
* Flux calculation for keff
* Homogenized properties for rod in
*-----
TRACK INTLIN := EXCELT: BCI ::
  EDIT 0 MAXR 40 TRAK TISO 2 1.0 ;
SYS := ASM: LIBRARY2 TRACK INTLIN ::
  EDIT 0 ;
FLUX := FLU: FLUX SYS LIBRARY2 TRACK ::
  TYPE K ;
EDITION := EDI: EDITION FLUX LIBRARY2 TRACK ::
  EDIT 2 MERG COMP COND 4.0 STAT DELS REFE 'NOBC' ;
TRACK INTLIN SYS := DELETE: TRACK INTLIN SYS ;
END: ;
QUIT "LIST" .

```

4.4.7 **TCWU07** – A CANDU-6 type calculation using various leakage options

This test case treats the CANDU cell with a cartesian moderator region (similar to the cell described in defined Figure 23) using various leakage options. This test case also uses the embedded DRAGON procedure stored in the TCWU05Lib.c2m file.

Input data for test case: **TCWU07.x2m**

```

*-----
*   TEST CASE TCWU07
*   CANDU-6 CARTESIAN CELL
*   iaea WLUP Library
*   TEST VARIOUS LEAKAGE OPTIONS
*
*-----
*   Define STRUCTURES and MODULES used
*-----
LINKED_LIST
  LIBRARY CANDU6S CANDU6T CANDU6SV CANDU6TV TRACK
  SYS FLUX EDITION ;
MODULE
  GEO: EXCELT: LIB: SHI: ASM: FLU: EDI:
  DELETE: END: ;
SEQ_BINARY
  INTLIN ;
*-----
*   Depletion data from file iaea format WIMSD4
*   Microscopic cross sections from file iaea format WIMSD4
*-----
PROCEDURE TCWU05Lib ;
INTEGER   iedit := 1 ;
LIBRARY := TCWU05Lib :: <<iedit>> ;
*-----
*   Geometry CANDU6S : GEOMETRY FOR SELF-SHIELDING   (NO VOID)
*               CANDU6F : GEOMETRY FOR TRANSPORT      (NO VOID)
*               CANDU6FV: GEOMETRY FOR TRANSPORT      (COOLANT VOID)
*               CANDU6FV: GEOMETRY FOR TRANSPORT      (COOLANT VOID)
*-----
CANDU6S := GEO: :: CARCEL  5
  X+ REFL X- REFL MESHX -14.2875 14.2875
  Y+ REFL Y- REFL MESHY -14.2875 14.2875
  RADIUS  0.00000 5.16890 5.60320 6.44780 6.58750 14.00
  MIX      1      2      3      4      5      5
  CLUSTER ROD1 ROD2 ROD3 ROD4
  ::: ROD1 := GEO: TUBE 2 MIX  6 10 NPIN  1 RPIN 0.0000 APIN 0.0000
    RADIUS 0.00000 0.6122 0.6540 ;
  ::: ROD2 := GEO: ROD1  MIX  7 10 NPIN  6 RPIN 1.4885 APIN 0.0000 ;
  ::: ROD3 := GEO: ROD1  MIX  8 10 NPIN 12 RPIN 2.8755 APIN 0.261799 ;
  ::: ROD4 := GEO: ROD1  MIX  9 10 NPIN 18 RPIN 4.3305 APIN 0.0 ;
;
CANDU6T := GEO: CANDU6S :: SPLITR  6 1 1  1 10
  ::: ROD1 := GEO: ROD1 SPLITR 2 1 ;

```

```

      ::: ROD2 := GEO: ROD2 SPLITR 2 1 ;
      ::: ROD3 := GEO: ROD3 SPLITR 2 1 ;
      ::: ROD4 := GEO: ROD4 SPLITR 2 1 ;
      ;
CANDU6SV := GEO: CANDU6S  :: MIX 0 2 3 4 5 5 ;
CANDU6TV := GEO: CANDU6SV :: SPLITR 6 1 1 1 10
      ::: ROD1 := GEO: ROD1 SPLITR 2 1 ;
      ::: ROD2 := GEO: ROD2 SPLITR 2 1 ;
      ::: ROD3 := GEO: ROD3 SPLITR 2 1 ;
      ::: ROD4 := GEO: ROD4 SPLITR 2 1 ;
      ;
*-----
* CASE WITH NO VOID
* Self-Shielding calculation EXCEL
* Transport calculation EXCEL
* Flux TYPE K AND B WITH VARIOUS LEAKAGE OPTIONS
*-----
TRACK INTLIN := EXCELT: CANDU6S ::
  TITLE 'TCWU07: CANDU-6 CARTESIAN FUEL TEMP= 941.29'
  EDIT 0 MAXR 14 TRAK TISO 7 20.0 SYMM 4 ;
LIBRARY := SHI: LIBRARY TRACK INTLIN ::
  EDIT 0 ;
TRACK INTLIN := DELETE: TRACK INTLIN ;
TRACK INTLIN := EXCELT: CANDU6T ::
  TITLE 'TCWU07: CANDU-6 CARTESIAN FUEL TEMP= 941.29'
  EDIT 0 MAXR 32 ANIS 2 TRAK TISO 7 20.0 SYMM 4 ;
SYS := ASM: LIBRARY TRACK INTLIN ::
  EDIT 0 PIJK ;
FLUX := FLU: SYS LIBRARY TRACK ::
  TYPE K ;
EDITION := EDI: FLUX LIBRARY TRACK ::
  EDIT 3 SAVE COND 4.0 TAKE REGI 1 4 7 10 16 24 ;
FLUX := FLU: FLUX SYS LIBRARY TRACK ::
  TYPE B B1 PNL ;
EDITION := EDI: EDITION FLUX LIBRARY TRACK ::
  EDIT 3 SAVE COND 4.0 TAKE REGI 1 4 7 10 16 24 ;
FLUX := FLU: FLUX SYS LIBRARY TRACK ::
  TYPE B B1 HETE ;
EDITION := EDI: EDITION FLUX LIBRARY TRACK ::
  EDIT 3 SAVE COND 4.0 TAKE REGI 1 4 7 10 16 24 ;
FLUX SYS TRACK INTLIN := DELETE: FLUX SYS TRACK INTLIN ;
*-----
* CASE WITH COOLANT VOIDED
* Self-Shielding calculation EXCEL
* Transport calculation EXCEL
* Flux TYPE K AND B WITH VARIOUS LEAKAGE OPTIONS
*-----
TRACK INTLIN := EXCELT: CANDU6SV ::
  TITLE 'TCWU07: CANDU-6 CARTESIAN FUEL TEMP= 941.29'
  EDIT 0 MAXR 14 TRAK TISO 7 20.0 SYMM 4 ;
LIBRARY := SHI: LIBRARY TRACK INTLIN ::
  EDIT 0 ;

```

```

TRACK INTLIN := DELETE: TRACK INTLIN ;
TRACK INTLIN := EXCELT: CANDU6TV ::
  TITLE 'TCWU07: CANDU-6 CARTESIAN FUEL TEMP= 941.29'
  EDIT 0 MAXR 32 ANIS 2 TRAK TISO 7 20.0 SYMM 4 ;
SYS := ASM: LIBRARY TRACK INTLIN ::
  EDIT 0 PIJK ;
FLUX := FLU: SYS LIBRARY TRACK ::
  TYPE K ;
EDITION := EDI: EDITION FLUX LIBRARY TRACK ::
  EDIT 3 SAVE COND 4.0 TAKE REGI 1 4 7 10 16 24 ;
FLUX := FLU: FLUX SYS LIBRARY TRACK ::
  TYPE B B1 PNL ;
EDITION := EDI: EDITION FLUX LIBRARY TRACK ::
  EDIT 3 SAVE COND 4.0 TAKE REGI 1 4 7 10 16 24 ;
FLUX := FLU: FLUX SYS LIBRARY TRACK ::
  TYPE B B1 HETE ;
EDITION := EDI: EDITION FLUX LIBRARY TRACK ::
  EDIT 3 SAVE COND 4.0 TAKE REGI 1 4 7 10 16 24 ;
FLUX SYS TRACK INTLIN := DELETE: FLUX SYS TRACK INTLIN ;
END: ;
QUIT "LIST" .

```

#### 4.4.8 TCWU08 – Burnup of an homogeneous cell

This case illustrate the burnup of an homogeneous cell that spends the first 1000 days in a reactor before being removed. The depletion of the isotopes in this cell for an additional 1000 days outside of the core is also investigated.

Input data for test case: **TCWU08.x2m**

```

*-----
*  TEST CASE TCWW08
*  HOMOGENEOUS DEPLETION CASE
*  iaea WLUP Library
*
*  REF: None
*
*-----
*  Define variables
*  Burnup paremeters
*  a) Power
*    = 600.0 kw/kg for 0.0 to 1000.0 days
*    = 0.0 kw/kg for 1000.0 to 2000.0 days
*  b) Burnup time interval Delt
*    = 10 days for 0 to 50 days
*    = 50 days for 50 to 500 days
*    = 100 days for 500 to 1000 days
*    = 1000 days for 1000 to 2000 days
*  c) Editing time Timec
*    = 0.0, 50.0, 500.0, 1000.0 and 2000.0 days
*  d) Burnup control time variables Timei, Timef, TotalTime

```

```

*      Timei = initial time
*      Timef = final time
*      TotalTime = Final time reached
*      d) Print variable Iprint
*          = 1 reduced print
*          = 3 full print
*-----
REAL
    Power  Delt  Timec  Timei  Timef  TotalTime :=
    600.0  10.0  50.0  0.0   0.0   2000.0 ;
INTEGER
    Iprint := 1 ;
*-----
*   Define STRUCTURES and MODULES used
*-----
LINKED_LIST
    LIBRARY HOM TRACK PIJ FLUX BURNUP EDITION ;
MODULE
    GEO: SYBILT: LIB: SHI: ASM: FLU: EVO: EDI:
    DELETE: END: ;
*-----
*   Depletion data from file iaea format WIMSD4
*   Microscopic cross sections from file iaea format WIMSD4
*-----
LIBRARY := LIB: ::
    NMIX 1 CTRA WIMS
    DEPL LIB: WIMSD4 FIL: iaea
    MIXS LIB: WIMSD4 FIL: iaea
    MIX 1 300.0                                H1          = '3001'          2.00000E+1
        U235      = '2235'          1.0          1
        U236      = '8238'          0.0          1
    ;
*-----
*   Geometry HOM : Homogeneous geometry
*-----
HOM := GEO: :: HOMOGE
    MIX 1 ;
*-----
*   Self-Shielding calculation SYBIL
*   Transport calculation          SYBIL
*   Flux calculation for keff
*-----
TRACK := SYBILT: HOM ::
    TITLE 'TCWW08: HOMOGENEOUS BENCHMARK WITH BURNUP' ;
LIBRARY := SHI: LIBRARY TRACK :: ;
PIJ := ASM: LIBRARY TRACK :: ;
FLUX := FLU: PIJ LIBRARY TRACK ::
    TYPE K ;
EDITION := EDI: FLUX LIBRARY TRACK ::
    COND 4.0 MERGE COMP SAVE ;
*-----
*   Burnup loop: for first step BURNUP is created

```

```

*   while for other steps it is modified
*-----
WHILE Timei TotalTime < DO
  EVALUATE Timef := Timei Delt + ;
  IF Timef Timec = THEN
    EVALUATE Iprint := 3 ;
  ELSE
    EVALUATE Iprint := 1 ;
  ENDIF ;
  IF Timei 0.0 = THEN
    BURNUP LIBRARY := EVO: LIBRARY FLUX TRACK ::
    EDIT <<Iprint>> DEPL <<Timei>> <<Timef>> DAY
    POWR <<Power>> ;
  ELSE
    BURNUP LIBRARY := EVO: BURNUP LIBRARY FLUX TRACK ::
    EDIT <<Iprint>> DEPL <<Timei>> <<Timef>> DAY
    POWR <<Power>> ;
  ENDIF ;
  LIBRARY := SHI: LIBRARY TRACK :: EDIT 0 ;
  PIJ := DELETE: PIJ ;
  PIJ := ASM: LIBRARY TRACK :: ;
  FLUX := FLU: FLUX PIJ LIBRARY TRACK ::
  TYPE K ;
  IF Iprint 3 = THEN
    EDITION := EDI: EDITION FLUX LIBRARY TRACK ::
    SAVE ;
  ENDIF ;
*-----
*   change delta t for burnup, final time and power if required
*-----
  IF Timef Timec = THEN
    IF Timec 1000.0 = THEN
      EVALUATE Power Delt Timec := 0.0 1000.0 2000.0 ;
    ENDIF ;
    IF Timec 500.0 = THEN
      EVALUATE Delt Timec := 100.0 1000.0 ;
    ENDIF ;
    IF Timec 50.0 = THEN
      EVALUATE Delt Timec := 50.0 500.0 ;
    ENDIF ;
  ENDIF ;
  EVALUATE Timei := Timef ;
ENDWHILE ;
END: ;
QUIT "LIST" .

```

#### 4.4.9 TCWU09 – Testing boundary conditions

This case test different boundary conditions for the Mosteller cell (see Figure 20).

Input data for test case: **TCWU09.x2m**

```

*-----
*   TEST CASE TCWU09
*   MOSTELLER BENCHMARK FOR 1-D ANNULAR CELL
*   iaea WLUP Library
*   REFLECTIVE AND VOID BC
*
*   REF: None
*
*-----
*   Define STRUCTURES and MODULES used
*-----
LINKED_LIST
  MOSTELA MOSTELV VOLMAT LIBRARY PIJ FLUX OUT ;
MODULE
  LIB: GEO: JPMT: SYBILT: SHI: ASM: FLU: EDI:
  DELETE: END: ;
*-----
*   Microscopic cross section from file iaea format WIMSD4
*-----
LIBRARY := LIB: ::
  NMIX 3 CTRA WIMS
  MIXS LIB: WIMSD4 FIL: iaea
  MIX 1 600.0                                O16          = '6016'      4.61309E-2
    U235      = '2235'      1.66078E-4 1
    U238      = '8238'      2.28994E-2 1
  MIX 2 600.0
    Zr91      = '91'        3.83243E-2
  MIX 3 600.0
    H1H2O     = '3001'      4.42326E-2  O16H2O     = '6016'      2.21163E-2
    BNat      = '1011'      1.02133E-5
  ;
*-----
*   Geometry MOSTELA : Annular cell with reflective BC
*   MOSTELV : Annular cell with void BC
*-----
MOSTELA := GEO: :: TUBE 3
  RADIUS 0.0 0.39306 0.45802 0.71206
  SPLITR   2      1      1
  MIX      1      2      3
  R+ REFL ;
MOSTELV := GEO: MOSTELA ::
  R+ VOID ;
*-----
*   Self-Shielding calculation JPM
*   Transport calculation SYBIL
*   Flux calculation for keff
*-----
VOLMAT := JPMT: MOSTELA ::
  TITLE 'TCWU09: JPM TRACK MOSTELLER BENCHMARK REFLECTIVE BC '
  MAXR 4 IP01 QUA1 5 ;

```

```

LIBRARY := SHI: LIBRARY VOLMAT :: ;
VOLMAT := DELETE: VOLMAT ;
VOLMAT := SYBILT: MOSTELA ::
  TITLE 'TCWU09: SYBIL TRACK MOSTELLER BENCHMARK REFLECTIVE BC '
  MAXR 4 QUA1 5 ;
PIJ := ASM: LIBRARY VOLMAT :: ;
FLUX := FLU: PIJ LIBRARY VOLMAT ::
  TYPE K ;
OUT := EDI: FLUX LIBRARY VOLMAT ::
  EDIT 4 MERG MIX 1 2 3 COND 4.0 SAVE ;
PIJ VOLMAT := DELETE: PIJ VOLMAT ;
VOLMAT := SYBILT: MOSTELV ::
  TITLE 'TCWU09: SYBIL TRACK MOSTELLER BENCHMARK VOID BC '
  MAXR 4 QUA1 5 ;
PIJ := ASM: LIBRARY VOLMAT :: ;
FLUX := FLU: FLUX PIJ LIBRARY VOLMAT ::
  TYPE K ;
OUT := EDI: OUT FLUX LIBRARY VOLMAT ::
  EDIT 4 MERG MIX 1 2 3 COND 4.0 SAVE ;
OUT FLUX PIJ LIBRARY VOLMAT := DELETE:
  OUT FLUX PIJ LIBRARY VOLMAT ;
END: ;
QUIT "LIST" .

```

#### 4.4.10 TCWU10 – Fixed source problem in multiplicative media

This case verify the use of a fixed source inside a cell where fission also takes place.

Input data for test case: **TCWU10.x2m**

```

*-----
*  TEST CASE TCWU10
*  MOSTELLER BENCHMARK FOR 1-D ANNULAR CELL
*  iaea WLUP Library
*  FIXED SOURCE PROBLEM IN MULTIPLICATIVE MEDIA
*
*  REF: None
*
*-----
*  Define STRUCTURES and MODULES used
*-----
LINKED_LIST
  MOSTELA VOLMAT LIBRARY PIJ FLUX OUT ;
MODULE
  LIB: MAC: GEO: JPMT: SYBILT: SHI: ASM: FLU: EDI:
  DELETE: END: ;
*-----
*  Microscopic cross section from file iaea format WIMSD4
*  Fixed source of 1.0E5 in group 6
*-----
LIBRARY := LIB: ::

```

```

EDIT 0 NMIX 3  CTRA WIMS
MIXS LIB: WIMSD4 FIL: iaea
MIX 1 600.0                                O16      = '6016'    4.61309E-2
    U235      = '2235'    1.66078E-4 1
    U238      = '8238'    2.28994E-2 1
MIX 2 600.0
    Zr91      = '91'      3.83243E-2
MIX 3 600.0
    H1H2O     = '3001'    4.42326E-2  O16H2O    = '6016'    2.21163E-2
    BNat      = '1011'    1.02133E-5
;
LIBRARY := MAC: LIBRARY ::
EDIT 0
READ INPUT
MIX 3 FIXE
0.0 0.0 0.0 0.0 0.0 1.0E+5 0.0 0.0 0.0 0.0
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
;
*-----
*  Geometry MOSTELA : Annular cell with reflective BC
*-----
MOSTELA := GEO: :: TUBE 3
RADIUS 0.0 0.39306 0.45802 0.71206
SPLITR      2      1      1
MIX          1      2      3
R+ REFL ;
*-----
*  Self-Shielding calculation JPM
*  Transport calculation      SYBIL
*  Flux calculation for keff
*-----
VOLMAT := JPMT: MOSTELA ::
TITLE 'TCWU10: JPM TRACK MOSTELLER BENCHMARK'
MAXR 4 IP01 QUA1 5 ;
LIBRARY := SHI: LIBRARY VOLMAT :: ;
VOLMAT := DELETE: VOLMAT ;
VOLMAT := SYBILT: MOSTELA ::
TITLE 'TCWU10: SYBILT TRACK MOSTELLER BENCHMARK'
MAXR 4 QUA1 5 ;
PIJ := ASM: LIBRARY VOLMAT :: ;
FLUX := FLU: PIJ LIBRARY VOLMAT ::
TYPE K ;
OUT := EDI: FLUX LIBRARY VOLMAT ::
EDIT 4 MERG MIX 1 2 3 COND 4.0 ;
FLUX := DELETE: FLUX ;
FLUX := FLU: PIJ LIBRARY VOLMAT ::
TYPE S EXTE 30 UNKT 1.0E-3 ;

```

```

OUT := EDI: OUT FLUX LIBRARY VOLMAT  ::
  EDIT 4 MERG MIX 1 2 3 COND 4.0 ;
OUT FLUX PIJ LIBRARY VOLMAT := DELETE:
  OUT FLUX PIJ LIBRARY VOLMAT  ;
END: ;
QUIT "LIST" .

```

#### 4.4.11 TCWU11 – Two group burnup of a CANDU-6 type cell

This case is similar to **TCWU05** except that the burnup module uses DRAGON generated two groups time dependent microscopic cross sections. This test case also uses the embedded DRAGON procedure stored in the TCWU05Lib.c2m file.

Input data for test case: **TCWU11.x2m**

```

*-----
*  TEST CASE TCWU11
*  CANDU-6 ANNULAR CELL
*  iaea WLUP Library
*  TWO GROUP BURNUP
*  POWER (KW)          = 615.00000
*  BURN POWER (KW/KG) = 31.97130
*  URANIUM MASS        = 19.23600
*  UO2 REAL DENSITY    = 10.59300
*  UO2 EFF DENSITY     = 10.43750
*  UO2 TEMPERATURE     = 941.28998
*  ENRICHMENT          = 0.71140
*  COOLANT D2 AT %     = 99.222
*  MODERATOR D2 AT %   = 99.911
*  NUMBER OF DAYS      = 50
*
*-----
*  Define variables
*  Burnup paremeters
*  a) Power
*    = 31.9713 kw/kg for 0.0 to 300.0 days
*  b) 69 Groups Burnup time interval Delt
*    = 300 day for 0 to 300 day
*  c) 2 Groups Burnup time interval Delt
*    = 1 day for 0 to 1 day
*    = 4 days for 1 to 5 days
*    = 5 days for 5 to 10 days
*    = 10 days for 10 to 50 days
*    = 20 days for 50 to 150 days
*    = 50 days for 150 to 300 days
*  c) Days with burnup interval changes
*    = 1.0, 5.0, 10.0, 50.0, 150.0 and 300.0 days
*  d) Burnup control time variables Timei, Timef
*    Timei = initial time
*    Timef = final time
*-----

```

```

REAL
  Power    Delt    Timec    Timei Timef :=
  31.9713  1.0     300.0    0.0   0.0 ;
*-----
*   Define STRUCTURES and MODULES used
*-----
LINKED_LIST LIBRARY ;
LINKED_LIST
  CANDU6S CANDU6F VOLMATS VOLMATF PIJ FLUX BURNUP EDITION ;
SEQ_BINARY
  INTLINS INTLINF ;
SEQ_ASCII
  res ;
MODULE
  GEO: EXCELT: LIB: SHI: ASM: FLU: EVO: EDI:
  DELETE: UTL: END: ;
*-----
*   Depletion data from file iaea format WIMSD4
*   Microscopic cross sections from file iaea format WIMSD4
*-----
PROCEDURE TCWU05Lib ;
INTEGER   iedit := 1 ;
LIBRARY := TCWU05Lib :: <<iedit>> ;
*-----
*   Geometry CANDU6S : 13 regions annular cluster for self-shielding
*   CANDU6F : 31 regions annular cluster for transport
*-----
CANDU6S := GEO: :: TUBE 5
  R+ REFL RADIUS  0.00000 5.16890 5.60320  6.44780 6.58750 16.12171
  MIX  1 2 3 4 5
  CLUSTER ROD1 ROD2 ROD3 ROD4
  ::: ROD1 := GEO: TUBE 2 MIX 6 10 NPIN  1 RPIN 0.0000 APIN 0.0000
    RADIUS 0.00000 0.6122 0.6540 ;
  ::: ROD2 := GEO: ROD1  MIX 7 10 NPIN  6 RPIN 1.4885 APIN 0.0000 ;
  ::: ROD3 := GEO: ROD1  MIX 8 10 NPIN 12 RPIN 2.8755 APIN 0.261799 ;
  ::: ROD4 := GEO: ROD1  MIX 9 10 NPIN 18 RPIN 4.3305 APIN 0.0 ;
  ;
CANDU6F := GEO: CANDU6S :: SPLITR  6 1 1 1 10
  ::: ROD1 := GEO: ROD1 SPLITR 2 1 ;
  ::: ROD2 := GEO: ROD2 SPLITR 2 1 ;
  ::: ROD3 := GEO: ROD3 SPLITR 2 1 ;
  ::: ROD4 := GEO: ROD4 SPLITR 2 1 ;
  ;
*-----
*   Self-Shielding calculation EXCEL
*   Transport calculation      EXCEL
*   Flux calculation for keff
*-----
VOLMATS INTLINS := EXCELT: CANDU6S ::
  TITLE 'TCWU11: FEW GROUP BURNUP / SELF-SHIELDING TRACKING'
  EDIT 0 MAXR 13 TRAK TISO 5 10.0 SYMM 12 ;
LIBRARY := SHI: LIBRARY VOLMATS INTLINS ::

```

```

EDIT 0 ;
VOLMATF INTLINF := EXCELT: CANDU6F ::
  TITLE 'TCWU11: FEW GROUP BURNUP / TRANSPORT TRACKING'
  EDIT 0 MAXR 31 TRAK TISO 5 10.0 SYMM 12 ;
PIJ := ASM: LIBRARY VOLMATF INTLINF :: ;
FLUX := FLU: PIJ LIBRARY VOLMATF ::
  TYPE K ;
EDITION := EDI: FLUX LIBRARY VOLMATF CANDU6F ::
  MERG REGI 6 6 10 7 7 10 1 1 8 8 10 1
            1 9 9 10 1 1 2 3 4 5 5 5
            5 5 5 5 5 5 5
  COND 4.0 FLIB ALL SAVE
  SPH MGEO CANDU6F
  ::: EXCELT: EDIT 0 MAXR 31 TRAK TISO 5 10.0 SYMM 12 ;
;
*-----
* 69 group Burnup
*-----
BURNUP LIBRARY := EVO: LIBRARY FLUX VOLMATF ::
  EDIT 3 EXPM 200.0 DEPL <<Timei>> <<Timec>> DAY POWR <<Power>> ;
LIBRARY := SHI: LIBRARY VOLMATS INTLINS ::
  EDIT 0 ;
PIJ := DELETE: PIJ ;
PIJ := ASM: LIBRARY VOLMATF INTLINF :: ;
FLUX := FLU: FLUX PIJ LIBRARY VOLMATF ::
  TYPE K ;
EDITION := EDI: EDITION FLUX LIBRARY VOLMATF CANDU6F ::
  PERT
  SPH MGEO CANDU6F
  ::: EXCELT: EDIT 0 MAXR 31 TRAK TISO 5 10.0 SYMM 12 ;
;
BURNUP FLUX PIJ LIBRARY INTLINS VOLMATS CANDU6S := DELETE:
  BURNUP FLUX PIJ LIBRARY INTLINS VOLMATS CANDU6S ;
EDITION := UTL: EDITION :: STEP UP 'REF-CASE 1' ;
LIBRARY := EDITION ;
EDITION := UTL: EDITION :: STEP DOWN ;
EDITION := DELETE: EDITION ;
PIJ := ASM: LIBRARY VOLMATF INTLINF :: ;
FLUX := FLU: PIJ LIBRARY VOLMATF ::
  TYPE K ;
EDITION := EDI: FLUX LIBRARY VOLMATF ::
  EDIT 1 MERGE COMP FLIB ALL SAVE ;
EVALUATE Timec := 1.0 ;
WHILE Timei Timec < DO
  EVALUATE Timef := Timei Delt + ;
  IF Timei 0.0 = THEN
    BURNUP LIBRARY := EVO: LIBRARY FLUX VOLMATF ::
      EDIT 3 DEPL <<Timei>> <<Timef>> DAY POWR <<Power>> ;
  ELSE
    BURNUP LIBRARY := EVO: BURNUP LIBRARY FLUX VOLMATF ::
      EDIT 3 DEPL <<Timei>> <<Timef>> DAY POWR <<Power>> ;
  ENDIF ;

```

```

    PIJ := DELETE: PIJ ;
    PIJ := ASM: LIBRARY VOLMATF INTLINF :: ;
    FLUX := FLU: FLUX PIJ LIBRARY VOLMATF ::
        TYPE K ;
    EDITION := EDI: EDITION FLUX LIBRARY VOLMATF ::
        SAVE ;
*-----
*  change delta t for burnup and final time if required
*-----
    IF Timef Timec = THEN
        IF Timec 5.0 = THEN
            EVALUATE Delt Timec := 5.0 10.0 ;
        ENDIF ;
        IF Timec 1.0 = THEN
            EVALUATE Delt Timec := 4.0 5.0 ;
        ENDIF ;
    ENDIF ;
    EVALUATE Timei := Timef ;
ENDWHILE ;
res := EDITION ;
EDITION BURNUP FLUX PIJ LIBRARY INTLINF VOLMATF CANDU6F := DELETE:
    EDITION BURNUP FLUX PIJ LIBRARY INTLINF VOLMATF CANDU6F ;
END: ;
QUIT "LIST" .

```

#### 4.4.12 TCWU12 – Mixture composition

This case illustrates the use of the INFO: module of DRAGON (see Section 3.12) as well as the new COMB option in the module LIB: (see Section 3.2).

Input data for test case: **TCWU12.x2m**

```

*-----
*  TEST CASE TCWU12
*  iaea WLUP Library
*  GENERATE A LIBRARY USING INFO AND OTHER OPTIONS
*
*  REF: None
*
*-----
*  Define variables and initialize
*  Coolant properties
*  a) Input
*      TempCool    = Coolant temperature (K)
*      Purity      = D2/(D2+H1) Weight % ratio in Coolant
*  b) Output
*      DensCool    = Coolant Density (g/cm**3)
*      WH1C        = H1 Weight % in Coolant
*      WD2C        = D2 Weight % in Coolant
*      WO16C       = O16 Weight % in Coolant
*  Fuel properties

```

```

*      a) Input
*      TempFuel      = Fuel temperature (K)
*      Enrichment    = U235/(U235+U238) Weight % ratio in Fuel
*      DensFuel      = Fuel Density (g/cm**3)
*      b) Output
*      WU235F        = U235 Weight % in Fuel
*      WU238F        = U238 Weight % in Fuel
*      WO16F         = O16 Weight % in Fuel
*-----
REAL
  TempCool Purity TempFuel Enrichment DensFuel  :=
    560.66   99.95  941.29   0.72         10.437501 ;
REAL
  WH1C   WD2C   WO16C   DensCool
  WU235F WU238F WO16F ;
*-----
*   Define STRUCTURES and MODULES used
*-----
LINKED_LIST
  LIBRARY ;
MODULE
  LIB: INFO:
  END: ;
*-----
*   Get Coolant properties
*-----
ECHO
  "Input - Coolant temperature (K)                " TempCool ;
ECHO
  "Input - D2/(D2+H1) Weight % ratio in Coolant" Purity ;
INFO: ::
  TMP: <<TempCool>> K
  PUR: <<Purity>>   WGT%
  CALC DENS WATER >>DensCool<<
  LIB: WIMSD4 FIL: iaea
  ISO: 3 '3001'   '3002'   '6016'
  CALC WGT% D2O >>WH1C<< >>WD2C<< >>WO16C<<
  ;
ECHO
  "Output - Coolant Density (g/cm**3)" DensCool ;
ECHO
  "Output - H1 Weight % in Coolant    " WH1C ;
ECHO
  "Output - D2 Weight % in Coolant    " WD2C ;
ECHO
  "Output - O16 Weight % in Coolant   " WO16C ;
*-----
*   Get Fuel properties
*-----
ECHO
  "Input - Fuel temperature (K)                " TempFuel ;
ECHO

```

```

      "Input - U235/(U235+U238) Weight % ratio in Fuel" Enrichment ;
ECHO
      "Input - Fuel Density (g/cm**3)                                " DensFuel ;
INFO: ::
      ENR: <<Enrichment>> WGT%
      LIB: WIMSD4 FIL: iaea
      ISO: 3 '2235'      '8238'      '6016'
      CALC WGT% UO2 >>WU235F<< >>WU238F<< >>WO16F<<
      ;
ECHO
      "Output - U235 Weight % in Fuel" WU235F ;
ECHO
      "Output - U238 Weight % in Fuel" WU238F ;
ECHO
      "Output - O16 Weight % in Fuel " WO16F ;
*-----
*   Microscopic cross sections from file iaea format WIMSD4
*-----
LIBRARY := LIB: ::
      NMIX 8 CTRA WIMS
      MIXS LIB: WIMSD4 FIL: iaea
      MIX 1 <<TempCool>> <<DensCool>> O16      = '6016'    <<WO16C>>
          D2D2O      = '3002'    <<WD2C>>      H1H2O      = '3001'    <<WH1C>>
      MIX 2 <<TempFuel>> <<DensFuel>> O16      = '6016'    <<WO16F>>
          U235      = '2235'    <<WU235F>> 1
          U238      = '8238'    <<WU238F>> 1
      MIX 3 COMB 1 0.5 0 0.5
      MIX 4 COMB 1 0.1 2 0.9
      ;
END: ;
QUIT "LIST" .

```

#### 4.4.13 TCWU13 – Solution by the method of cyclic characteristics

This case illustrates the use of the MOCC: module of DRAGON for a solution by the transport equation by the method of cyclic characteristics. This test case also uses the embedded DRAGON procedure stored in the TCWU05Lib.c2m file.

Input data for test case: **TCWU13.x2m**

```

*-----
*   TEST CASE TCWW13
*   CANDU-6 ANNULAR CELL
*   iaea WLUP Library
*   POWER (KW)           = 615.00000
*   BURN POWER (KW/KG)   = 31.97130
*   URANIUM MASS         = 19.23600
*   UO2 REAL DENSITY     = 10.59300
*   UO2 EFF DENSITY      = 10.43750
*   UO2 TEMPERATURE      = 941.28998
*   ENRICHMENT           = 0.71140

```

```

*   COOLANT D2 AT %      =   99.222
*   MODERATOR D2 AT %    =   99.911
*   NUMBER OF DAYS       =   50
*
*-----
*   Define variables and initialize
*   Burnup paremeters
*   a) Power
*     = 31.9713 kw/kg for   0.0 to 300.0 days
*   b) Burnup time interval Delt
*     =   1 day for   0 to   1 day
*     =   4 days for  1 to   5 days
*     =   5 days for  5 to  10 days
*     =  10 days for 10 to  50 days
*     =  20 days for 50 to 150 days
*     =  50 days for 150 to 300 days
*   c) Days with burnup interval changes
*     = 1.0, 5.0, 10.0, 50.0, 150.0 and 300.0 days
*   d) Burnup control time variables Timei, Timef, TotalTime
*     Timei = initial time
*     Timef = final time
*     TotalTime = Final time reached
*-----
*   Define STRUCTURES and MODULES used
*-----
LINKED_LIST
  LIBRARY CANDU6F VOLMATF PIJ FLUX ;
SEQ_BINARY
  INTLINP ;
SEQ_ASCII
  flxxel flxmoc ;
MODULE
  GEO: EXCELT: ASM: FLU: MOCC:
  DELETE: END: ;
*-----
*   Depletion data from file iaea format WIMSD4
*   Microscopic cross sections from file iaea format WIMSD4
*-----
PROCEDURE TCWU05Lib ;
INTEGER   iedit := 1 ;
LIBRARY := TCWU05Lib :: <<iedit>> ;
*-----
*   Geometry CANDU6S : 13 regions annular cluster for self-shielding
*   CANDU6F : 31 regions annular cluster for transport
*-----
CANDU6F := GEO: :: CARCEL 5
  X- REFL X+ REFL Y- REFL Y+ REFL
  MESHX 0.0 28.375
  MESHY 0.0 28.375
  RADIUS 0.00000 5.16890 5.60320 6.44780 6.58750 14.0
  MIX 1 2 3 4 5 5
  SPLITR 6 1 1 1 10

```

```

CLUSTER ROD1 ROD2 ROD3 ROD4
::: ROD1 := GEO: TUBE 2 MIX 6 10 NPIN 1 RPIN 0.0000 APIN 0.0000
    RADIUS 0.00000 0.6122 0.6540 SPLITR 2 1 ;
::: ROD2 := GEO: ROD1 MIX 7 10 NPIN 6 RPIN 1.4885 APIN 0.0000 ;
::: ROD3 := GEO: ROD1 MIX 8 10 NPIN 12 RPIN 2.8755 APIN 0.261799 ;
::: ROD4 := GEO: ROD1 MIX 9 10 NPIN 18 RPIN 4.3305 APIN 0.0 ;
;
VOLMATF INTLINF := EXCELT: CANDU6F ::
    TITLE 'TCWW13: CANDU-6 ANNULAR POWER= 31.971 FUEL TEMP= 941.29'
    EDIT 0 MAXR 32 TRAK TSPC 12 10.0 ;
PIJ := ASM: LIBRARY VOLMATF INTLINF :: ;
FLUX := FLU: PIJ LIBRARY VOLMATF ::
    TYPE K ;
flxxel := FLUX ;
FLUX PIJ := DELETE: FLUX PIJ ;
FLUX := MOCC: LIBRARY VOLMATF INTLINF ::
    CACB TYPE K
    THER 1.0E-5 100 EXTE 1.0E-5 100 ;
flxmoc := FLUX ;
FLUX := DELETE: FLUX ;
INTLINF VOLMATF CANDU6F := DELETE: INTLINF VOLMATF CANDU6F ;
LIBRARY := DELETE: LIBRARY ;
END: ;
QUIT "LIST" .

```

#### 4.4.14 TCWU14 – SPH Homogenisation without tracking

This case illustrates the use of the SPH homogenisation procedure in the EDI: module of DRAGON when a tracking data structure is provided as input. This test case also uses the embedded DRAGON procedure stored in the TCWU05Lib.c2m file.

Input data for test case: **TCWU14.x2m**

```

*-----
*   TEST CASE TCWW14
*   CANDU-6 Cartesian CELL
*   UO2 REAL DENSITY   =   10.59300
*   UO2 EFF DENSITY    =   10.43750
*   UO2 TEMPERATURE    =   941.28998
*   ENRICHMENT          =    0.71140
*   COOLANT D2 AT %     =    99.222
*   MODERATOR D2 AT %   =    99.911
*
*-----
*   Define STRUCTURES and MODULES used
*-----
LINKED_LIST
    LIBRARY CANDU6F VOLMATF CANDU6H VOLMATH PIJ FLUX EDITION ;
SEQ_BINARY
    INTLINF INTLINH ;
MODULE

```

```

GEO: EXCELT: LIB: ASM: FLU: EDI:
DELETE: END: ;
*-----
* Depletion data from file iaea format WIMSD4
* Microscopic cross sections from file iaea format WIMSD4
*-----
PROCEDURE TCWU05Lib ;
INTEGER   iedit := 1 ;
LIBRARY   := TCWU05Lib :: <<iedit>> ;
*-----
* Geometry CANDU6S : 13 regions annular cluster for self-shielding
*                   CANDU6F : 31 regions annular cluster for transport
*-----
CANDU6F := GEO: :: CARCEL 8
X- REFL MESHX -14.2875 14.2875 X+ REFL
Y- REFL MESHY -14.2875 14.2875 Y+ REFL
RADIUS  0.00000 0.7221626 2.160324 3.600681
         5.168878 5.60320 6.44780 6.587482 14.0
SPLITR  1  2  2  2  1  1  1  9
MIX      14 15 16 17
         2  3  4  5  5
CLUSTER ROD1 ROD2 ROD3 ROD4
::: ROD1 := GEO: TUBE 2 MIX  6 10
  NPIN  1 RPIN 0.0000 APIN 0.0000
  RADIUS 0.00000 0.6122 0.6540 SPLITR 2 1 ;
::: ROD2 := GEO: ROD1  MIX  7 11
  NPIN  6 RPIN 1.4885 APIN 0.0000 ;
::: ROD3 := GEO: ROD1  MIX  8 12
  NPIN 12 RPIN 2.8755 APIN 0.261799 ;
::: ROD4 := GEO: ROD1  MIX  9 13
  NPIN 18 RPIN 4.3305 APIN 0.0 ;
;
CANDU6H := GEO: :: CARCEL 8
X- REFL MESHX -14.2875 14.2875 X+ REFL
Y- REFL MESHY -14.2875 14.2875 Y+ REFL
RADIUS  0.00000 0.7221626 2.160324 3.600681
         5.168878 5.60320 6.44780 6.587482 14.0
SPLITR  1  2  2  2  1  1  1  9
MIX      1  2  3  4
         5  6  7  8  8
;
VOLMATF INTLINF := EXCELT: CANDU6F ::
  TITLE 'TCWW14 Flux geometry'
  EDIT 0 MAXR 100 TRAK TISO 12 20.0 ;
VOLMATH INTLINH := EXCELT: CANDU6H ::
  TITLE 'TCWW14 Homogenisation geometry'
  EDIT 0 MAXR 100 TRAK TISO 12 20.0 ;
PIJ := ASM: LIBRARY VOLMATF INTLINF :: ;
FLUX := FLU: PIJ LIBRARY VOLMATF ::
  TYPE K ;
EDITION := EDI: FLUX LIBRARY VOLMATF VOLMATH INTLINH ::
  MERGE MIX

```

```
0 5 6 7 8
1 2 3 4 1
2 3 4 1 2
3 4
SPH MTRK SAVE ;
PIJ FLUX EDITION := DELETE: PIJ FLUX EDITION ;
INTLINF VOLMATF CANDU6F := DELETE: INTLINF VOLMATF CANDU6F ;
INTLINH VOLMATH CANDU6H := DELETE: INTLINH VOLMATH CANDU6H ;
LIBRARY := DELETE: LIBRARY ;
END: ;
QUIT "LIST" .
```



## REFERENCES

- [1] G. Marleau, A. Hébert, and R. Roy, “New Computational Methods Used in the Lattice Code DRAGON,” *Topical Meeting on Advances in Reactor Physics*, p. 1.177, Charleston, South Carolina (1992).
- [2] G. Marleau, R. Roy, and A. Hébert, *DRAGON: A Collision Probability Transport Code for Cell and Supercell Calculations*, Technical Report IGE-157, École Polytechnique de Montréal (1994).
- [3] A. Hébert, G. Marleau, and R. Roy, “Application of the Lattice Code DRAGON to CANDU Analysis,” *Trans. Am. Nucl. Soc.*, **72**, 335 (1995).
- [4] A. Hébert, G. Marleau, and R. Roy, *A Description of the Data Structures for DRAGON 3.06*, Technical Report IGE-232 Rev. 5, École Polytechnique de Montréal (2008).
- [5] G. Marleau, *The EXCELL Geometries Numbering Scheme in DRAGON*, Technical Report IGE-233, École Polytechnique de Montréal (1997).
- [6] G. Marleau, *DRAGON Theory Manual Part 1: Collision Probability Calculations*, Technical Report IGE-236 Rev. 1, École Polytechnique de Montréal (2001).
- [7] R. Roy, and A. Hébert, *The GAN Generalized Driver*, Technical Report IGE-158, École Polytechnique de Montréal (2000).
- [8] R. Roy, *The CLE-2000 Tool-Box*, Technical Report IGE-163, École Polytechnique de Montréal (1999).
- [9] F. E. Drigger, *A Method for Calculating Neutron Absorption and Flux Spectra at Epithermal Energies*, Technical Report AECL-1996, Atomic Energy of Canada Limited (1964).
- [10] G. Marleau, R. Roy, and A. Hébert, “An Integral Transport Method for Treating CANDU and GCR Clusters,” *Nucl. Sci. Eng.*, **18**, 197–205 (1986).
- [11] G. Marleau, R. Roy, and A. Hébert, “Analytic Reductions for Transmission and Leakage Probabilities in Finite Tubes and Hexahedra,” *Nucl. Sci. Eng.*, **104**, 209–216 (1990).
- [12] G. Marleau, M. L. Vergain, A. Hébert, and R. Roy, “Computation of the DP1 Collision Probabilities for Spherical and Cylindrical Geometries,” *Ann. Nucl. Energy*, **17**, 119–134 (1990).
- [13] M. Ouisloumen, G. Marleau, A. Hébert, and R. Roy, “Computation of Collision Probabilities for Mixed Hexagonal-Cylindrical Geometries Using the DP1 Approximation to the  $J_{\pm}$  Technique,” *International Topical Meeting on Advances in Mathematica, Computation and Reactor Physics*, pp. 2.2.1.1–2.2.1.12, Pittsburgh, PA (1991).
- [14] G. Marleau, and A. Hébert, “Analysis of Cluster Geometries Using the DP1 Approximation of the  $J_{\pm}$  Technique,” *Nucl. Sci. Eng.*, **111**, 257–270 (1992).
- [15] A. Hoffman, *APOLLO: Code Multigroupe de résolution de l’équation du transport pour les neutrons thermiques et rapides*, Technical Report CEA-N-1610, Commissariat à l’énergie Atomique (1973).
- [16] A. Hébert, *Développement de la méthode SPH: Homogénéisation de cellules dans un réseau non uniforme et calcul des paramètres de réflecteur*, Technical Report CEA-N-2209, Commissariat à l’énergie Atomique (1981).
- [17] R. Roy, A. Hébert, and G. Marleau, “A Transport Method for Treating Three-Dimensional Lattices of Heterogeneous Cells,” *Nucl. Sci. Eng.*, **101**, 217–225 (1989).
- [18] R. Roy, G. Marleau, J. Tajmouati, and D. Rozon, “Modeling of CANDU Reactivity Control Devices with the Lattice Code DRAGON,” *Ann. Nucl. Energy*, **21**, 115–132 (1994).

- [19] R. Roy, "Anisotropic Scattering for Integral Transport Codes. Part 1. Slab Assemblies," *Ann. Nucl. Energy*, **17**, 379–388 (1990).
- [20] R. Roy, "Anisotropic Scattering for Integral Transport Codes. Part 2. Cyclic Tracking and its Application to XY Lattices," *Ann. Nucl. Energy*, **18**, 511–524 (1991).
- [21] R. Roy, G. Marleau, and A. Hébert, "A Cyclic Tracking Procedure for Collision Probability Calculation in 2-D Lattices," *International Topical Meeting Advances in Mathematics, Computations and Reactor Physics*, pp. 2.2.4.1–2.2.4.14, Pittsburgh, PA (1991).
- [22] G. Marleau, and A. Hébert, "Solving the Multigroup Transport Equation Using the Power Iteration Method," *1985 Simulation Symposium on Reactor Dynamics and Plant Control*, Kingston, ON (1985).
- [23] G. Marleau, and A. Hébert, "Introduction of an Improved Critical Buckling Search in WIMS," *1986 Simulation Symposium on Reactor Dynamics and Plant Control*, Hamilton, ON (1986).
- [24] A. Hébert, *DRAGON: Description of the DRAGLIB Format*, Technical Report IGE-117, École Polytechnique de Montréal (1991).
- [25] R. E. MacFarlane, *TRANSX-CTR: A Code for Interfacing MATXS Cross-Section Libraries to Nuclear Transport Codes for Fusion System Analysis*, Technical Report LA-9863-MS, Los Alamos National Laboratory (1984).
- [26] RSIC Data Library Collection, DLC-117, *MATXS7A - 69 Neutron Group Cross Section Library in MATXS* (1985).
- [27] P. Vontobel, and S. Pelloni, "New JEF/EFF Based MATXS-Formatted Nuclear Data Libraries," *Nucl. Sci. Eng.*, **101**, 298 (1989).
- [28] J. R. Askew, F. J. Fayers, and P. B. Kemshell, "A General Description of the Lattice Code WIMS," *J. Brit. Nucl. Energy Soc.*, **5**, 564 (1966).
- [29] C. J. Taubman, *The WIMS 69-Group Library Tape 166259*, Technical Report AEEW-M1324, United Kingdom Atomic Energy Establishment (1975).
- [30] J. J. Kim, J. T. Lee, and H. R. Kim, "Generation and Benchmarking of a 69 Group Cross Section Library for Thermal Reactor Applications," *J. Korean Nucl. Soc.*, **21**, 245 (1989).
- [31] WLUP, *Final Stage of the WIMS-D Library Update Project*, [www-nds.iaea.org/wimsd](http://www-nds.iaea.org/wimsd) (2005).
- [32] J. V. Donnelly, *WIMS-CRNL, A User's Manual for the Chalk River Version of WIMS*, Technical Report AECL-8955, Atomic Energy of Canada Limited (1986).
- [33] R. E. MacFarlane, *TRANSX-2: A Code for Interfacing MATXS Cross-Sections Libraries to Nuclear Transport Codes*, Technical Report LA-12312-MS, Los Alamos National Laboratory (1992).
- [34] R. Roy, "The Cyclic Characteristics Method," *International Topical Meeting on the Physics of Nuclear Science and Technology*, pp. 407–414, Long Island, NY (1998).
- [35] R. Roy, "The Cyclic Characteristics Method with Anisotropic Scattering," *M&C-1999 Conference on Mathematics and Computation, Reactor Physics and Environmental Analysis in Nuclear Applications*, pp. 27–30, Madrid, Spain (1999), (Proceedings available on CD-Rom).
- [36] G. J. Wu, and R. Roy, "A New Characteristics Algorithm for 3D Transport Calculations," *Ann. Nucl. Energy*, **30**, 1–16 (2003).
- [37] M. Dahmani, R. Roy, and J. Koclas, "New Computational Methodology for Large 3D Neutron Transport Problems," *PHYSOR-2004*, Chicago, IL (2004), (Proceedings available on CD-Rom).

- [38] M. Dahmani, and R. Roy, "Parallel Solver Based on Three-Dimensional Characteristics Method: Design and Performance Analysis," *Nucl. Sci. Eng.*, **150**, 155–169 (2005).
- [39] M. T. Sissaoui, and G. Marleau, "Application of the Feedback Model for the History Base Using DRAGON," *19<sup>th</sup> CNS Simulation Symposium*, Hamilton, ON (1995).
- [40] M. T. Sissaoui, G. Marleau, and D. Rozon, "Accounting For Actinide Burnup History in CANDU Reactor simulation," *Advances In Nuclear Fuel Management II*, Myrtle beach, SC (1997).
- [41] M. T. Sissaoui, G. Marleau, and D. Rozon, "CANDU Reactor Simulations Using the Feedback Model with Actinide Burnup History," *Nuclear Technology*, **125**, 197 (1999).
- [42] T. Courau, and G. Marleau, "Calculating Adjoint Fluxes in the Code DRAGON Using the Collision Probability Method," *PHYSOR-2000 International Topical Meeting, Advances in Reactor Physics and Mathematics and Computation into the Next Millennium*, Pittsburgh, PA (2000), (Proceedings available on CD-Rom).
- [43] T. Courau, *Application de la théorie des perturbations généralisées aux calculs de cellules utilisant la méthode des probabilités de collision*, Ph.D. thesis, École Polytechnique de Montréal (2001).
- [44] T. Courau, and G. Marleau, "Generalized Perturbation Theory in DRAGON: Application to CANDU Cell Calculations," *22nd Annual Canadian Nuclear Society Conference*, Toronto, ON (2001), (Proceedings available on CD-Rom).
- [45] T. Courau, and G. Marleau, "Adjoint and Generalized Adjoint Flux Calculations Using the Collision Probability Technique," *Nucl. Sci. Eng.*, **141**, 46–54 (2002).
- [46] T. Courau, and G. Marleau, "Perturbation Theory for Lattice Cell Calculations," *Nucl. Sci. Eng.*, **143**, 19–32 (2003).
- [47] E. Varin, A. Hébert, R. Roy, and J. Koclas, *A User's Guide for DONJON*, Technical Report IGE-208 Rev. 2, École Polytechnique de Montréal (2004).
- [48] G. Marleau, and E. Varin, *An History Interface Between DRAGON and DONJON: The HST: module*, Technical Report IGE-259 Rev. 1, École Polytechnique de Montréal (2004).
- [49] E. Varin, and G. Marleau, "Transport-Diffusion Coupling for CANDU Reactor Core Follow-up," *SNA'2003, International Conference on Supercomputing in Nuclear Applications*, Paris, France (2003), (Proceedings available on CD-Rom).
- [50] E. Varin, and G. Marleau, "A First Attempt at a Candu-6 Core Tracking Using Coupled DRAGON/DONJON Calculations," *6th International Conference on Simulation Methods in Nuclear Engineering*, Montréal, QC (2004), (Proceedings available on CD-Rom).
- [51] E. Varin, and G. Marleau, "Validating the History-based Method in DRAGON/DONJON Using G2 Core Follow-up," *26th Annual Conference of the Canadian Nuclear Society*, Toronto, ON (2005), (Proceedings available on CD-Rom).
- [52] MATLAB, *The Language of Technical Computing*, [www.mathworks.com](http://www.mathworks.com) (2006).
- [53] C. Plamondon, *Vérification des lignes d'intégration et illustration des géométries DRAGON*, Technical Report IGE-290, École Polytechnique de Montréal (2006).
- [54] A. Kavenoky, *Calcul et utilisation des probabilités de première collision pour les milieux hétérogènes à une dimension*, Technical Report CEA-N-1077, Commissariat à l'énergie Atomique (1969).
- [55] A. Hébert, "A Collision Probability Analysis of the Double-Heterogeneity Problem," *Nucl. Sci. Eng.*, **115**, 177 (1993).

- [56] G. Marleau, *New Geometries Processing in DRAGON: The NXT: Module*, Technical Report IGE-260, École Polytechnique de Montréal (2006).
- [57] A. Hébert, "Application of a Dual Variational Formulation to Finite Element Reactor Calculations," *Ann. Nucl. Energy*, **20**, 823 (1993).
- [58] B. G. Carlson, *Tables of Equal Weight Quadrature  $EQ_n$  Over the Unit Sphere*, Technical Report LA-4734, Los Alamos Scientific Laboratory (1971).
- [59] T. Jevremovic, T. Postma, J. Vujic, and K. Tsuda, "A Comparative Study of the NEACRP Nine-Pin Supercell Benchmark by the Two-Dimensional General Geometry Transport Codes," *Trans. Am. Nucl. Soc.*, **99**, 169 (1998).
- [60] M. J. Halsall, *CACTUS: A Characteristics Solution to the Neutron Transport Equation in Complicated Geometries*, Technical Report AEEW-R 1291, United Kingdom Atomic Energy Establishment (1980).
- [61] G. Longoni, and A. Haghghat, "Development of New Quadrature Sets with the "Ordinate Splitting" Technique," *M&C-2001, American Nuclear Society Topical Meeting in Mathematics and Computations*, Salt Lake City, Utah (2001), (Proceedings available on CD-Rom).
- [62] R. Sanchez, L. Mao, and S. Santandrea, "Treatment of Boundary Conditions in Trajectory-Based Deterministic Transport Methods," *Nucl. Sci. Eng.*, **140**, 23–50 (2002).
- [63] A. Hébert, and G. Marleau, "Generalization of the Stamm'ler Method for the Self-Shielding of Resonant Isotopes in Arbitrary Geometries," *Nucl. Sci. Eng.*, **108**, 230 (1991).
- [64] A. Hébert, "Revisiting the Stamm'ler Self-Shielding Method," *25th Annual Canadian Nuclear Society Conference*, Toronto (2004), (Proceedings available on CD-Rom).
- [65] R. Roy, and G. Marleau, "Normalization Techniques for Collision Probability Matrices," *PHYSOR-1990*, pp. IX.40–IX.49, Marseille, France (1990).
- [66] E. A. Villarino, R. J. Stamm'ler, A. A. Ferri, and J. J. Casal, "HELIOS: Angularly Dependent Collision Probabilities," *Nucl. Sci. Eng.*, **112**, 16–31 (1992).
- [67] A. Hébert, "A Consistent Technique for the Pin-by-Pin Homogenization of a Pressurized Water Reactor Assembly," *Nucl. Sci. Eng.*, **113**, 227 (1993).
- [68] A. Hébert, and A. Mathonnière, "Development of a Third-Generation Superhomogénéisation Method for the Homogenization of a Pressurized Water Reactor Assembly," *Nucl. Sci. Eng.*, **115**, 129 (1993).
- [69] G. Rimpault, "Algorithmic Features of the ECCO Cell Code for Treating Heterogeneous Fast Reactor Sub-assemblies," *M&C-1995, International Conference on Mathematics and Computations, Reactor Physics, and Environmental Analyses*, Portland, OR (1995), (Proceedings available on CD-Rom).
- [70] P. Benoist, J. Mondot, and I. Petrovic, "Calculational and Experimental Investigations of Void Effect - A Simple Theoretical Model for Space-Dependent Leakage Treatment of Heterogeneous Assemblies," *Nucl. Sci. Eng.*, **118**, 194 (1994).
- [71] I. Petrovic, P. Benoist, and G. Marleau, "A Quasi-Isotropic Reflecting Boundary Condition for the Heterogeneous Leakage Model Tibere," *Nucl. Sci. Eng.*, **122**, 151 (1996).
- [72] G. Marleau, and E. Debos, "Homogenization of Linearly Anisotropic Scattering Cross Sections in a Consistent  $B_1$  Heterogeneous Leakage Model," *Nineteenth Annual Conference of the Canadian Nuclear Society*, Toronto, ON (1998).
- [73] G. Marleau, "Coherent Anisotropic Scattering Homogenization in the  $B_1$  Leakage Model," *M&C-1999 Conference on Mathematics and Computation, Reactor Physics and Environmental Analysis in Nuclear Applications*, Madrid, Spain (1999), (Proceedings available on CD-Rom).

- [74] A. Hébert, "Development of a Second Generation SPH Technique for the Pin-by-Pin Homogenization of a Pressurized Water Reactor Assembly in Hexagonal Geometry," *Trans. Am. Nucl. Soc.*, **71**, 253 (1994).
- [75] W. H. Press, B. P. Flannery, S. A. Teukolsky, and W. T. Vetterling, *Numerical Recipes, Second Edition (FORTRAN Version)*, Cambridge University Press, Cambridge, MA (1994).
- [76] G. Marleau, "Fine Mesh 3-D Collision Probability Calculations Using the Lattice Code DRAGON," *International Conference on the Physics of Nuclear Science and Technology*, Long Island, NY (1998).
- [77] G. Marleau, "New Geometric Capabilities of DRAGON," *Nineteenth Annual Conference of the Canadian Nuclear Society*, Toronto, ON (1998).
- [78] K. E. Kohler, *PostScript for Technical Drawings PSPLLOT: A FORTRAN-Callable PostScript Plotting Library User's Manual*, [www.nova.edu/ocean](http://www.nova.edu/ocean) (2000).
- [79] T. O. Theisen, *Ghostview: An X11 user interface for Ghostscript* (2000).
- [80] v. Stankovski, "Refinement of the Substructure Method for Integral Transport Calculations," *Nucl. Sci. Eng.*, **92**, 255 (1986).
- [81] R. T. Akroyd, and N. S. Riyait, "Iteration and Extrapolation Methods for the Approximate Solution of the Even-Parity Transport Equation for systems with voids," *Ann. Nucl. Energy*, **16**, 1 (1989).
- [82] R. D. Mosteller, L. D. Eisenhart, R. C. Little, W. J. Eich, and J. Chao, "Benchmark Calculations for the Doppler Coefficient of Reactivity," *Nucl. Sci. Eng.*, **107**, 265–271 (1991).



## FIGURES

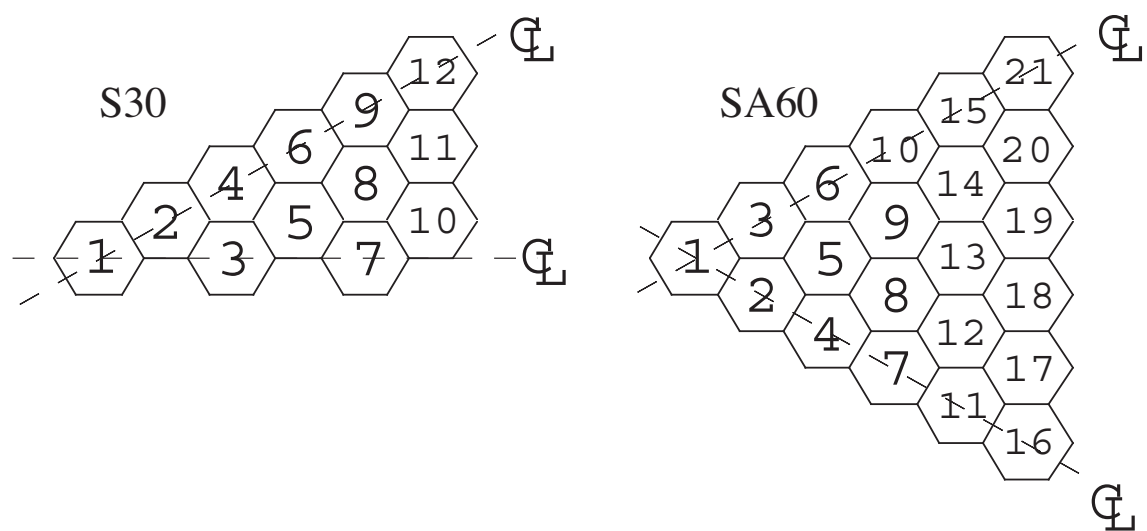


Figure 1: Hexagonal geometries of type S30 and SA60

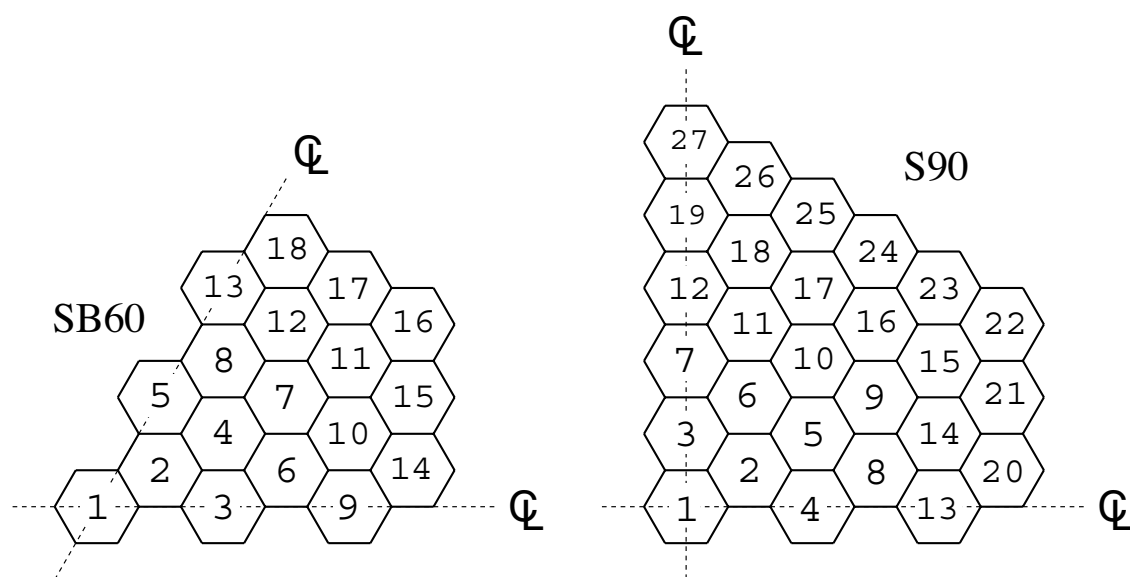


Figure 2: Hexagonal geometries of type SB60 and S90

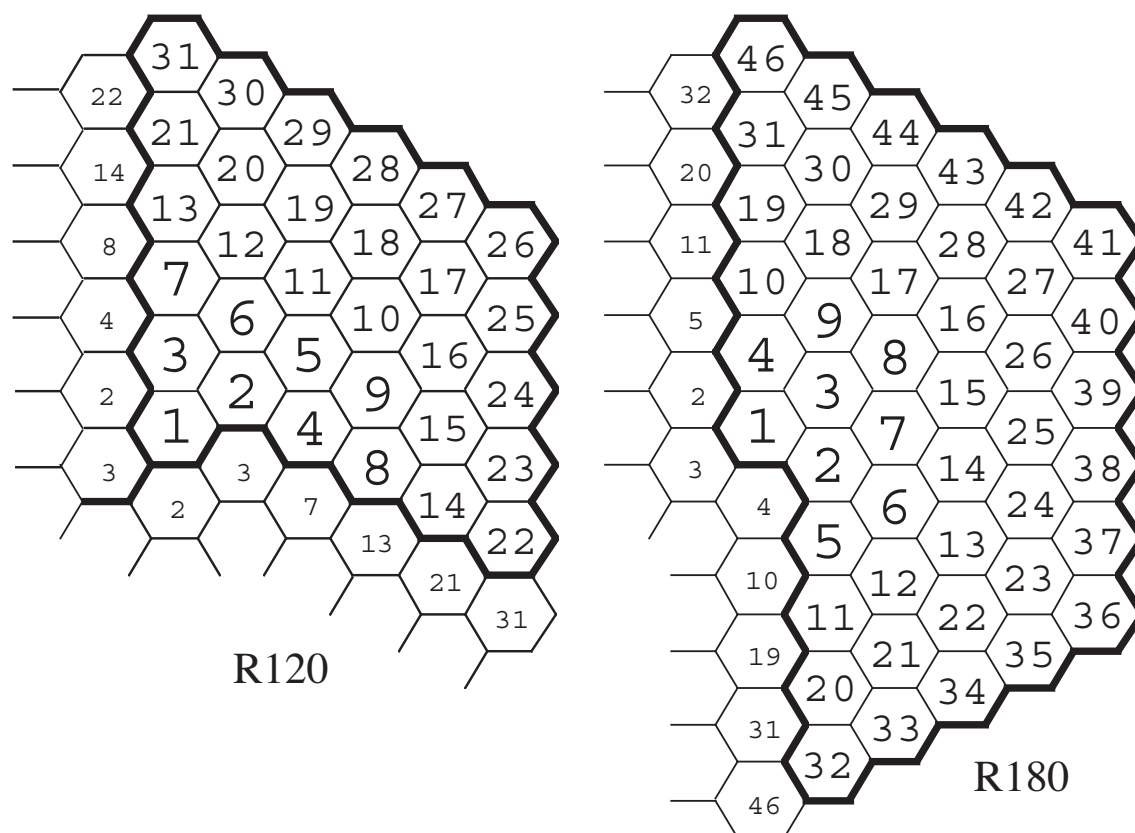


Figure 3: Hexagonal geometries of type R120 and R180

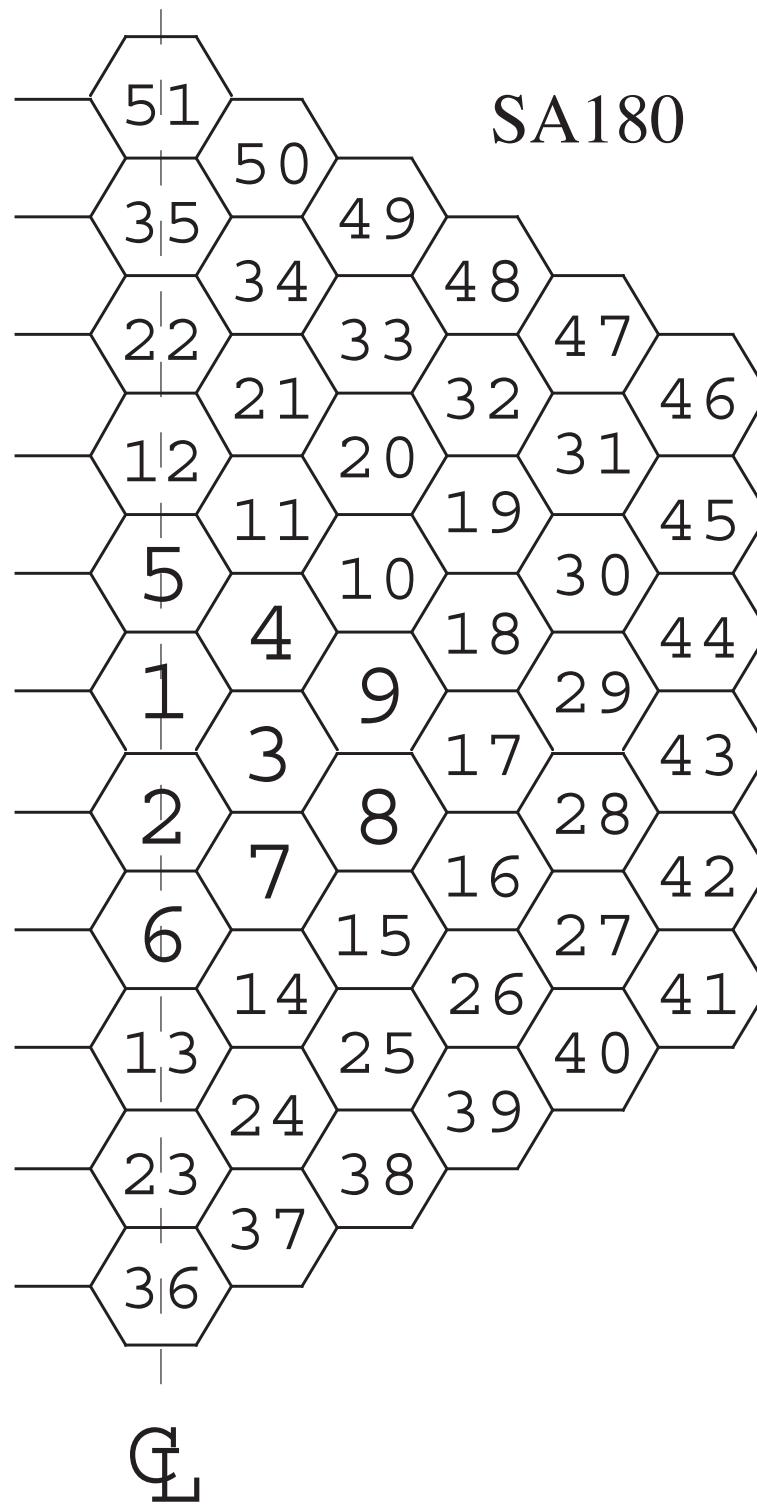


Figure 4: Hexagonal geometry of type SA180

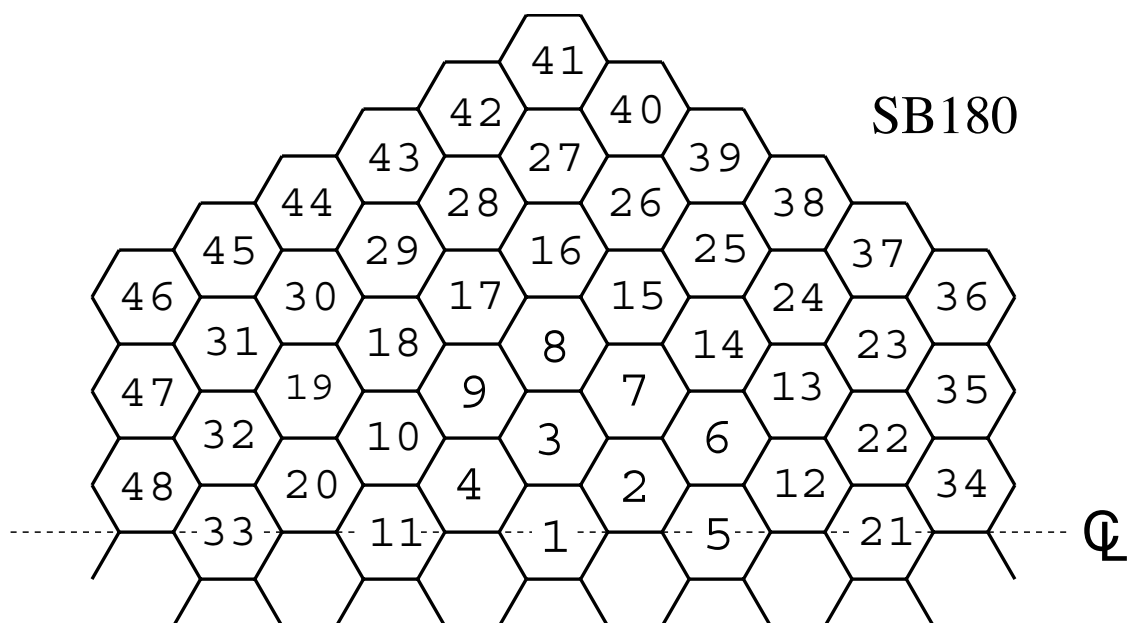


Figure 5: Hexagonal geometry of type SB180

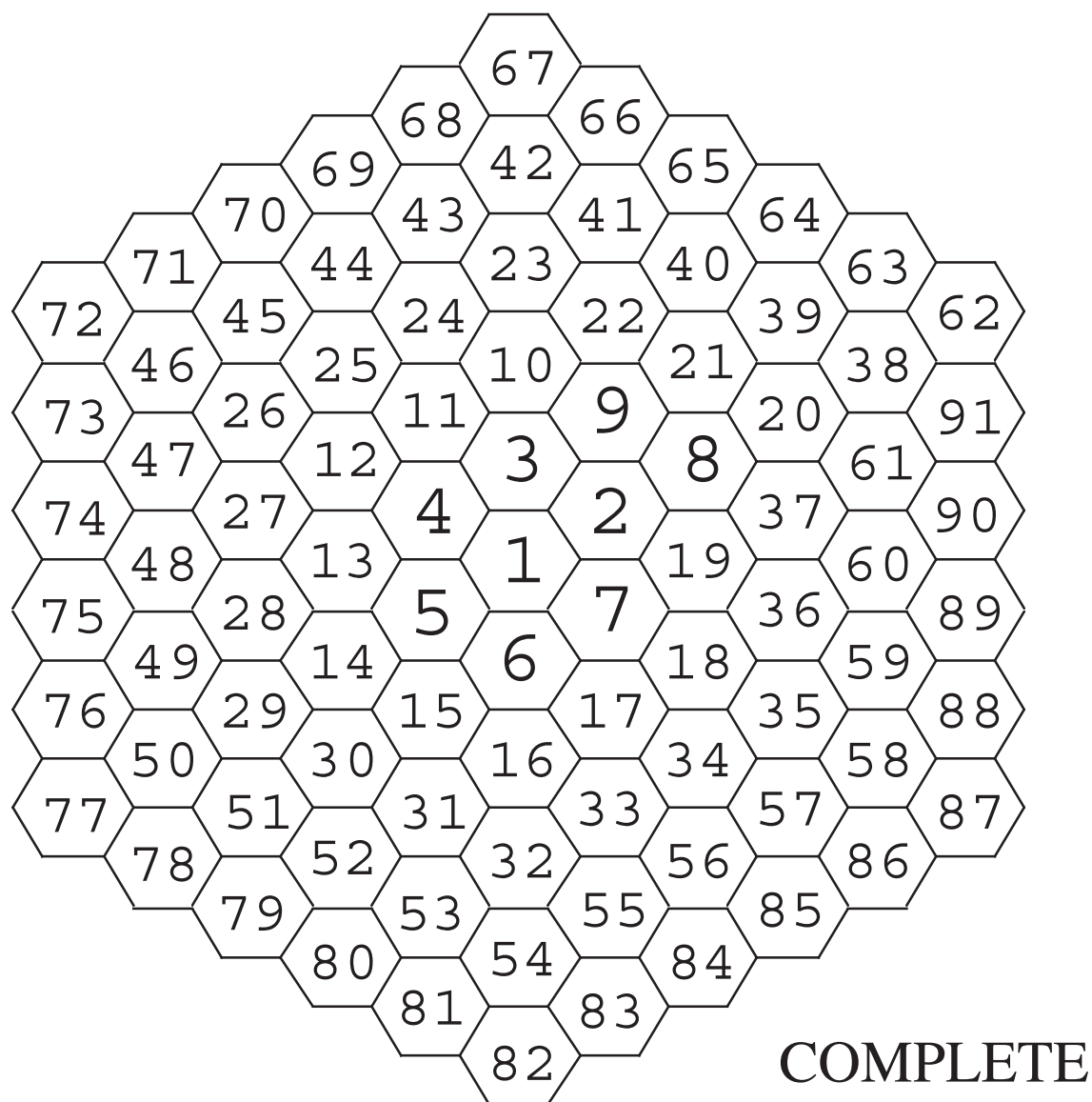


Figure 6: Hexagonal geometry of type COMPLETE

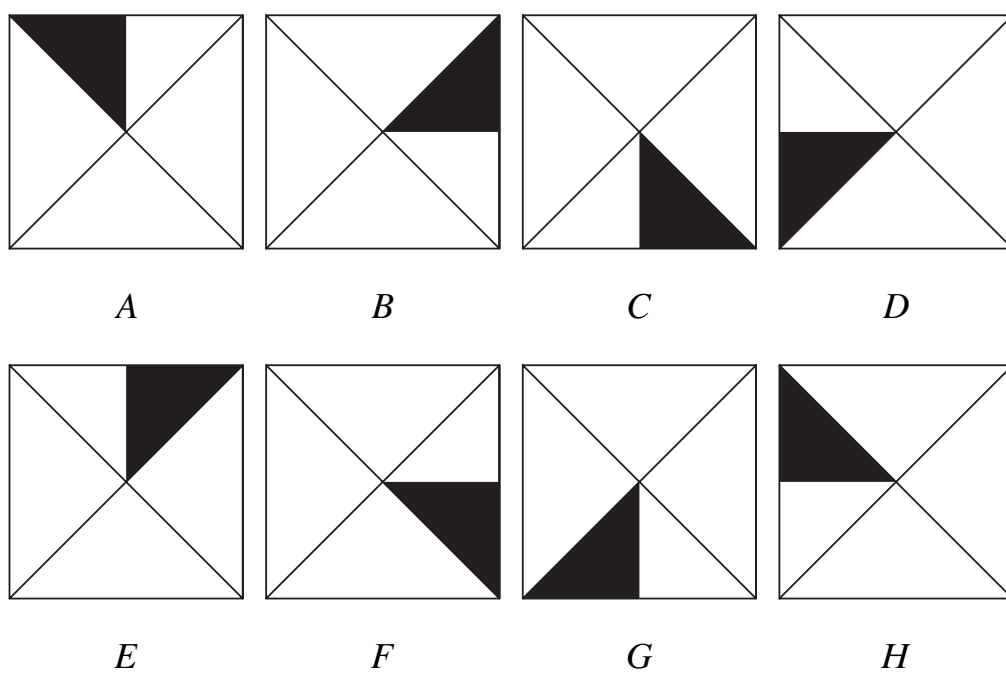


Figure 7: Description of the various rotations allowed for Cartesian geometries

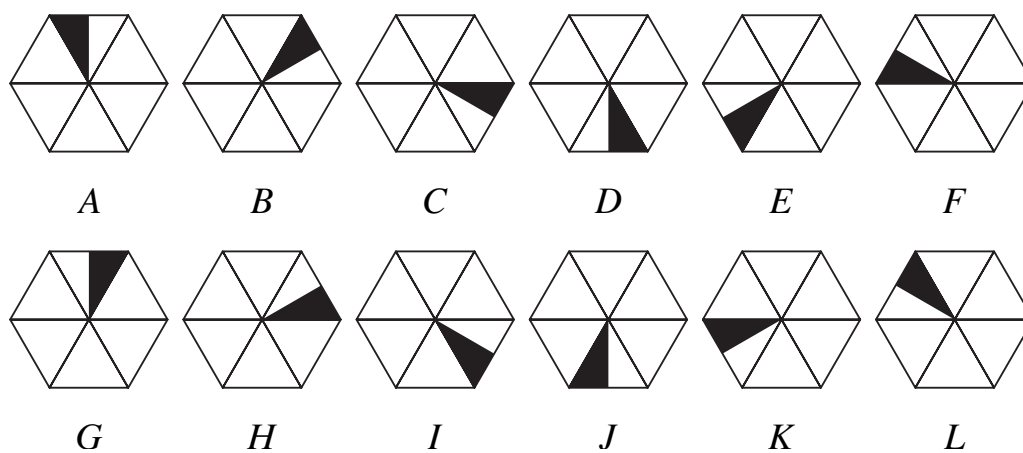


Figure 8: Description of the various rotation allowed for hexagonal geometries

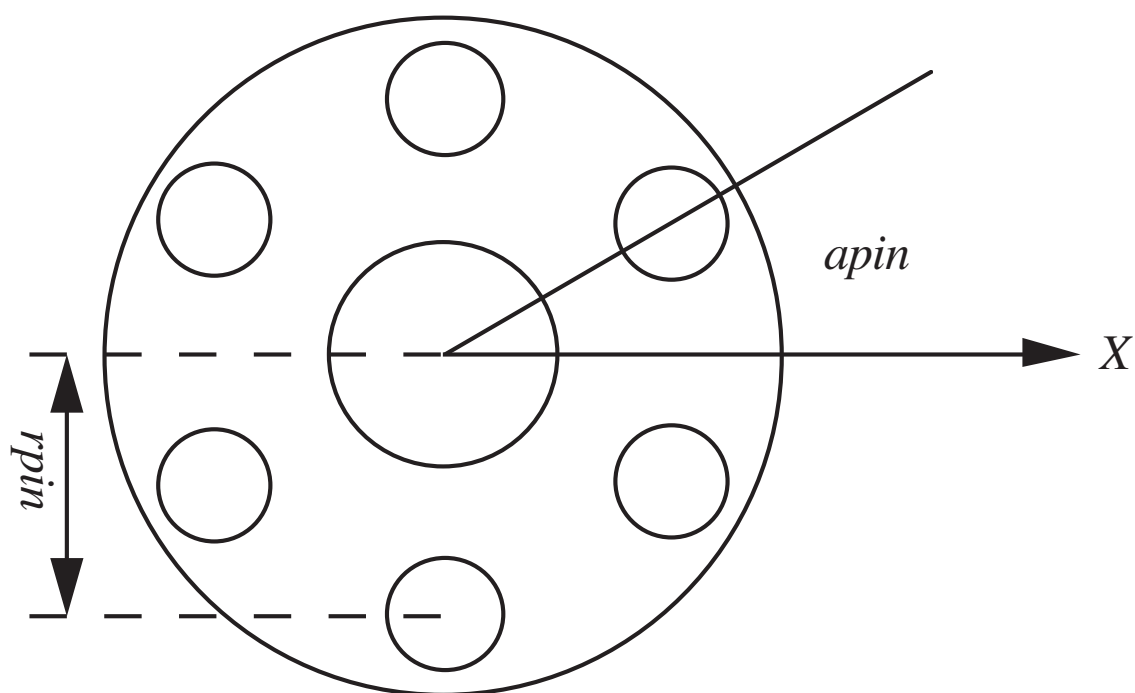


Figure 9: Typical cluster geometry



Figure 10: Slab geometry with mesh splitting

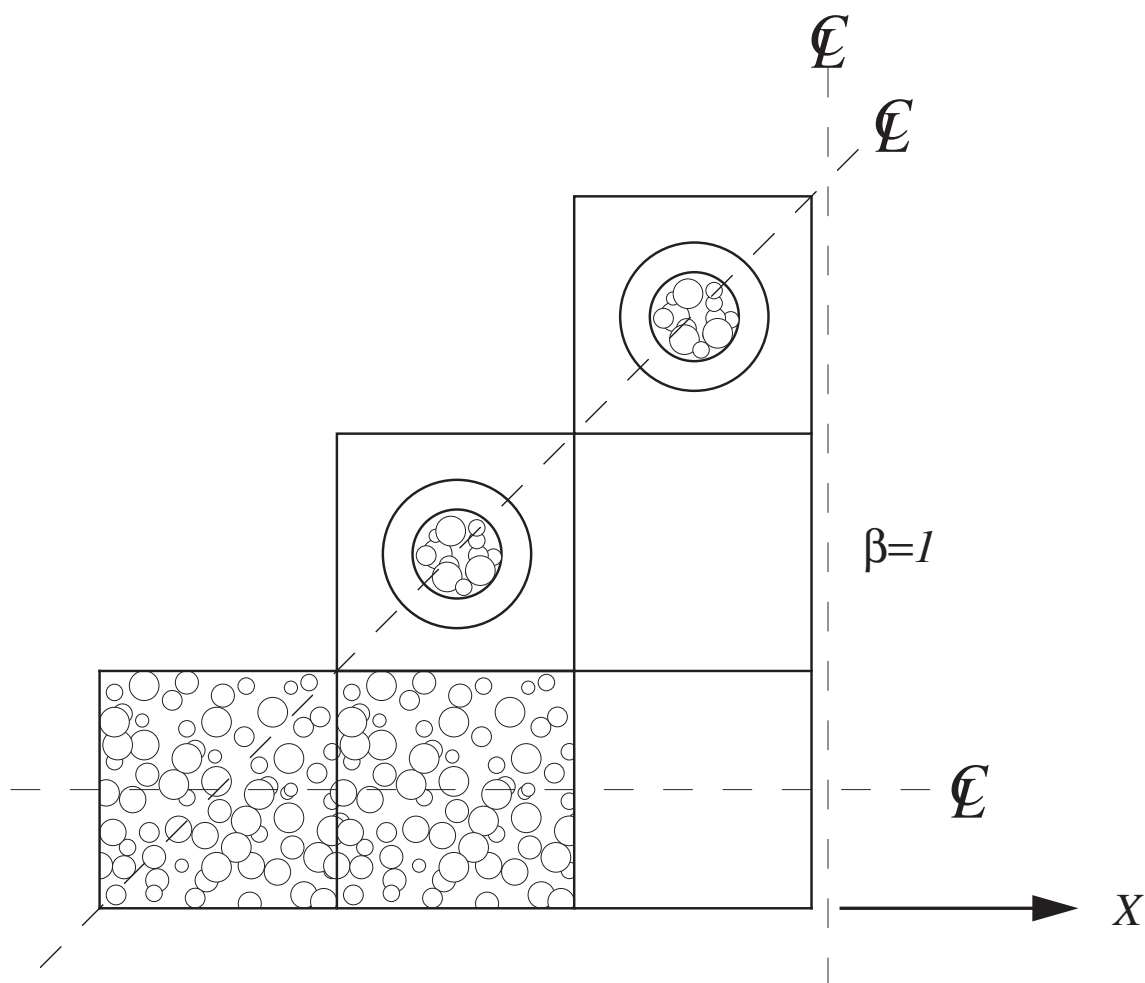


Figure 11: Two dimensional Cartesian assembly containing micro structures

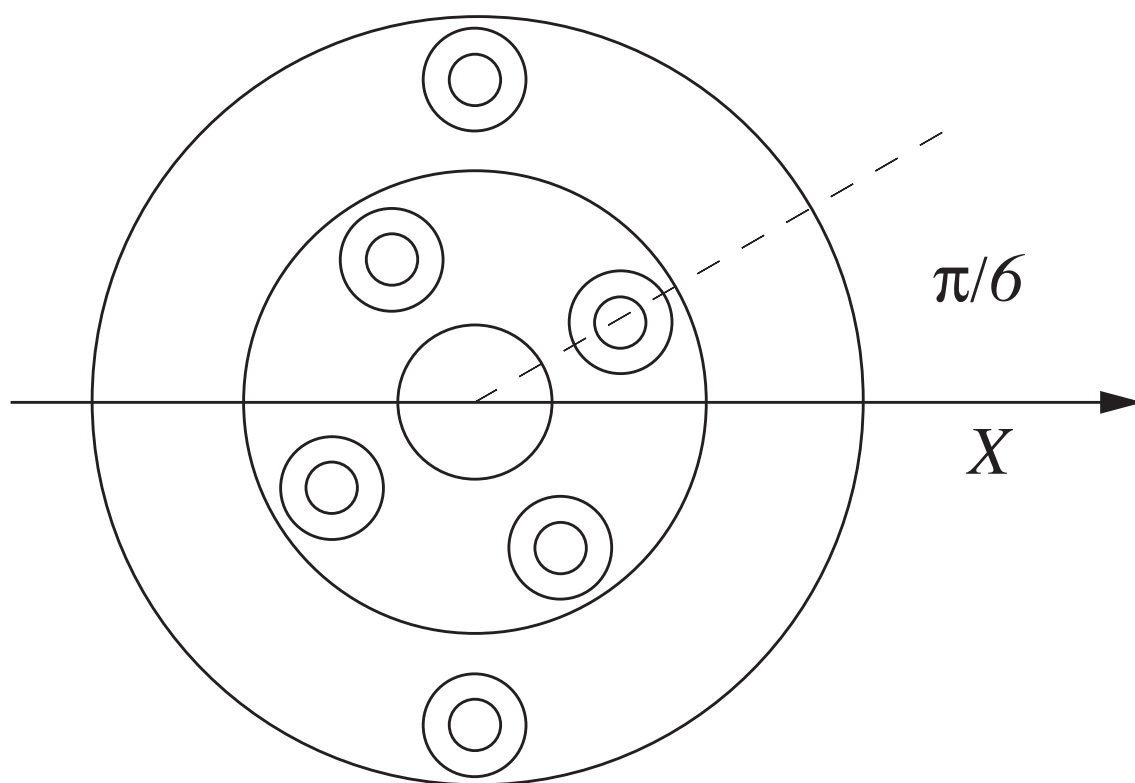


Figure 12: Cylindrical cluster geometry

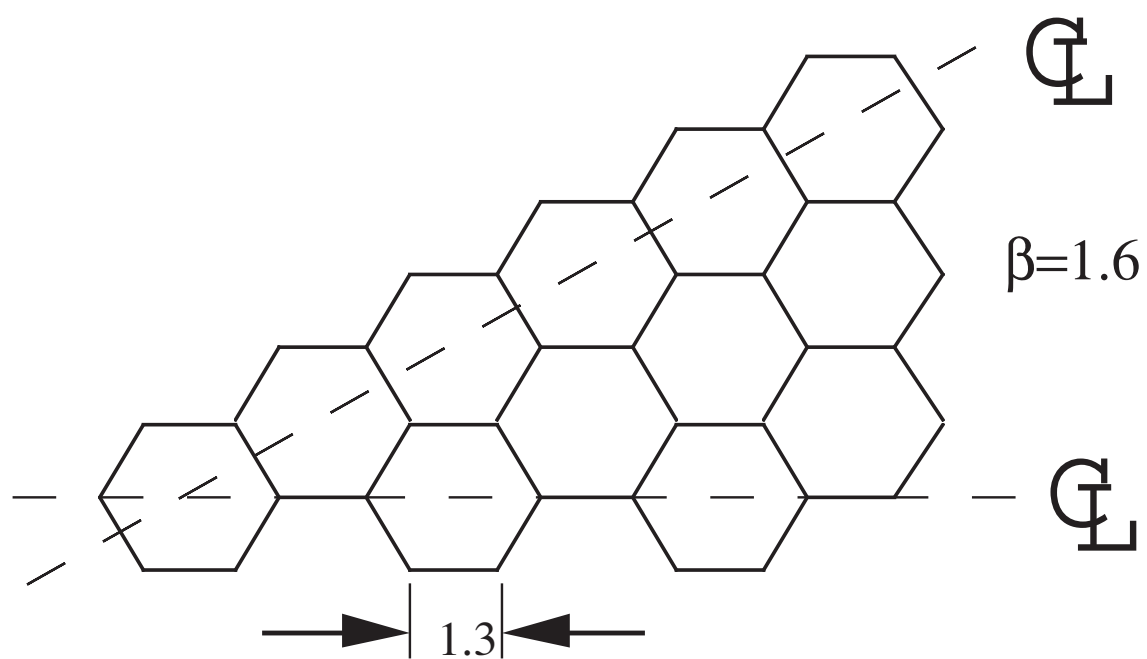


Figure 13: Two dimensional hexagonal geometry

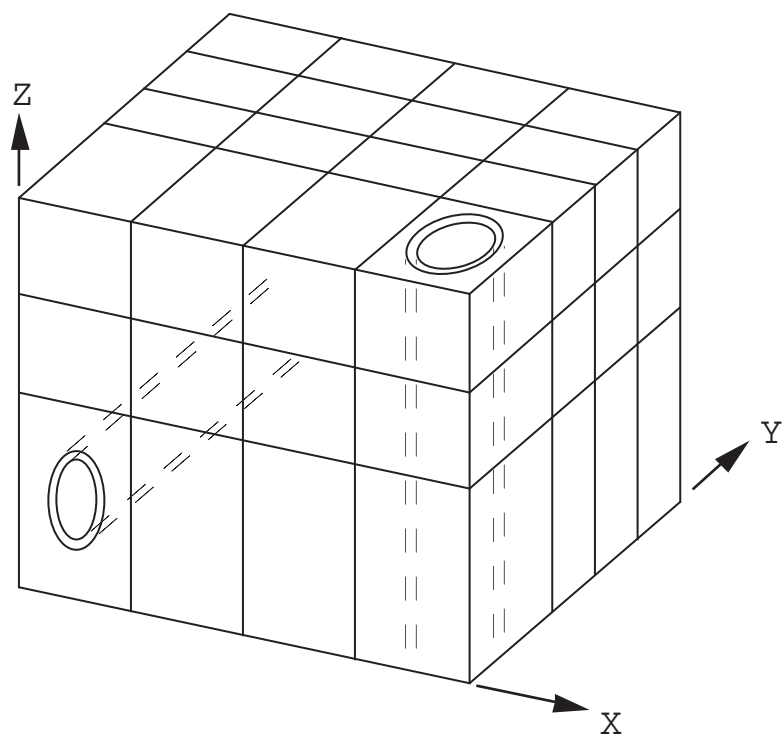


Figure 14: Three dimensional Cartesian supercell

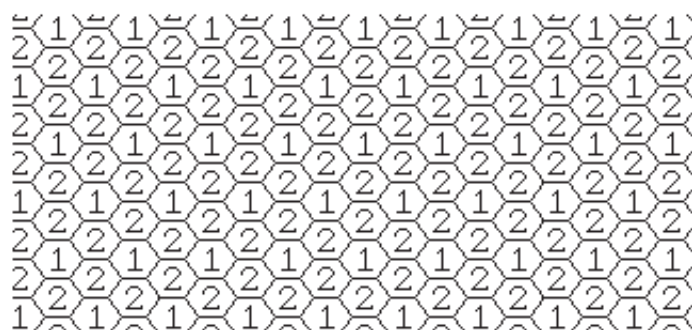


Figure 15: Hexagonal multicell lattice geometry

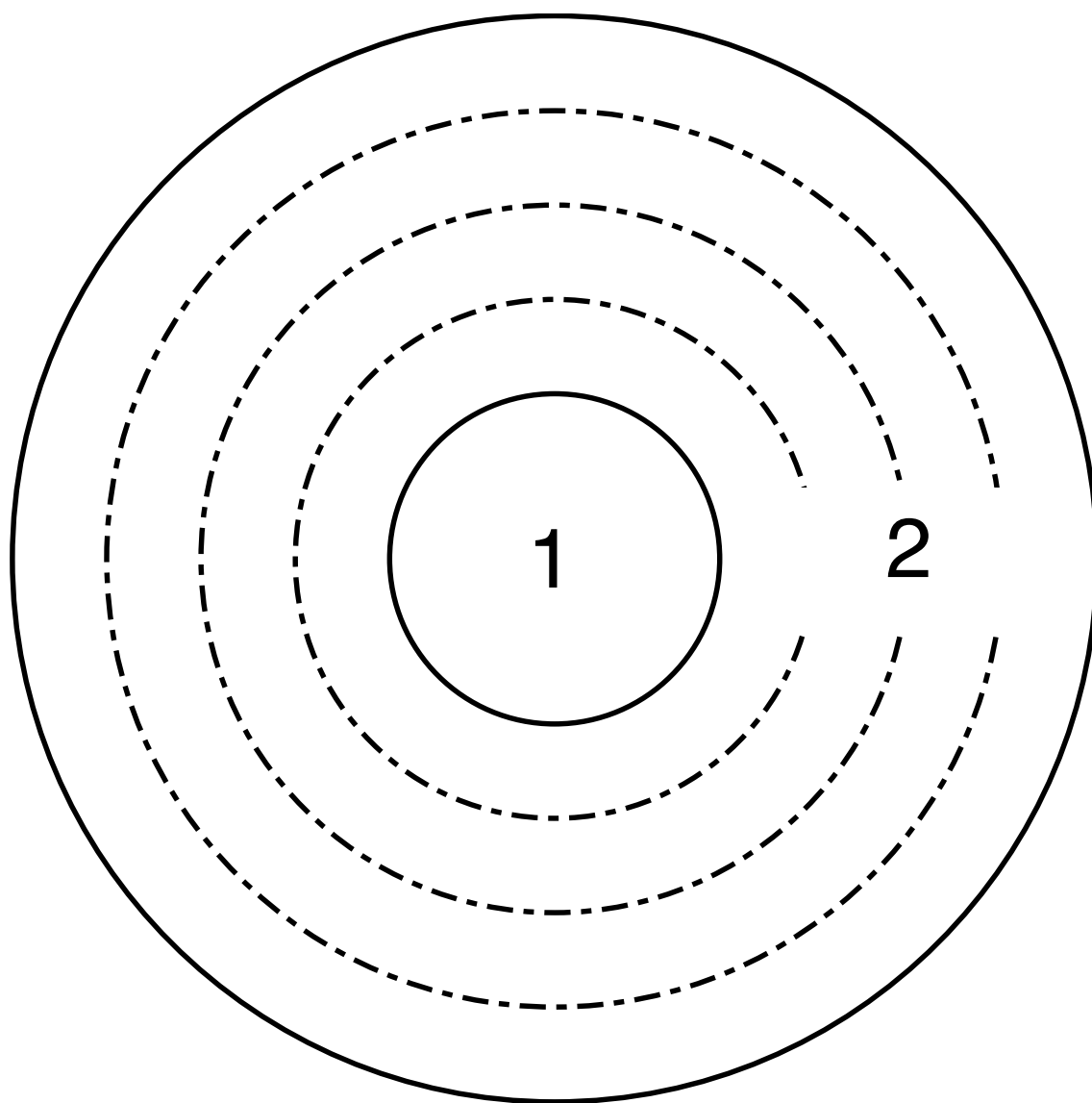
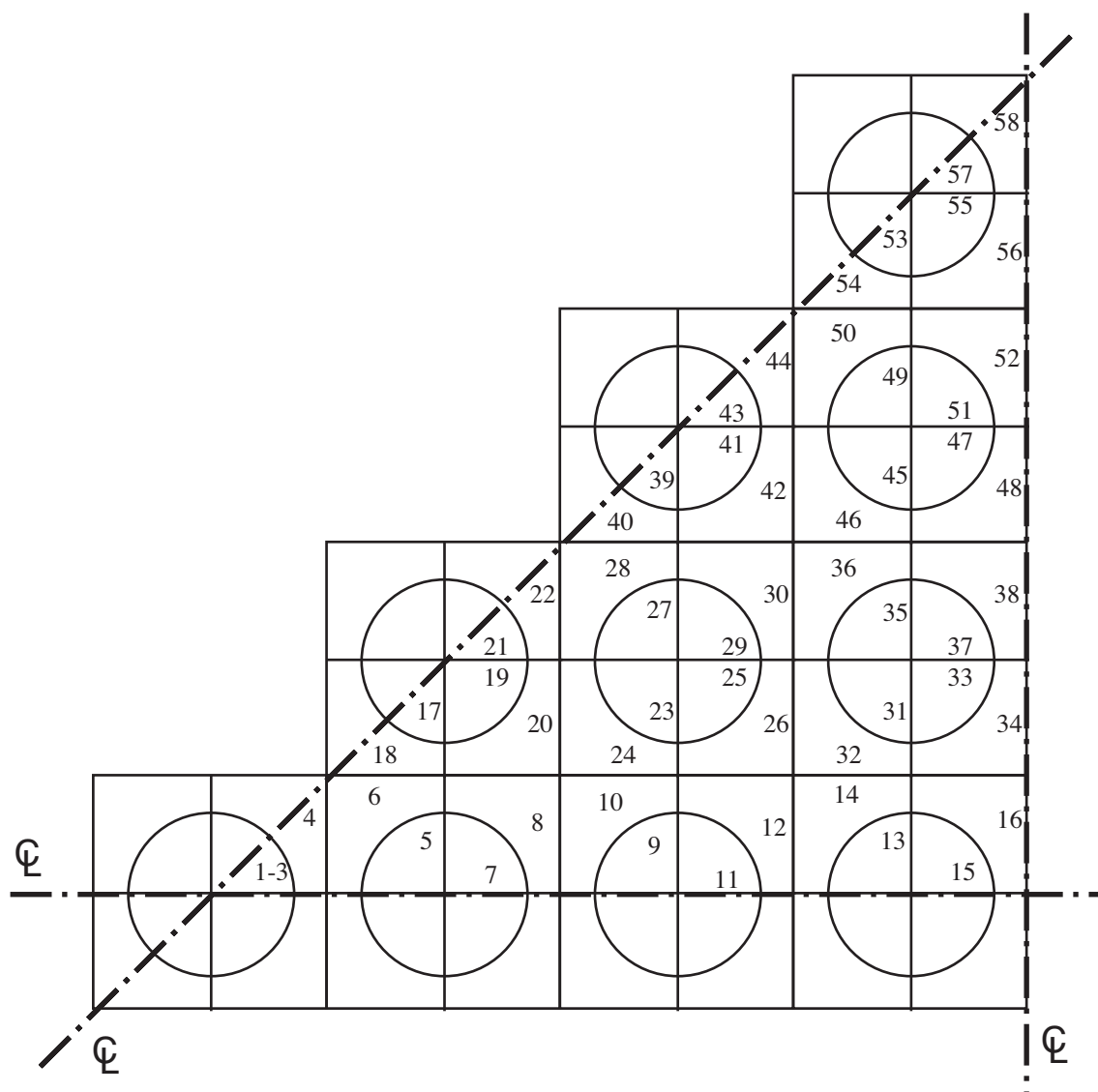


Figure 16: Geometry for test case **TCM01** for an annular cell with macroscopic cross sections.

Figure 17: Geometry for test case **TCM02**.

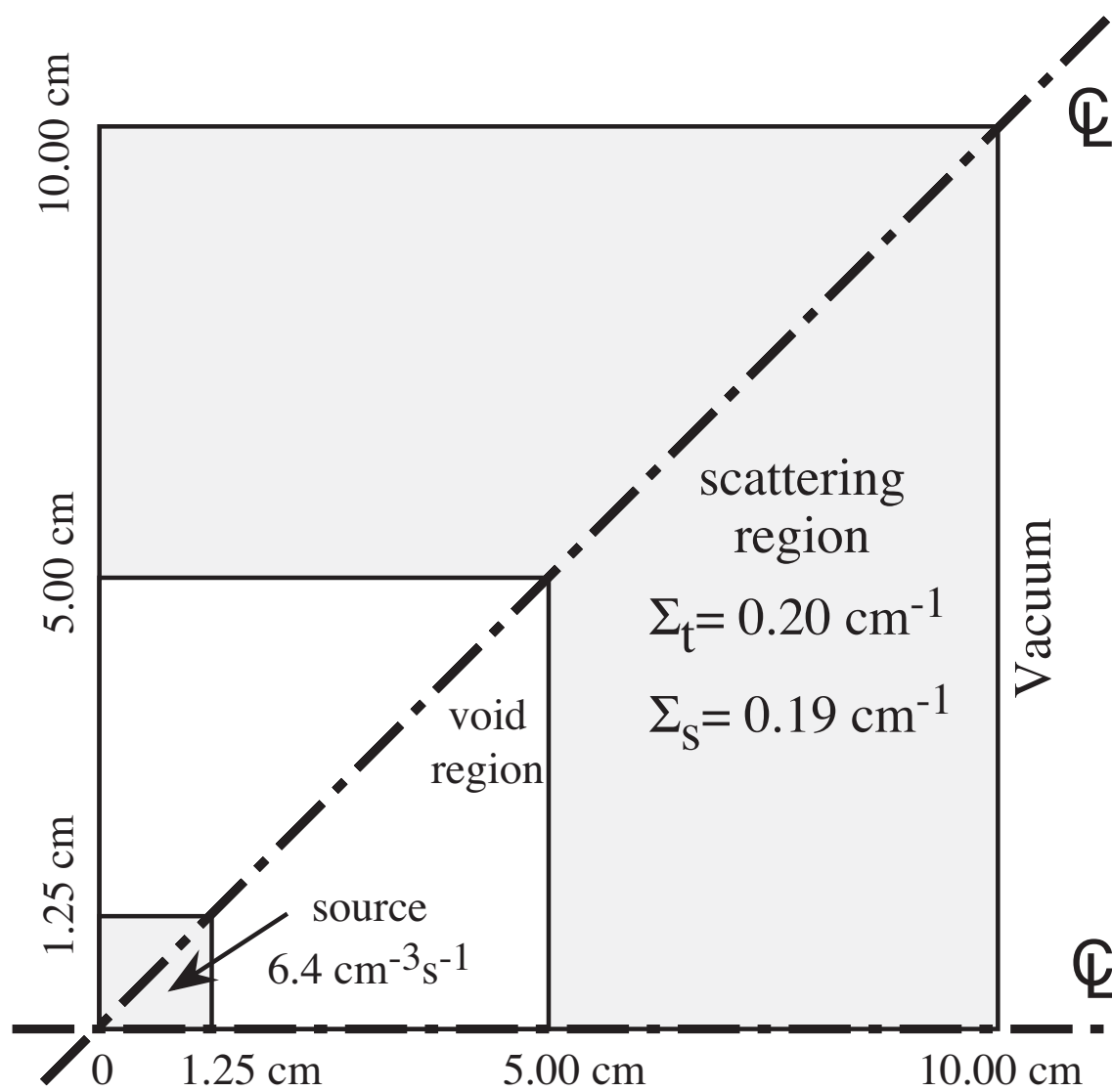


Figure 18: Geometry for test case TCM03.

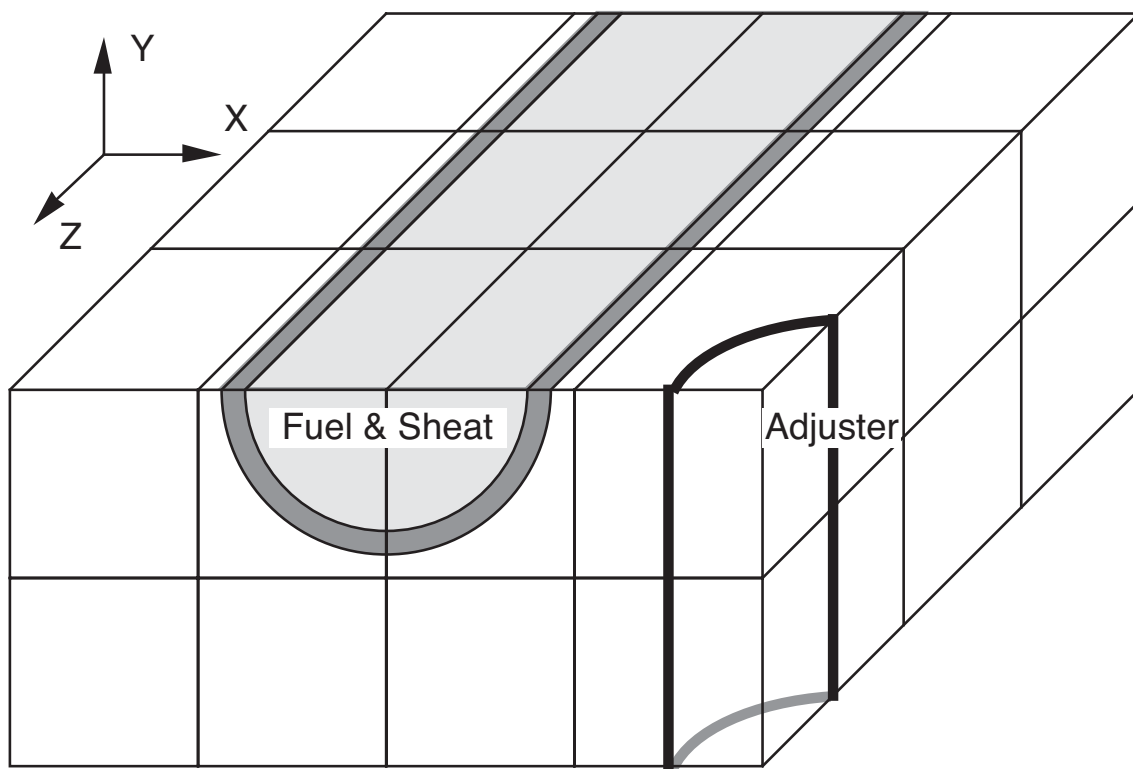


Figure 19: Geometry of the CANDU-6 supercell with stainless steel adjuster rods.

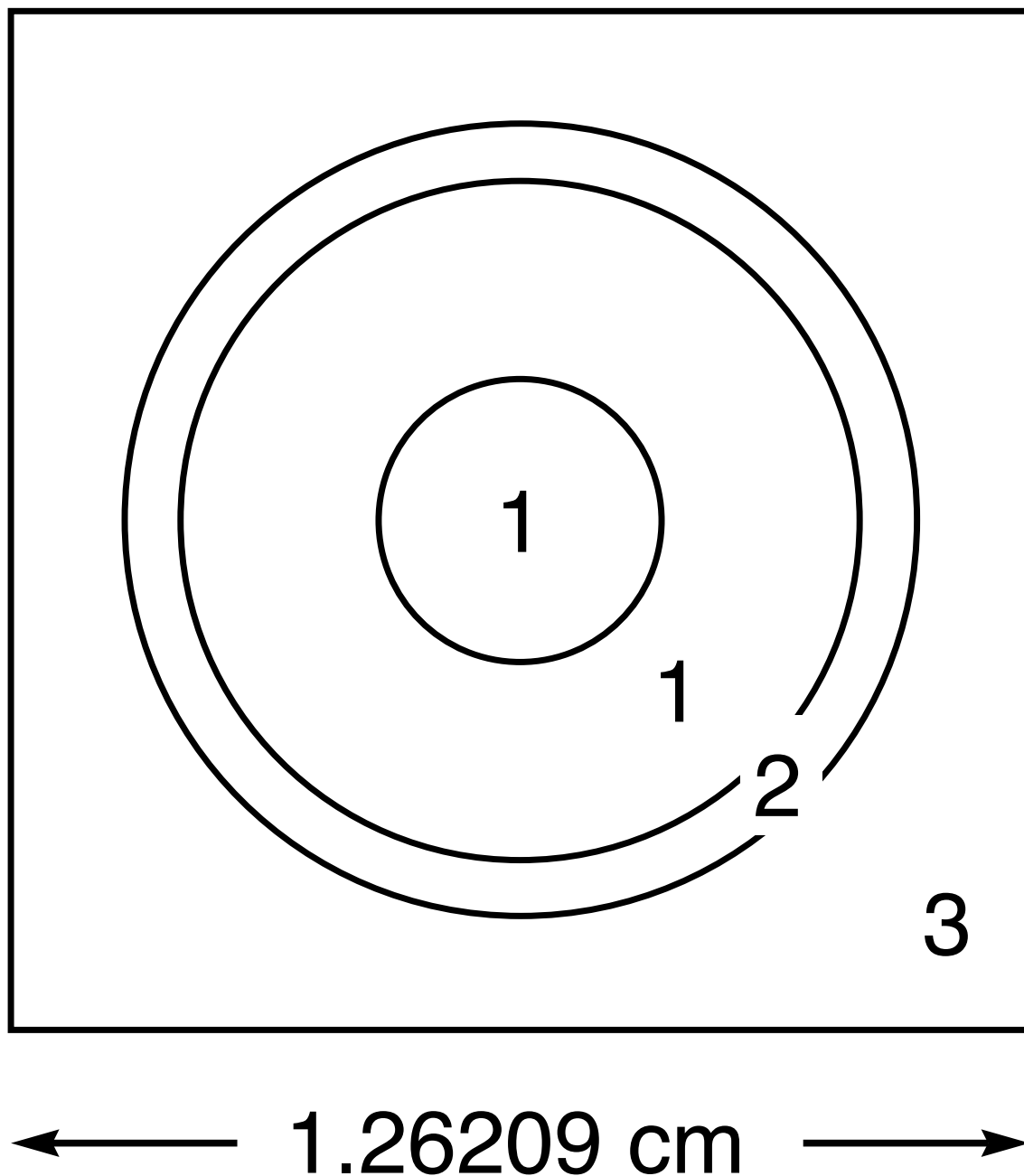


Figure 20: Geometry for the Mosteller benchmark problem used for TCWU01.

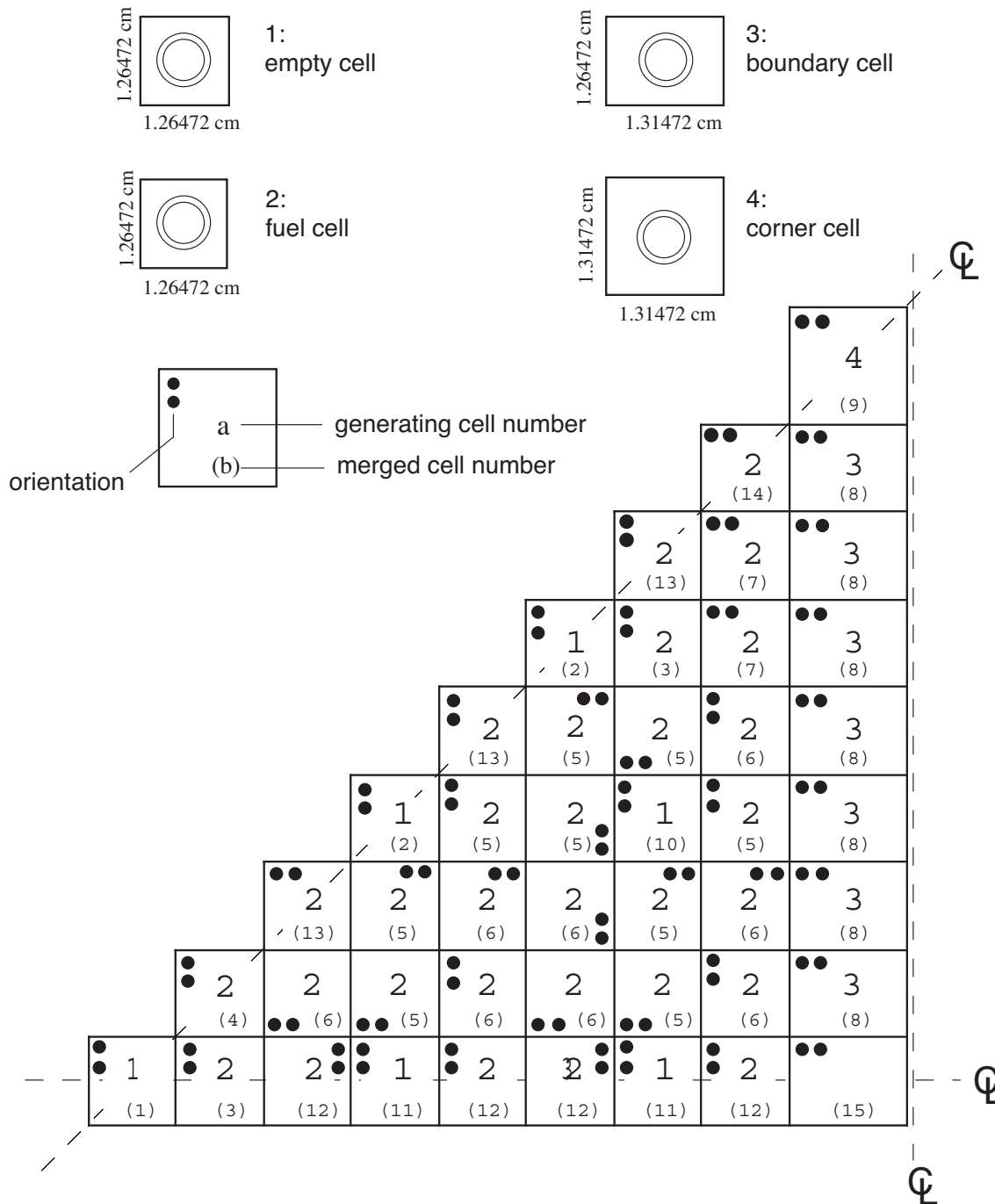
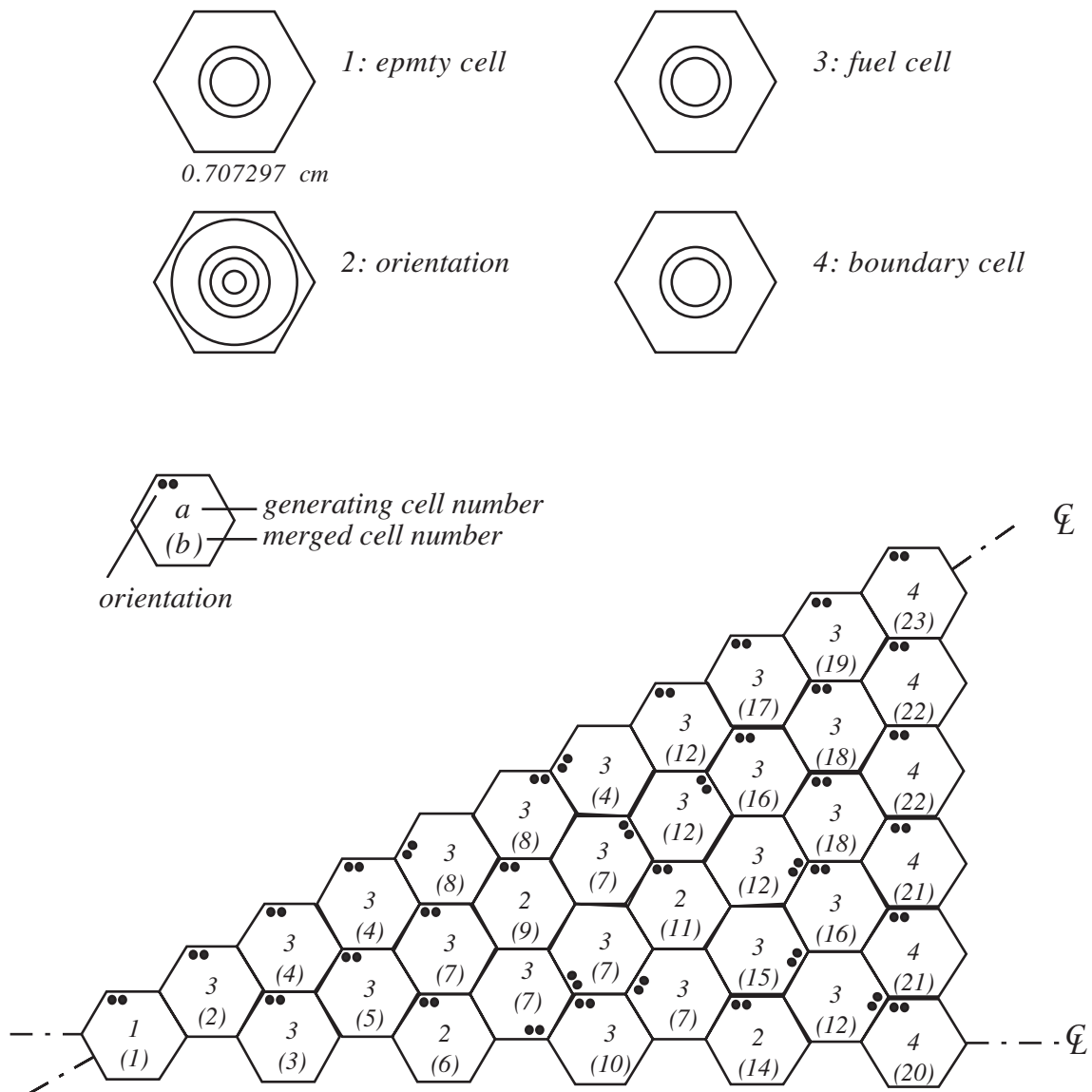


Figure 21: Geometry for test case TCWU02.

Figure 22: Geometry for test case **TCWU03**.

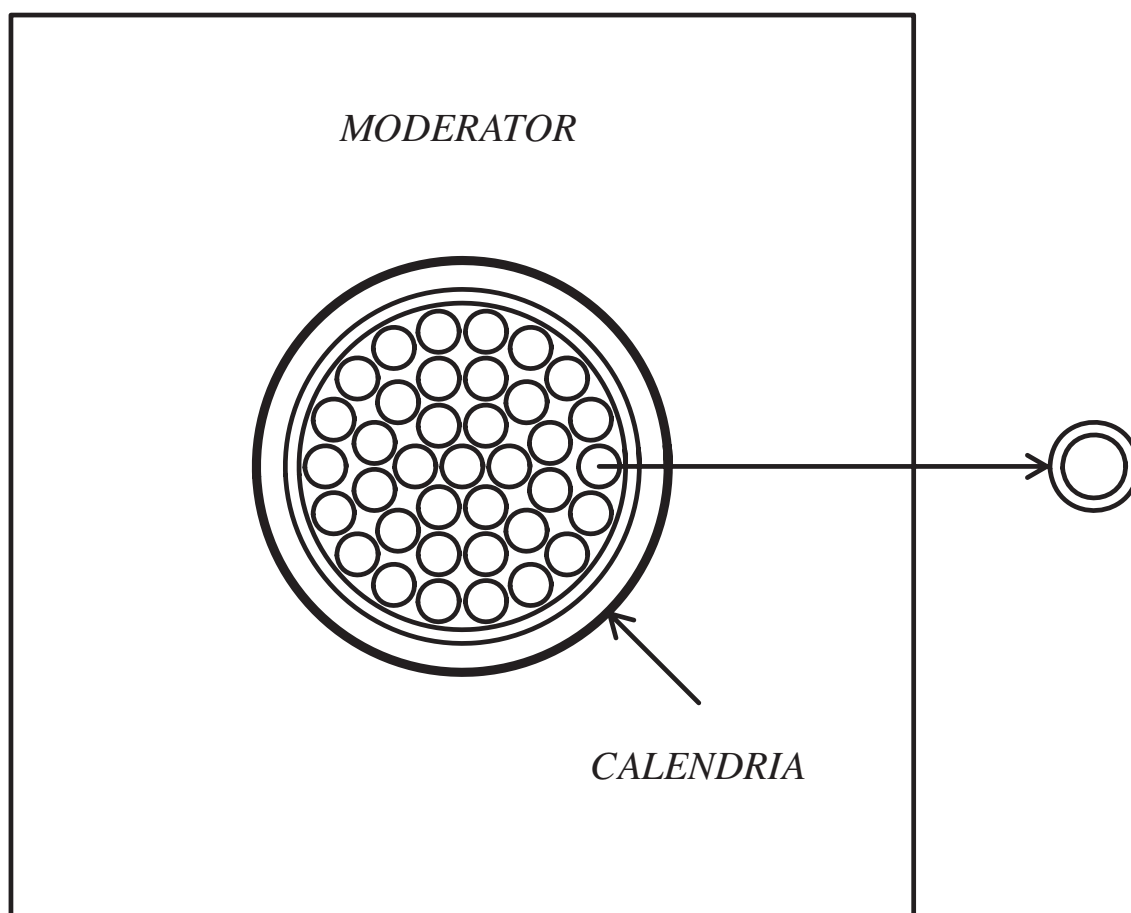


Figure 23: Geometry of the CANDU-6 cell.

## INDEX

**Symbols**

**:**, 9, 15, 25, 39, 40, 51, 53, 56, 61, 63, 69, 72, 74,  
76, 78, 79, 81, 84–86, 88  
**::**, 26, 67  
**:=**, 9, 15, 25, 26, 39, 40, 51, 53, 56, 61, 63, 69, 72,  
76, 78, 79, 81, 84–86, 88  
**;**, 4, 5, 26  
**=**, 21, 22

**A**

a, 89, 90  
A, 89, 90  
ACCE, 57, 58, 62, 81, 83  
ACTI, 64, 66  
ADD, 11, 12  
ADED, 16, 17  
AF, 57, 81, 82  
ALBE, 28, 29  
albedo, 28, 29  
albedp, 11  
albp, 15  
ALBP, 11  
ALBPG, 15  
ALBS, 54–56, 59, 67, 68  
ALL, 64, 66, 67, 73, 74, 81  
ALLG, 54, 55  
ALSB, 57, 58  
ANIS, 10, 16, 17, 40, 41, 59  
APIN, 30, 31  
apins, 30, 31, 39  
APLIB1, 16  
APOL, 11, 16, 17  
AREFL, 86  
ARM, 54  
ASCII, 88  
ASKE, 45–47, 49  
(ASM:), xiv, 53  
ASM:, viii, 3, 6, 7, 39, 42, 44, 53, 54, 57–59, 68, 83  
ASMPIJ, 3, 7, 53, 56, 63, 81  
ATM%, 75, 76

**B**

b, 89, 90  
B, 57, 59, 62, 89, 90  
B0, 59, 68  
B0TR, 59, 68  
B1, 59, 68  
B2, 59, 60, 73  
BIHET, 36  
(BIVACT:), xiv, 40

BIVACT:, viii, 6, 7, 37, 38, 40, 41, 49, 67–69  
BP00, 47, 49  
BP01, 47, 49  
BREFL, 86  
BRNNAM, 69, 70, 72, 73  
BRNOLD, 15, 19, 24  
(brnpar), 86  
BUCK, 59, 60  
BUNBLES, 87  
BUNDLES, 87  
bunl, 87  
BURN, 19, 88  
BURNUP, xv, 8, 15, 16, 23, 69, 73, 85, 86  
BURNUP, 85, 86  
BURNUP, 73

**C**

c, 89, 90  
C, 75, 89, 90  
CACA, 42–44  
CACB, 42–44  
CALC, 75, 76, 85  
CAR1D, 26, 32, 38, 46, 48  
CAR2D, 26, 32, 38  
CAR3D, 26, 32, 38  
CARCEL, 26, 27, 31, 33, 34, 38, 42  
CARCELX, 26, 27, 31, 33, 34, 38, 39  
CARCELY, 26, 27, 31, 33, 35, 38, 39  
CARCELZ, 26, 27, 31, 33, 34, 38, 39  
CDEPCHN, 16, 18  
CDIRN, 66, 67  
CELL, 34, 35, 37  
CELLID, 88  
CELLID, 85, 86  
(CFC:), xv, 76  
CFC:, ix, 6, 8, 76, 77  
CFCNAM, 76, 77  
CGPA, 57, 58, 81, 83  
CHAIN, 20  
CHANNELS, 87  
CHI, 13, 14  
CHID, 17  
CHIS, 17  
CLUSTER, 34, 35, 39  
CMYK, 80  
COHERENT, 64  
COMB, 21, 23, 155  
COMP, 64, 65, 68, 81, 83  
COMPLETE, 28, 29  
COND, 64, 65, 81, 83

*congpa*, 57, 58  
 COOL, 70, 71  
 CORN, 42, 43, 45, 56  
 CPO, 8, 72, 77  
**(CPO:)**, xv, 72  
 CPO:, ix, 6–8, 72, 73  
 CPONAM, 72, 73, 76, 77  
 CTRA, 11–13, 16, 17, 52, 73  
 CURRENT, 64  
 CUT, 42–44

## D

*d*, 89, 90  
 D, 89, 90  
 D2O, 75, 76  
 DAY, 70, 71  
 DB2, 59, 60  
 DBYE, 21, 22  
*dcr*, 20  
 DECAY, 20  
 DECO, 57, 58  
 DELE, 11, 12  
 DELS, 64, 67  
*denmix*, 21, 22  
*dens*, 21, 22, 24, 42, 43, 45, 56, 75, 76  
 DENS, 75, 76  
*densz*, 42, 43, 45  
 DEPL, 16, 18, 70  
**(descasm)**, xiv, 53, 54  
**(descBC)**, xiv, 26–28, 57, 58  
**(descbivac)**, xiv, 40, 49, 67, 69  
**(descfc)**, xv, 76–78  
**(descppo)**, xv, 72, 73  
**(descdepl)**, xiv, 16, 18, 20  
**(descedi)**, xv, 63, 64  
**(descevo)**, 69  
**(descexcel)**, xiv, 39, 40, 42, 61, 67, 69  
**(descflu)**, xiv, 56, 57  
**(descgcnt)**, xiv, 25, 26  
**(descgtyp)**, xiv, 25, 26  
**(descinfo)**, xv, 74, 75  
**(descjpm)**, xiv, 39, 40, 47, 67, 69  
**(descleak)**, xiv, 57–59, 62  
**(desclib)**, xiv, 15, 16  
**(desclibbrn)**, xiv, 15, 16, 18, 19  
**(desclibupd)**, xiv, 15, 16, 19  
**(descmac)**, viii, xiv, 9, 10  
**(descmaci)**, viii, xiv, 9–11  
**(descmacm)**, viii, xiv, 9, 12  
**(descmcu)**, xiv, 61, 62  
**(descmix1)**, viii, xiv, 16, 18, 21, 23  
**(descmix2)**, viii, xiv, 19, 23, 24

**(descmix3)**, viii, xiv, 19, 20, 24  
**(descmoc)**, xiv, 61, 62  
**(descmpa)**, xiv, 11, 12, 15  
**(descmrg)**, xv, 78, 79  
**(descNSG)**, xiv, 26, 27, 36  
**(descnxt)**, xiv, 39, 40, 43, 67, 69  
**(descper)**, xv, 84, 85  
**(descPP)**, xiv, 26, 27, 33, 34  
**(descpsp)**, xv, 79, 80  
**(descsad)**, xv, 81  
**(descshi)**, xiv, 51, 52  
**(descSP)**, xiv, 26, 27, 29, 30  
**(descsph)**, xv, 64, 67  
**(descsybil)**, xiv, 40, 45, 67, 69  
**(descslm)**, xv, 88, 89  
**(desctrack)**, xiv, 39, 40, 53, 54, 67, 69  
**(desctrak)**, 61  
**(descXL)**, xiv, 53–56  
**(descxs)**, xiv, 11–13  
 DIAG, 28, 29, 34, 54–56  
*dil*, 21, 22  
 DIMENSIONS, 87  
 DIR, 85, 89, 90  
 DIRA, 70, 72  
 DIRECTION, 64, 65  
 DIRECTIONS, 89  
*DIRN*, 64, 66  
*DIRO*, 64, 67  
*dist*, 89, 90  
 DIST, 89, 90  
*disxyz*, 30, 31  
 DNAME, 78  
 DP00, 45–48  
 DP01, 45–47, 49  
**(DRAGON)**, xiv, 3, 4  
 DRAGON, 16, 18, 75  
 DUAL, 49, 50  
*dxt*, 70

## E

**(EDI:)**, xv, 63  
 EDI:, ix, 6, 7, 17, 37, 63, 68, 73, 74, 159  
 EDINAM, 63, 66–68, 72, 73, 81, 84  
 EDIT, 10, 16, 19, 26, 27, 40, 41, 52, 54, 57, 61, 62, 64, 70, 73, 75, 79–82, 87–89  
 EDITION, 7, 9, 63, 66, 73, 81, 84  
*efiss*, 13, 14  
 EFISS, 13  
 EGPA, 57, 58, 81, 83  
 END:, 4, 5  
 ENDCHAIN, 20, 21  
 ENER, 11, 12

energy, 11, 12, 20, 21, 64, 66, 81, 83  
 ENR:, 75  
 enrichment, 75, 76  
 EPS, 52  
 EPS1, 70, 71  
 EPS2, 70, 71  
 epsgpa, 57  
 epsgps, 58  
 epsout, 57, 58, 62, 81, 82  
 epsthr, 57, 58, 62, 81, 82  
 epsunk, 57, 58, 62, 81, 82  
 EQW, 42–48  
 ETAB, 62  
 (evo), xv, 70  
 (EVO:), xv, 69  
 EVO:, ix, 6–8, 69, 87, 126  
 EVONAM, 70  
 EXAC, 61, 62  
 (EXCELL:), xiv, 53  
 EXCELL:, viii, 6, 7, 31, 53–56, 80  
 (EXCELT:), xiv, 39  
 EXCELT:, viii, 1, 5–7, 31, 37–41, 43, 53, 54, 56, 59, 65, 67–69, 78–80, 92, 93, 122, 126  
 EXPM, 70, 71  
 EXTE, 57, 58, 62, 81, 82  
 EXTR, 70, 72  
 EXTRACT, 73, 74

## F

FBMXSDB, 8, 76  
 FIL:, 16, 18, 75  
 FILL, 80  
 FIXA, 13, 14  
 FIXE, 13, 14  
 FIXG, 13, 14  
 FLIB, 64, 66  
 (FLU:), xiv, 56  
 FLU:, viii, 6, 7, 37, 54, 56, 68  
 FLUNAM, 56, 57, 59–61, 63, 69, 79–81, 84  
 FLUNAP, 84  
 flux, 70, 71  
 FLUX, 64, 67, 70, 71, 80  
 fluxes, 57, 81, 82  
 FLUXNAM, 84  
 FLUXNAP, 84, 85  
 FLUXUNK, 7, 56, 57, 61, 63, 69, 70, 80–82, 84, 94  
 FLX, 57, 81, 82  
 fract, 36, 37  
 FREE, 22  
 FROM, 20, 21

## G

G, 59, 60

GAUS, 42–48  
 GC, 52  
 GELB, 54–56  
 GEO, 64, 65  
 (GEO:), xiv, 25  
 GEO:, viii, 3, 5, 7, 11, 25, 26, 37, 42, 45, 47, 50  
 GEOMETRY, 7, 25, 39, 40, 53, 61, 63, 79  
 GEONAM, 25, 39, 40, 53, 61, 79  
 GET, 75, 85, 86, 88  
 GET MASS, 76  
 GLOB, 70, 72  
 GLOBAL, 87  
 GOXSRN, 11, 12  
 GOXSWN, 11, 12  
 GRAY, 80  
 GRMAX, 52  
 GRMIN, 52  
 GROUP, 26, 27

## H

H1, 70, 72  
 HALT, 45–48  
 HBC, 28, 29  
 HCELL, 34, 35  
 HCOH, 21, 22  
 hd2, 75  
 HEDIT, 16, 17  
 HELI, 54–56  
 HETE, 54, 59  
 HEX, 26, 32, 38  
 HEXCEL, 26, 27, 33, 34, 38  
 HEXCELZ, 26, 27, 33, 34  
 HEXZ, 26, 33, 38  
 HINC, 21, 22  
 HISO, 64, 66  
 HISTORY, xv, 8, 85–88  
 HISTORY, 85, 86  
 HOMO, 67, 68  
 HOMOGE, 25, 26, 38  
 HSB, 80  
 HST:, ix, 6, 8, 85, 86  
 (hstbrn), xv, 86–88  
 (hstdim), xv, 85–87  
 (hstpar), xv, 85, 86, 88  
 HTURN, 34, 35  
 hu8, 75

## I

iaea, 125  
 ialbp, 15  
 ibun, 85, 86  
 iburn, 19

*icha*, 85, 86  
*icode*, 28, 29  
*icol*, 49, 50  
*icond*, 64, 66, 81, 83  
*IDEM*, 59, 60  
*idfuel*, 85, 86  
*idir*, 89, 90  
*idirm*, 64, 66, 67  
*idiro*, 64, 67  
*ielem*, 49, 50  
*igroup*, 11  
*ilastg*, 13, 14  
*imat*, 11, 12  
*imerge*, 34, 35  
*imix*, 34, 35  
*imixa*, 64, 66  
*imixm*, 64, 65, 83  
*imixt*, 64, 65, 81, 84  
*imxit*, 52  
*INF*, 21, 22  
**(INFO:)**, xv, 74  
*INFO:*, ix, 6, 74, 76, 155  
*INFOR*, 78  
*INIT*, 57, 81, 82  
*INPUT*, 3  
*INPUT*, 11, 12  
*inrs*, 21, 22, 51  
*IP00*, 47, 48  
*IP01*, 47, 48  
*iplan*, 89, 90  
*iplot*, 89  
*iprint*, 4, 10, 16, 19, 26, 27, 40, 41, 52, 54, 57, 61, 62, 64, 70, 73, 75, 79–82, 87, 89  
*iqua1*, 45–48  
*iqua2*, 45–48  
*iquab*, 45, 47, 49  
*ireg*, 81, 83, 84  
*iregm*, 64, 65  
*iregt*, 64, 65  
*irmrg*, 79  
*ismrg*, 79  
*ISO:*, 75, 76  
*ISONAM*, 75, 76  
*ISOT*, 64, 66  
*isplh*, 49, 50  
*ispltr*, 30, 31  
*ispltx*, 30  
*isplty*, 30  
*ispltz*, 30  
*isymm*, 42, 43, 56  
*ITLM*, 62, 63  
*iuv*, 89, 90

*izae*, 20

## J

**(JPMT:)**, xiv, 39

*JPMT:*, viii, 1, 6, 7, 31, 35, 37–40, 47, 53, 54, 67–69, 91–94, 126

## K

*K*, 57, 59, 62, 75, 81, 82

*KAPS*, 70, 72

*KEFF*, 59, 60

## L

*L*, 57, 58

*LCMD*, 42–44

*LEVE*, 52

*level*, 52, 53

*lgrmax*, 52

*lgrmin*, 52

*lh*, 26, 27

**(LIB:)**, xiv, 15

*LIB:*, viii, 5, 7, 15, 16, 18, 19, 73, 75, 125, 155

*LIBNAM*, 53, 56, 61, 63, 81, 84

*LIBNAP*, 84

*LIGN*, 45–47, 49

*LIN*, 85

*LINKED\_LIST*, 4

*LJ*, 52

*LKRD*, 59, 68

*LOCAL*, 87

*lp*, 26, 27, 36

*lr*, 25–27, 30

*lx*, 26, 27, 30

*ly*, 26, 27, 30

*lz*, 26, 27, 30

## M

*m-file*, 6, 88

**(MAC:)**, xiv, 9

*MAC:*, viii, 5, 7, 9, 10, 12, 29, 73, 94

*MACGEO*, 67, 68

*MACLIB*, 9–11, 13

*MACOLD*, 19

*MACROBIL*, 9

*MACROLIB*, 5, 7, 9, 11–13, 16, 53, 56, 57, 61, 63, 66, 81, 82, 84

*MAP*, xv, 85–87

*MAP*, 85, 86

*mass*, 75, 76

*MASS*, 75

*mati*, 21, 23

*matnum*, 13, 21, 23, 24

*matold*, 24

MATXS, 16–18, 22, 52, 75  
 MATXS2, 16–18, 22, 75  
*maxcur*, 45, 47  
*maxint*, 45, 47  
 MAXJ, 45, 47  
*maxmix*, 34, 36, 37, 65, 66, 83, 84  
*maxout*, 57, 58, 62, 81, 82  
 MAXR, 42, 45, 47, 49, 50  
*maxreg*, 31, 37, 42, 45, 47, 49, 50, 65, 83, 84  
 MAXS, 19  
*maxscr*, 62  
*maxthr*, 57, 58, 62, 63, 81, 82  
 MAXZ, 45, 47  
 MCU, 60  
 (MCU:), xiv, 61  
 MCU: , viii, ix, 6, 7, 60–62, 122  
 MEDI, 42  
 MERG, 64–66, 68, 81, 83  
 MERGE, 34, 35, 128  
 MESHX, 30, 93  
 MESHY, 30, 93  
 MESHZ, 30  
 MFILE, 88  
 MGEO, 67, 68  
 MGFLUX, 80  
 MICLIB, 9, 15, 16, 19, 20, 24, 51  
 MICNAM, 69  
 MICOLD, 15, 19, 24  
 MICR, 64, 66, 74  
 MICROLIB, 5, 7, 9, 13, 15, 16, 24, 51, 53, 56, 57, 61, 63, 66, 69, 81, 82, 84  
*milie*, 36  
 MIX, 12, 13, 21, 24, 34, 64, 65, 81, 83, 84  
*mixdil*, 36  
*mixgr*, 36, 37  
 MIXS, 16, 18  
 MIXTURE, 80  
 MOCC, 7  
 (MOCC:), xiv, 61  
 MOCC: , viii, ix, 6, 7, 60, 61, 114, 116, 119, 157  
 MODNAME, 4  
 (module), 4, 5  
 MODULE, 4  
 (MRG:), xv, 78  
 MRG: , ix, 6, 7, 78  
 MTRK, 67, 68  
 MXIS, 16  
 MXIT, 52

## N

N, 57, 62, 81, 82  
 N2N, 17, 20

N2NF, 17  
 N3N, 17, 20  
 N3NF, 17  
 N4N, 17, 21  
 NA, 17, 21  
*naccel*, 57, 58, 62, 81, 83  
*nacti*, 66  
*nalbp*, 11, 15  
 NALBP, 11  
 NAMALI, 21, 22, 24  
 NAMDPL, 20  
 NAME, 54, 55, 73, 74  
 NAMEFIL, 16, 18, 75  
 NAMISO, 21, 22, 24  
 NAMPAR, 20, 21, 88  
 NAMPIN, 34, 35  
 NAMREC, 85  
 NAMS, 21, 22  
*nanagl*, 42–44, 56  
*nanis*, 40, 41, 54  
*naniso*, 10, 13, 16, 17, 91  
 NBAL, 64, 67  
*nbiso*, 75, 76  
 NBPN, 61, 62  
*nbscat*, 13, 14  
*nbun*, 87  
*ncha*, 87  
 NCOR, 81, 83  
*nd2*, 76  
*ndepl*, 16, 18  
 NDIR, 73, 74  
*nedit*, 16, 17  
 NELAS, 17  
 NEWNAME, 73, 74  
 NF, 17  
 NFSLO, 17  
 NFTOT, 13, 14, 21, 81  
 NG, 17, 20  
*nglo*, 87  
*nglob*, 87  
 NGRO, 10, 11  
*ngroup*, 10–13, 15, 57, 58, 66, 81–83, 91  
*ngroup+1*, 66, 83  
*nh1*, 75, 76  
 NHEAT, 17  
 NIFI, 10  
*nifiss*, 10, 13  
 NINEL, 17  
*nis*, 64, 66  
*nl*, 61, 62  
*nlibre*, 57, 58, 62, 81, 83  
*nloc*, 87

*nmilg*, 36  
*nmisot*, 16  
*nmistr*, 36  
*nmix*, 66  
 NMIX, 10, 16  
*nmixt*, 10–13, 16, 21  
 NMPIJ, 54, 55  
 NNF, 17  
*no16*, 75, 76  
 NOBA, 62  
 NOCONTOUR, 80  
 NODI, 70, 71  
 NOEV, 21, 23  
 NOEX, 70, 72  
 NOGC, 52  
 NOGL, 70, 72  
 NOLJ, 52  
 NOMDIR, 73  
 NONE, 16, 54–56, 64, 65, 80, 81  
 NONL, 54–56  
 NoPause, 89, 90  
 NOR2, 54, 58, 83  
 NORE, 40, 41  
 NORM, 11, 12, 42, 44, 54–58  
 NOSA, 70  
 NOTR, 43, 44, 52, 73  
 NP, 17, 21  
*nphi*, 42–44  
 NPIN, 30, 31  
*npins*, 30, 31, 33  
*nplots*, 89  
*nreg*, 79  
*nregio*, 57, 81  
*ns*, 36  
 NSAT, 70, 71  
*nsegment*, 45–48  
*nsubg*, 55, 56  
*nsur*, 79  
*ntfg*, 21, 23  
*nth2*, 75, 76  
 NTOT0, 17  
 NTOT1, 17  
 NTPO, 89  
*nu3*, 75, 76  
*nu5*, 75, 76  
*nu8*, 76  
 NUDEL, 17  
*numnew*, 12, 13  
*numold*, 12, 13  
 NUSIGF, 13, 14, 81  
 NWT0, 17  
 NWT1, 17

(NXT:), xiv, 39  
 NXT:, viii, 5–7, 31, 37–41, 43, 45, 54, 67–69, 80, 88, 92, 93

## O

*OFF*, 62  
 OFF, 11–13, 57, 58, 67, 68, 81–83  
 OFFCENTER, 30, 31  
 OLD, 47  
*OLDGEO*, 25–27  
 OLDL, 12, 13  
*OLDLIB*, 9, 13, 51  
*OLDMIC*, 69  
*OLDNAME*, 73, 74  
 OLDW, 16, 17  
 ON, 62  
 ON, 11–13, 57, 58, 64, 66, 81, 82

## P

P0, 59, 68  
 POW, 64, 65  
 P1, 59, 68  
 P1SCAT, 64  
 P1W, 64, 65  
 PAF, 57, 81, 82  
*param*, 76  
*pcinl*, 36, 37  
*pcorn*, 42, 43, 45, 56  
*pcut*, 42–44  
 PER, 85  
 (PER:), xv, 84  
 PER:, ix, 6, 7, 84  
*period*, 88  
 PERT, 64, 67  
 PIJ, 52–55  
*pijcel*, 36, 37  
 PIJK, 41, 54, 59  
*PIJNAM*, 53, 55, 56, 81  
 PISO, 42–44  
 PLAN, 89, 90  
 PLANA, 89  
 PLANP, 89  
 PNL, 59  
 PNOR, 54–56  
 PNTN, 43, 44  
 POINTS, 89  
 POURCE, 36, 37  
*power*, 70, 71, 88  
 POWR, 70, 71  
*PREFIX*, 73  
 PRIM, 49, 50  
 PROCEDURE, 4, 5

PROCEL, 36, 37  
 PROCNAME, 4, 5  
 PROM, 16, 17  
 PSGEO, 79  
 (PSP:), xv, 79  
 PSP:, ix, 6, 7, 44, 79, 80  
 PSPC, 42–44  
 PUR:, 75  
 purity, 75  
 PUT, 86, 88

## Q

QUA1, 45–48  
 QUA2, 45–48  
 QUAB, 45, 47, 49

## R

R, 59, 60  
 R+, 28  
 R120, 28, 29  
 R180, 28, 29  
 RADIUS, 30  
 RATE, 64, 67  
 RDEPCHN, 16, 18  
 reaction, 20, 21  
 READ, 11, 12  
 REBA, 57, 58, 81, 82  
 RECD, 47, 49  
 RECR, 47, 49  
 RECT, 45, 47, 49  
 REFE, 64, 67  
 REFGEO, 63  
 REFL, 28  
 REFPIJ, 63  
 REGI, 64, 65, 79, 81, 83, 84  
 REGION, 80  
 relden, 24  
 relvol, 21, 23  
 REND, 40, 41  
 RENM, 40, 41  
 RENO, 40, 41  
 REPEAT, 34, 35  
 RGB, 80  
 RNAME, 78  
 RNANE, 78  
 ROT+, 45–49  
 ROTH, 45–49  
 RPIN, 30, 31  
 rpins, 30, 31, 39  
 rrr, 30  
 rs, 36  
 RUNG, 70, 72

## S

S, 57, 62, 70, 71, 81, 82  
 S30, 28, 29  
 S90, 28, 29  
 SA180, 28, 29  
 SA60, 28, 29  
 (SAD:), xv, 81  
 SAD:, ix, 6, 7, 81, 83, 84  
 SADNAM, 82  
 SAT, 70, 71  
 SATOFF, 70, 71  
 SAVE, 64, 66, 70, 73, 81, 83  
 SB180, 28, 29  
 SB60, 28, 29  
 SCAD, 81  
 SCAT, 13, 14  
 SCR, 62  
 SELE, 67, 68, 81, 84  
 SEQ\_ASCII, 4  
 SEQ\_BINARY, 4  
 SET, 70  
 (SHI:), xiv, 51  
 SHI:, viii, 6, 7, 22, 37, 51  
 SHIB, 21, 22  
 SIDE, 30, 31  
 sidhex, 30, 31  
 SIGS, 59  
 SKIP, 54–56, 59  
 SMS, 43, 44  
 SP01, 47, 48  
 SPH, 49, 64, 67, 159  
 SPHE, 36  
 SPHERE, 25, 26, 32, 38, 48  
 SPHGEO, 63, 68  
 SPHLINE, 63, 68  
 SPHNAM, 67, 68  
 SPHTRK, 63, 68  
 SPLITR, 30, 31, 92  
 SPLITX, 30  
 SPLITY, 30  
 SPLITZ, 30  
 SPRD, 67, 68  
 SSYM, 28  
 STABLE, 20, 21  
 STAT, 64, 67  
 STEP, 73  
 STRNAME, 4, 5  
 SUBG, 55, 56  
 SUBGEO, 26, 27  
 SURF, 79  
 (SYBILT:), xiv, 40

SYBILT: , viii, 1, 6, 7, 31, 35, 37, 38, 40, 45, 67–69,  
91–94, 126

SYME, 28, 29, 34

SYMM, 42, 43, 56

## T

TAKE, 64–66, 81, 83

*tburn*, 19

TCM01, ix, xii, 94, 185

TCM02, ix, xii, 96, 186

TCM03, ix, xii, 98, 187

TCM04, ix, 103

TCM05, ix, 105

TCM06, ix, 109

TCM07, ix, 110

TCM08, ix, 112

TCM09, ix, 114

TCM10, ix, 116

TCM11, ix, 119

TCM12, ix, 94, 122

TCOH, 21, 22

TCWU01, ix, xii, 125, 126, 189

TCWU02, ix, xii, 128, 190

TCWU03, ix, xii, 131, 191

TCWU04, ix, 134

TCWU05, ix, 136, 152

TCWU06, ix, 140

TCWU07, ix, 144

TCWU08, ix, 146

TCWU09, ix, 148

TCWU10, ix, 150

TCWU11, ix, 152

TCWU12, x, 155

TCWU13, x, 157

TCWU14, x, 125, 159

TDXS, 70, 72

*temp*, 21, 22, 75

*tempd*, 21, 22

TFILNEW, 78

TFIOLD, 78

THER, 21, 22, 57, 58, 62, 81, 82

THO2, 75, 76

TISO, 42–44, 56, 126

TITL, 40, 41

TITLE, 40, 41, 78

TIXS, 70, 72

(TLM:), xv, 88

TLM:, ix, 6, 88, 89

TMP:, 75

TOTAL, 13, 14, 81

TRACKING, 7, 38–40, 51, 53, 54, 56, 61, 63, 68, 69,  
78, 80, 81, 84, 89

TRAK, 42, 55

TRAN, 13, 14, 28

TRANC, 81

TRKFIL, 39, 40, 51, 53, 54, 61, 88, 89

TRKNAM, 39, 40, 47, 51, 53, 56, 61, 63, 69, 79–81,  
84, 88, 89

TRKNEW, 78

TRKOLD, 78

TSPC, 42, 44, 126

TUBE, 26, 31, 32, 34–36, 38, 48

TUBEX, 26, 31, 32, 34, 35

TUBEY, 26, 31, 32, 35

TUBEZ, 26, 31, 33–35, 38, 48

TURN, 34, 35, 128

TYPE, 57, 62, 80–82, 85

## U

U, 89, 90

UNKT, 57, 58, 62, 81, 82

UO2, 75, 76

UPDL, 12, 13

UPS, 64, 65

## V

V, 89, 90

*valb2*, 59, 60

*valbr2*, 59, 60

*valbx2*, 59, 60

*valby2*, 59, 60

*valbz2*, 59, 60

*valeps*, 52

*valeps1*, 70, 71

*valeps2*, 70, 71

*valexp*, 70, 71

*valh1*, 70, 72

*valk*, 59, 60

*valpar*, 88

VIRTUAL, 25, 26, 38

VOID, 28, 55, 57–59, 68

## W

W/CC, 70, 71

WATER, 75, 76

wcc, 70, 71

WGT%, 75, 76

WIMS, 11, 16–18, 75

WIMSAECL, 16–18, 52, 75

WIMSD4, 16–18, 52, 75

WRIT, 11

## X

X, 59, 60

X+, 28, 30, 34, 35

X-, 28, 30, 34, 35  
xschi, 13, 14  
xsfiss, 13, 14  
xsfixa, 13, 14  
xsfixe, 13, 14  
xsfixg, 13, 14  
XSM\_FILE, 4  
xsscat, 13, 14  
xssigf, 13, 14  
xssigt, 13, 14  
xssigtr, 13, 14  
xtf, 70-72  
xti, 70-72  
xtr, 70, 71  
xts, 70, 71  
xxx, 30

**Y**

Y, 59, 60  
Y+, 28, 30, 34, 35  
Y-, 28, 30, 34, 35  
YEAR, 70, 71  
yield, 20, 21  
yyy, 30

**Z**

Z, 59, 60  
Z+, 28, 30, 34, 35  
Z-, 28, 30, 34, 35  
zzz, 30